

# Dynamic Analysis Using MSC Nastran

**NAS102A Workbook**

---

*June 2013*



## Legal Information

MSC.Software Corporation reserves the right to make changes in specifications and other information contained in this document without prior notice. The concepts, methods, and examples presented in this text are for illustrative and educational purposes only, and are not intended to be exhaustive or to apply to any particular engineering problem or design. MSC.Software Corporation assumes no liability or responsibility to any person or company for direct or indirect damages resulting from the use of any information contained herein.

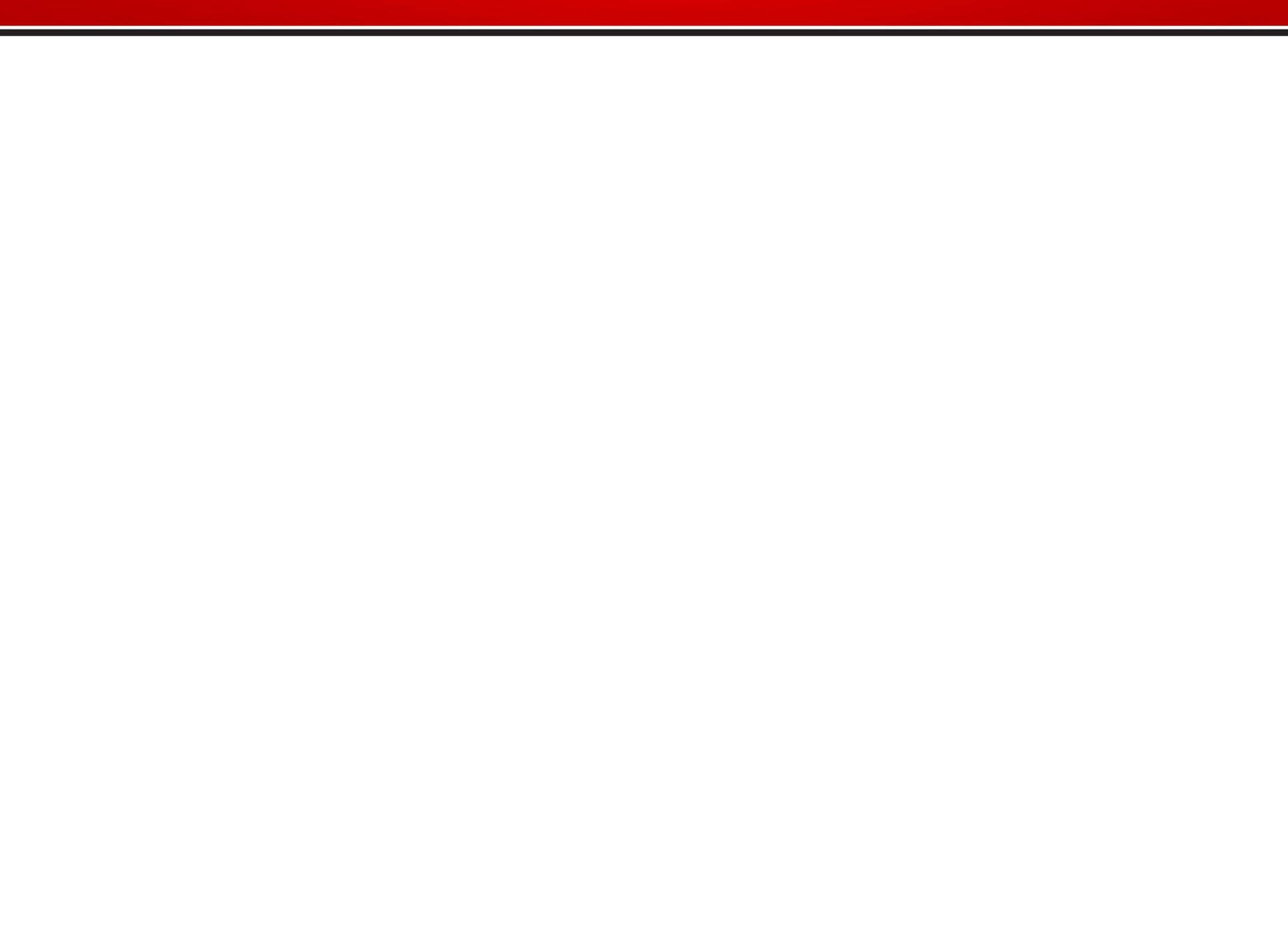
Copyright © 2013 MSC.Software Corporation. All Rights Reserved. This notice shall be marked on any reproduction of this documentation, in whole or in part. Any reproduction or distribution of this document, in whole or in part, without the prior written consent of MSC.Software Corporation is prohibited.

The MSC.Software corporate logo, Adams, Dytran, Easy5, Fatigue, Laminate Modeler, Marc, Mentat, MD Nastran, Patran, MSC, MSC Nastran, Mvision, Patran, SimDesigner, SimEnterprise, SimManager, SimXpert and Sofy are trademarks or registered trademarks of the MSC.Software Corporation in the United States and/or other countries. NASTRAN is a registered trademark of NASA. All other trademarks belong to their respective owners.

# CONTENTS

## Workshop

- 1 Modal Analysis of a Flat Plate
- 2 Normal Modes with Preload
- 3 Normal Modes Analysis Using Guyan Reduction
- 4 Direct Transient Response
- 5 Modal Transient Response
- 6 Direct Frequency Response
- 7 Modal Frequency Response
- 8a Direct Transient Response with Enforced Acceleration
- 8b Modal Transient Response with Enforced Acceleration
- 9a Direct Frequency Response with Enforced Displacement
- 9b Modal Frequency Response with Enforced Displacement
- 10a Generate Shock Spectrum Input
- 10b Apply Shock Spectrum
- 11 Random Response with Single Input
- 12 Random Response with Multiple Inputs



# **WORKSHOP 1**

## **MODAL ANALYSIS OF A FLAT PLATE**



- **Workshop Objectives**

- Use the Lanczos method to find the first ten natural frequencies and mode shapes of a flat rectangular plate.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

- plate.bdf
- wkshp1.dat

- **Problem Description:**

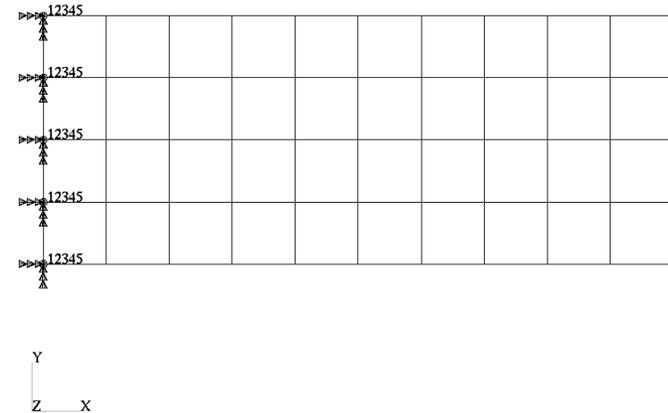
- The next page contains information on the flat plate, including the finite element representation, boundary condition, and structural parameters necessary to construct the input file.

## Structural Information

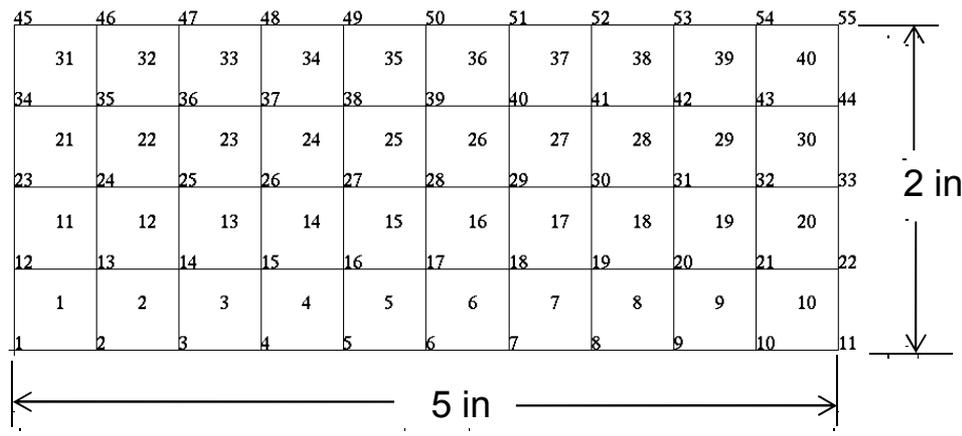
Table 3A.

Length (a)	5 in
Height (b)	2 in
Thickness	0.100 in
Weight Density	0.282 lbs/in <sup>3</sup>
Mass/Weight Factor	2.59E-3 sec <sup>2</sup> /in
Elastic Modulus	30.0E6 lbs/in <sup>2</sup>
Poisson's Ratio	0.3

## Boundary Condition



## Grid Coordinates and Elements



- **Suggested Steps**

1. Open and review the plate.bdf include file.
2. Modify the starting input file, wkshp1.dat, to add the Lanczos method.
3. Save and run the new input file.
4. Review the MSC Nastran results using the solution file soln1.f06.

# Step 1. Open and Review the Plate.bdf File

```
$
$ plate.bdf
$
$ geometric input file for plate model
$
PSHELL 1 1 .1 1 1
CQUAD4 1 1 1 2 13 12
CQUAD4 2 1 2 3 14 13
CQUAD4 3 1 3 4 15 14
CQUAD4 4 1 4 5 16 15
CQUAD4 5 1 5 6 17 16
CQUAD4 6 1 6 7 18 17
CQUAD4 7 1 7 8 19 18
CQUAD4 8 1 8 9 20 19
CQUAD4 9 1 9 10 21 20
CQUAD4 10 1 10 11 22 21
CQUAD4 11 1 12 13 24 23
CQUAD4 12 1 13 14 25 24
CQUAD4 13 1 14 15 26 25
CQUAD4 14 1 15 16 27 26
CQUAD4 15 1 16 17 28 27
CQUAD4 16 1 17 18 29 28
CQUAD4 17 1 18 19 30 29
CQUAD4 18 1 19 20 31 30
CQUAD4 19 1 20 21 32 31
CQUAD4 20 1 21 22 33 32
```

```
CQUAD4 21 1 23 24 35 34
CQUAD4 22 1 24 25 36 35
CQUAD4 23 1 25 26 37 36
CQUAD4 24 1 26 27 38 37
CQUAD4 25 1 27 28 39 38
CQUAD4 26 1 28 29 40 39
CQUAD4 27 1 29 30 41 40
CQUAD4 28 1 30 31 42 41
CQUAD4 29 1 31 32 43 42
CQUAD4 30 1 32 33 44 43
CQUAD4 31 1 34 35 46 45
CQUAD4 32 1 35 36 47 46
CQUAD4 33 1 36 37 48 47
CQUAD4 34 1 37 38 49 48
CQUAD4 35 1 38 39 50 49
CQUAD4 36 1 39 40 51 50
CQUAD4 37 1 40 41 52 51
CQUAD4 38 1 41 42 53 52
CQUAD4 39 1 42 43 54 53
CQUAD4 40 1 43 44 55 54
$
MAT1 1 3.+7 .3 .282
$
```

 Weight Density  
see PARAM,WTMASS

# Step 1. Open and Review the Plate.bdf File (Cont.)

```
$
GRID 1      0.    0.    0.
GRID 2      .5    0.    0.
GRID 3      1.    0.    0.
GRID 4      1.5  0.    0.
GRID 5      2.    0.    0.
GRID 6      2.5  0.    0.
GRID 7      3.    0.    0.
GRID 8      3.5  0.    0.
GRID 9      4.    0.    0.
GRID 10     4.5  0.    0.
GRID 11     5.    0.    0.
GRID 12     0.    .5    0.
GRID 13     .5    .5    0.
GRID 14     1.    .5    0.
GRID 15     1.5  .5    0.
GRID 16     2.    .5    0.
GRID 17     2.5  .5    0.
GRID 18     3.    .5    0.
GRID 19     3.5  .5    0.
GRID 20     4.    .5    0.
GRID 21     4.5  .5    0.
GRID 22     5.    .5    0.
GRID 23     0.    1.    0.
GRID 24     .5    1.    0.
GRID 25     1.    1.    0.
GRID 26     1.5  1.    0.
GRID 27     2.    1.    0.
GRID 28     2.5  1.    0.
GRID 29     3.    1.    0.
GRID 30     3.5  1.    0.
```

```
GRID 31     4.    1.    0.
GRID 32     4.5  1.    0.
GRID 33     5.    1.    0.
GRID 34     0.    1.5  0.
GRID 35     .5    1.5  0.
GRID 36     1.    1.5  0.
GRID 37     1.5  1.5  0.
GRID 38     2.    1.5  0.
GRID 39     2.5  1.5  0.
GRID 40     3.    1.5  0.
GRID 41     3.5  1.5  0.
GRID 42     4.    1.5  0.
GRID 43     4.5  1.5  0.
GRID 44     5.    1.5  0.
GRID 45     0.    2.    0.
GRID 46     .5    2.    0.
GRID 47     1.    2.    0.
GRID 48     1.5  2.    0.
GRID 49     2.    2.    0.
GRID 50     2.5  2.    0.
GRID 51     3.    2.    0.
GRID 52     3.5  2.    0.
GRID 53     4.    2.    0.
GRID 54     4.5  2.    0.
GRID 55     5.    2.    0.
$
SPC1  1      12345  1      12      23      34      45
```

# Step 2. Modify the wkshp1.dat File

Start with the partial input file wkshp1.dat and change the file name to **soln1.dat**, then modify as follows:

## Executive Control Section

- a. Add the solution sequence, **SOL 103**.

## Case Control Section

- b. Add eigenvalue **METHOD** callout.
- c. Add eigenvector printout.

## Bulk Data Section

- d. Add weight/mass conversion factor.
- e. Add eigenvalue method with **10** roots.

Start with partial input file,  
wkshp1.dat

```

$
$   wkshp1.dat
$
$   exec control add:  solution sequence
$   case control add:  eigenvalue method callout
$                       eigenvector printout
$
$   bulk data add:    weight/mass conversion factor
$                       eigenvalue method
$
CEND
TITLE = NORMAL MODES EXAMPLE
ECHO = UNSORTED
SUBCASE 1
    SUBTITLE= USING LANCZOS
    SPC = 1
BEGIN BULK
PARAM,POST, 0
PARAM   COUPMASS 1
$
include 'plate.bdf'
$
ENDDATA

```

Modified input file,  
save as soln1.dat

```

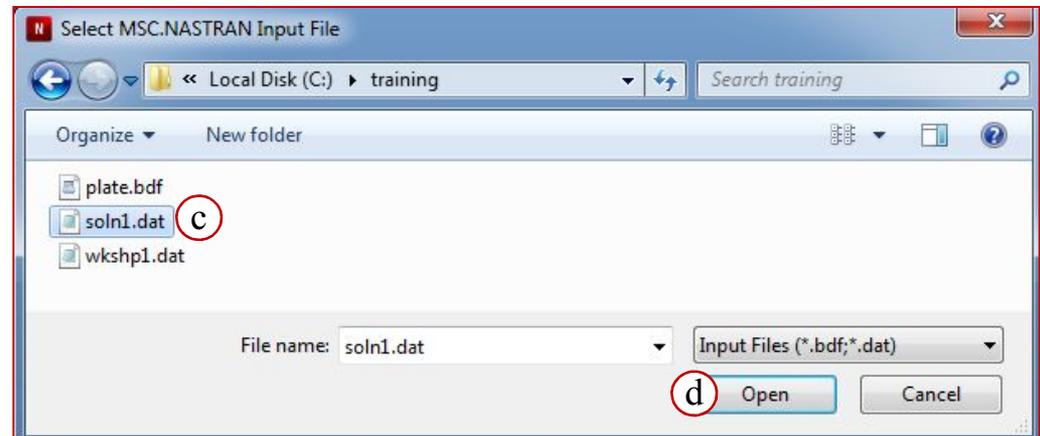
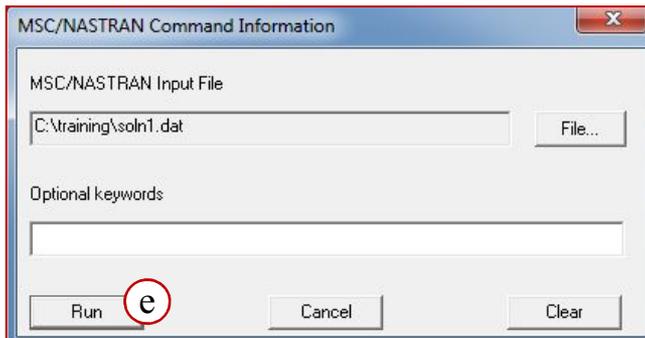
$
$   soln1.dat
$
SOL 103 (a)
CEND
TITLE = NORMAL MODES EXAMPLE
ECHO = UNSORTED
SUBCASE 1
    SUBTITLE= USING LANCZOS
    (b) METHOD = 1
    SPC = 1
    (c) VECTOR=ALL
BEGIN BULK
PARAM,POST,0
PARAM   COUPMASS 1
PARAM   WTMASS   .00259
    (d) EIGRL     1                10      0
    (e)
$
include 'plate.bdf'
$
ENDDATA

```

# Step 3. Save and Run the Input File

Save and run the modified file in Nastran.

- a. Save the modified file as **soln1.dat**.
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln1.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 4. Review the Results

## 1<sup>st</sup> 10 Natural Frequencies (eigenvalues) of the Plate

```

E I G E N V A L U E   A N A L Y S I S   S U M M A R Y   (READ MODULE)

      BLOCK SIZE USED ..... 7
      NUMBER OF DECOMPOSITIONS ..... 2
      NUMBER OF ROOTS FOUND ..... 10
      NUMBER OF SOLVES REQUIRED ..... 7

1  NORMAL MODES EXAMPLE
0
                                           PAGE    10
                                           SUBCASE 1

      M O D E      E X T R A C T I O N      R E A L   E I G E N V A L U E S
      N O .      O R D E R      E I G E N V A L U E      R A D I A N S      C Y C L E S      G E N E R A L I Z E D      G E N E R A L I Z E D
                                           M A S S      S T I F F N E S S
      1           1           7.055894E+05      8.399937E+02      1.336891E+02      1.000000E+00      7.055894E+05
      2           2           1.877186E+07      4.332651E+03      6.895628E+02      1.000000E+00      1.877186E+07
      3           3           2.811177E+07      5.302053E+03      8.438480E+02      1.000000E+00      2.811177E+07
      4           4           1.929422E+08      1.389036E+04      2.210720E+03      1.000000E+00      1.929422E+08
      5           5           2.221657E+08      1.490523E+04      2.372240E+03      1.000000E+00      2.221657E+08
      6           6           2.328451E+08      1.525926E+04      2.428587E+03      1.000000E+00      2.328451E+08
      7           7           6.832397E+08      2.613885E+04      4.160127E+03      1.000000E+00      6.832397E+08
      8           8           9.600053E+08      3.098395E+04      4.931249E+03      1.000000E+00      9.600053E+08
      9           9           1.365293E+09      3.694987E+04      5.880754E+03      1.000000E+00      1.365293E+09
      10          10          1.850317E+09      4.301531E+04      6.846099E+03      1.000000E+00      1.850317E+09
  
```

# Step 4. Review the Results (Cont.)

1<sup>st</sup> Mode shape (eigenvector) of the Plate  
(see the soln1.f06 file for all 10 eigenvectors)

1 NORMAL MODES EXAMPLE										PAGE	11
0 USING LANCZOS										SUBCASE 1	
EIGENVALUE = 7.055894E+05											
CYCLES = 1.336891E+02											
REAL EIGENVECTOR NO. 1											
POINT ID.	TYPE	T1	T2	T3	R1	R2	R3				
1	G	0.0	0.0	0.0	0.0	0.0	-3.203115E-16				
2	G	-2.647930E-16	-5.375144E-16	-9.732725E-01	-1.099511E+00	4.003941E+00	-8.053012E-16				
3	G	-8.087117E-16	-4.758965E-16	-4.168619E+00	-1.599071E+00	8.686669E+00	-6.711056E-16				
4	G	-1.626329E-15	-1.430922E-15	-9.445514E+00	-1.530855E+00	1.230146E+01	-7.343100E-16				
5	G	-2.322747E-15	-3.606068E-15	-1.636256E+01	-1.365152E+00	1.522518E+01	-3.038820E-15				
6	G	-1.990909E-15	-5.712441E-15	-2.455516E+01	-1.080930E+00	1.740494E+01	-2.924235E-15				
7	G	-2.838505E-15	-5.273217E-15	-3.367780E+01	-8.040399E-01	1.895419E+01	-2.625783E-15				
8	G	-2.569822E-15	-8.191124E-15	-4.362896E+01	-5.477144E-01	1.993718E+01	-4.513898E-15				
9	G	-2.878096E-15	-9.511272E-15	-5.355173E+01	-3.472317E-01	2.046533E+01	-2.554486E-15				
10	G	-1.787771E-15	-7.901818E-15	-6.384777E+01	-2.192121E-01	2.066150E+01	-7.381784E-16				
11	G	-1.525222E-15	-1.227910E-14	-7.419273E+01	-1.687060E-01	2.069914E+01	-2.505442E-15				
12	G	0.0	0.0	0.0	0.0	0.0	-9.275404E-17				
13	G	-1.817918E-16	-2.669867E-16	-1.263801E+00	-1.865870E-01	4.860682E+00	-3.589973E-16				
14	G	-5.010032E-16	-5.740304E-16	-4.701082E+00	-5.743318E-01	8.765023E+00	-1.347162E-15				
15	G	-5.656739E-16	-1.027553E-15	-9.996819E+00	-7.007096E-01	1.228685E+01	-1.209610E-15				
16	G	-9.612353E-16	-2.247265E-15	-1.686138E+01	-6.388398E-01	1.505788E+01	-1.898507E-15				
17	G	-6.105141E-16	-4.902903E-15	-2.495921E+01	-5.380088E-01	1.722623E+01	-2.911906E-15				
18	G	-1.005600E-15	-5.329151E-15	-3.398207E+01	-4.108650E-01	1.877065E+01	-3.143212E-15				
19	G	-8.334120E-16	-6.381899E-15	-4.364096E+01	-2.955683E-01	1.978425E+01	-2.666923E-15				
20	G	-6.960247E-16	-1.165354E-14	-5.369084E+01	-2.025815E-01	2.035270E+01	-2.617565E-15				
21	G	-6.969010E-16	-1.455675E-14	-6.394039E+01	-1.431027E-01	2.060489E+01	-2.515600E-15				
22	G	-2.602731E-16	-7.629489E-15	-7.426575E+01	-1.162434E-01	2.068187E+01	-1.934333E-15				
23	G	0.0	0.0	0.0	0.0	0.0	-1.462061E-16				
24	G	9.579574E-17	-2.205528E-16	-1.304640E+00	4.137257E-13	4.982256E+00	-4.744146E-16				
25	G	7.577010E-17	-7.562545E-16	-4.836426E+00	1.255042E-12	8.970780E+00	-1.159996E-15				
26	G	1.068947E-16	-2.104532E-15	-1.017065E+01	2.190421E-12	1.224473E+01	-1.410772E-15				
27	G	2.136506E-16	-2.658570E-15	-1.701966E+01	3.194220E-12	1.503499E+01	-2.576460E-15				
28	G	6.530271E-17	-3.975412E-15	-2.509360E+01	4.153128E-12	1.716072E+01	-3.349055E-15				
29	G	4.017865E-16	-6.490876E-15	-3.408485E+01	5.109411E-12	1.871469E+01	-3.234585E-15				
30	G	7.421371E-17	-9.740674E-15	-4.371526E+01	5.919765E-12	1.973188E+01	-1.420714E-15				
31	G	2.606822E-16	-8.591735E-15	-5.374205E+01	6.782683E-12	2.031692E+01	-3.003384E-15				
32	G	2.809869E-16	-1.179285E-14	-6.397686E+01	7.635899E-12	2.058428E+01	-1.236170E-15				
33	G	-1.208140E-16	-1.247271E-14	-7.429531E+01	8.056112E-12	2.067510E+01	-2.066537E-15				
34	G	0.0	0.0	0.0	0.0	0.0	-3.561726E-16				
35	G	3.621218E-16	-4.085483E-16	-1.263801E+00	1.865870E-01	4.860682E+00	-3.678138E-16				
36	G	6.559925E-16	-7.955298E-16	-4.701082E+00	5.743318E-01	8.765023E+00	-1.409231E-15				
37	G	1.083153E-15	-2.038945E-15	-9.996819E+00	7.007096E-01	1.228685E+01	-1.863387E-15				
38	G	8.744897E-16	-3.104541E-15	-1.686138E+01	6.388398E-01	1.505788E+01	-2.552158E-15				
39	G	1.332937E-15	-4.874745E-15	-2.495921E+01	5.380088E-01	1.722623E+01	-3.511278E-15				
40	G	7.735295E-16	-5.145106E-15	-3.398207E+01	4.108650E-01	1.877065E+01	-2.618612E-15				
41	G	9.920307E-16	-7.457224E-15	-4.364096E+01	2.955683E-01	1.978425E+01	-3.621345E-15				
42	G	9.650012E-16	-1.396022E-14	-5.369084E+01	2.025815E-01	2.035270E+01	-2.094507E-15				
43	G	1.753142E-15	-9.154671E-15	-6.394039E+01	1.431027E-01	2.060489E+01	-9.017031E-16				
44	G	9.631351E-16	-1.074976E-14	-7.426575E+01	1.162434E-01	2.068187E+01	-6.017072E-15				
45	G	0.0	0.0	0.0	0.0	0.0	-4.908038E-16				
46	G	8.365107E-16	-4.007768E-16	-9.732725E-01	1.099511E+00	4.003941E+00	-9.484552E-16				
47	G	1.686705E-15	-6.674223E-16	-4.168619E+00	1.599071E+00	8.686669E+00	-1.941661E-15				
48	G	2.653727E-15	-2.462040E-15	-9.445514E+00	1.530855E+00	1.230146E+01	-2.034165E-15				
49	G	2.882346E-15	-2.249532E-15	-1.636256E+01	1.365152E+00	1.522518E+01	-2.236856E-15				
50	G	1.735332E-15	-3.983470E-15	-2.455516E+01	1.080930E+00	1.740494E+01	-2.972010E-15				



# **WORKSHOP 2**

## **NORMAL MODES WITH PRELOAD**



- **Workshop Objectives**

- For a simply supported beam with no pre-load, use SOL 103 to find the first bending frequency.
- Add a preload to the beam, then use SOL 103 to once again find the first bending frequency.

- **Software Version**

- MSC Nastran 2013

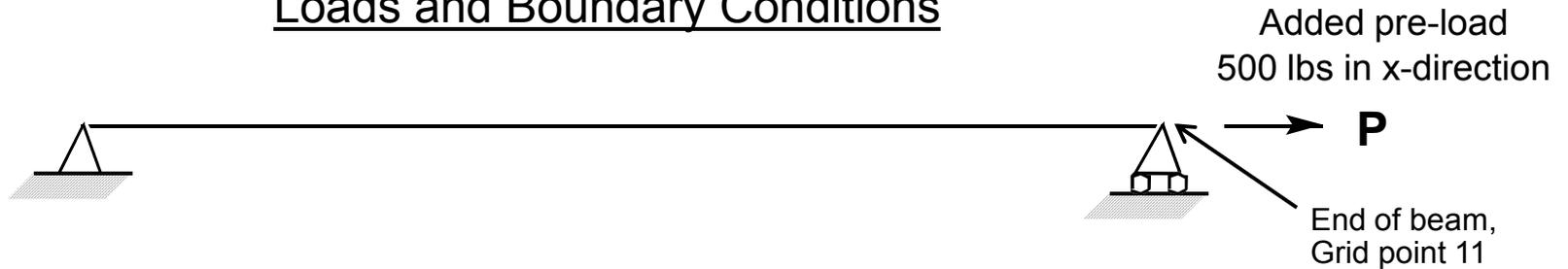
- **Files Required**

- wkshp2.dat

- **Problem Description**

- The next page contains information on the beam, including the cross-section of the beam with its dimensions, the loads and boundary conditions, and the structural parameters necessary to construct the input file.

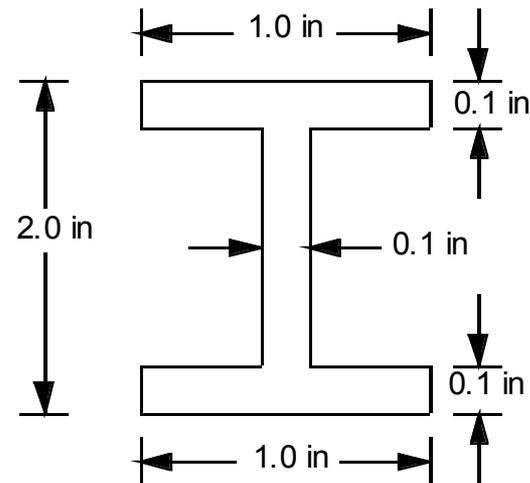
## Loads and Boundary Conditions



## Structural Information

<b>Length:</b>	<b>100 in</b>
<b>Height:</b>	<b>2 in</b>
<b>Width:</b>	<b>1 in</b>
<b>Thickness:</b>	<b>0.100 in</b>
<b>Area:</b>	<b>0.38 in<sup>2</sup></b>
<b><math>I_1</math>:</b>	<b>0.229 in<sup>4</sup></b>
<b><math>I_2</math>:</b>	<b>0.017 in<sup>4</sup></b>

## Cross-section of beam



- **Suggested Steps**

1. Open and Review the starting input file, wkshp2.dat.
2. Run the input file in MSC Nastran.
3. Review the MSC Nastran results for beam with no pre-load.
4. Modify the wkshp2.dat file to add the pre-load and re-run the file in MSC Nastran.
5. Review the MSC Nastran results using the soln2.f06 file for beam with pre-load of 500 lbs.

# Step 1. Open and Review the wkshp2.dat File

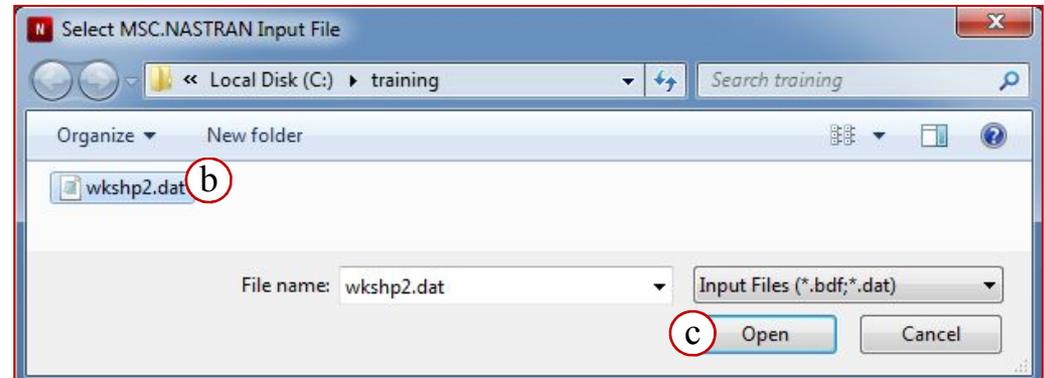
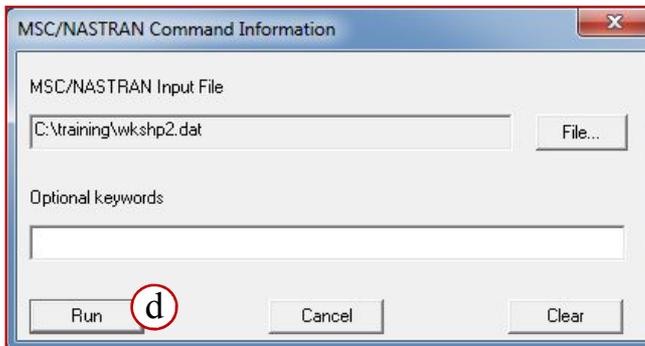
The file wkshp2.dat is the baseline model without a pre-load

```
$
$ wkshp2.dat
$
SOL 103
CEND
TITLE = NORMAL MODES EXAMPLE (NO PRE-LOAD)
$
SPC = 1
VECTOR=ALL
$
SUBCASE 1
METHOD = 1
$
BEGIN BULK
CBAR 1 1 1 2 0. 1. 0.
CBAR 2 1 2 3 0. 1. 0.
CBAR 3 1 3 4 0. 1. 0.
CBAR 4 1 4 5 0. 1. 0.
CBAR 5 1 5 6 0. 1. 0.
CBAR 6 1 6 7 0. 1. 0.
CBAR 7 1 7 8 0. 1. 0.
CBAR 8 1 8 9 0. 1. 0.
CBAR 9 1 9 10 0. 1. 0.
CBAR 10 1 10 11 0. 1. 0.
EIGRL 1 3 0
GRID 1 0. 0. 0. 345
GRID 2 10. 0. 0. 345
GRID 3 20. 0. 0. 345
GRID 4 30. 0. 0. 345
GRID 5 39.9999 0. 0. 345
GRID 6 49.9999 0. 0. 345
GRID 7 60. 0. 0. 345
GRID 8 70. 0. 0. 345
GRID 9 80. 0. 0. 345
GRID 10 90. 0. 0. 345
GRID 11 100. 0. 0. 345
MAT1 1 1.+7 .3 .101
PARAM COUPMASS1
PARAM WTMASS .00259
PBARL 1 1 I + A
+ A2. 1. 1. .1 .1 .1
SPC1 1 1234 1
SPC1 1 234 11
ENDDATA
```

# Step 2. Run the File wkshp2.dat in MSC Nastran

Run the wkshp2.dat file in MSC Nastran.

- a. Double click the **MSC Nastran** desktop icon to open Nastran.
- b. Navigate to the correct directory and select the file **wkshp2.dat**.
- c. Click **Open**.
- d. Click **Run**.



# Step 3. Review Results for wkshp2.dat Input File

## Eigenvalue Results for Beam with No Pre-Load

```

E I G E N V A L U E   A N A L Y S I S   S U M M A R Y   (R E A D   M O D U L E)

      BLOCK SIZE USED ..... 6
      NUMBER OF DECOMPOSITIONS ..... 2
      NUMBER OF ROOTS FOUND ..... 3
      NUMBER OF SOLVES REQUIRED ..... 4

1  NORMAL MODES EXAMPLE
0
                                           PAGE      8
                                           SUBCASE 1

MODE NO.  EXTRACTION ORDER  EIGENVALUE  REAL EIGENVALUES
              RADIANS      CYCLES      GENERALIZED MASS      GENERALIZED STIFFNESS
1             1             2.239525E+04  1.496504E+02  2.381760E+01  1.000000E+00  2.239525E+04
2             2             3.550680E+05  5.958759E+02  9.483659E+01  1.000000E+00  3.550680E+05
3             3             1.772663E+06  1.331414E+03  2.119011E+02  1.000000E+00  1.772663E+06

```

# Step 4. Modify the wkshp2.dat File to Add Preload

Use wkshp2.dat as a starting point and modify the file to add the pre-load of 500 lbs at the end of the beam.

- Change the name of file to **soln2.dat**.
- Change the portion of the TITLE that is in parenthesis to **(WITH PRE-LOAD)**
- In Case Control, add the two necessary subcases when using a pre-load.
- In Bulk Data, add the pre-load of **500 lbs** in the **x-direction** at the end of the beam, **GRID 11**.
- Save the modified file as **soln2.dat**.
- Run the new file, **soln2.dat**, in MSC Nastran, (to review this process, see step 2, page 7)

```
$
$ soln2.dat
$
SOL 103
CEND
TITLE = NORMAL MODES EXAMPLE (WITH PRE-LOAD)
$
SPC = 1
VECTOR=ALL
$
SUBCASE 1
LOAD = 2
$
SUBCASE 2
METHOD = 1
STATSUB = 1
$
BEGIN BULK
CBAR 1 1 1 2 0. 1. 0.
CBAR 2 1 2 3 0. 1. 0.
CBAR 3 1 3 4 0. 1. 0.
CBAR 4 1 4 5 0. 1. 0.
CBAR 5 1 5 6 0. 1. 0.
CBAR 6 1 6 7 0. 1. 0.
CBAR 7 1 7 8 0. 1. 0.
CBAR 8 1 8 9 0. 1. 0.
CBAR 9 1 9 10 0. 1. 0.
CBAR 10 1 10 11 0. 1. 0.
EIGRL 1 3 0
GRID 1 0. 0. 0. 345
GRID 2 10. 0. 0. 345
GRID 3 20. 0. 0. 345
GRID 4 30. 0. 0. 345
GRID 5 39.9999 0. 0. 345
GRID 6 49.9999 0. 0. 345
GRID 7 60. 0. 0. 345
GRID 8 70. 0. 0. 345
GRID 9 80. 0. 0. 345
GRID 10 90. 0. 0. 345
GRID 11 100. 0. 0. 345
MAT1 1 1.+7 .3 .101
PARAM COUPMASS1
PARAM WTMASS .00259
PBARL 1 1 I + A
+ A2. 1. 1. .1 .1 .1
SPC1 1 1234 1
SPC1 1 234 11
$
LOAD 2 1. 1. 1
FORCE 1 11 0 500. 1. 0. 0.
ENDDATA
```

# Step 5. Review Results for soln2.dat Input File

## Eigenvalue Results for Beam with Pre-Load

```

                                E I G E N V A L U E   A N A L Y S I S   S U M M A R Y   (READ MODULE)

                                BLOCK SIZE USED ..... 6
                                NUMBER OF DECOMPOSITIONS ..... 2
                                NUMBER OF ROOTS FOUND ..... 3
                                NUMBER OF SOLVES REQUIRED ..... 4

1  NORMAL MODES EXAMPLE (WITH PRE-LOAD)
0
                                PAGE 11
                                SUBCASE 2

                                R E A L   E I G E N V A L U E S
                                R A D I A N S           C Y C L E S

MODE NO.  EXTRACTION ORDER  EIGENVALUE          REAL EIGENVALUES
                                GENERALIZED          GENERALIZED
                                MASS                 STIFFNESS
1           1                2.735964E+04      1.654075E+02      2.632542E+01      1.000000E+00      2.735964E+04
2           2                3.749264E+05      6.123123E+02      9.745253E+01      1.000000E+00      3.749264E+05
3           3                1.817354E+06      1.348093E+03      2.145556E+02      1.000000E+00      1.817354E+06

```

# **WORKSHOP 3**

# **NORMAL MODES ANALYSIS USING GUYAN**

# **REDUCTION**



- **Workshop Objectives**

- Use Guyan Reduction to reduce the model used in Workshop 1.
- After the reduction is complete, using the Lanczos method, find the first five natural frequencies and mode shapes of the plate.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

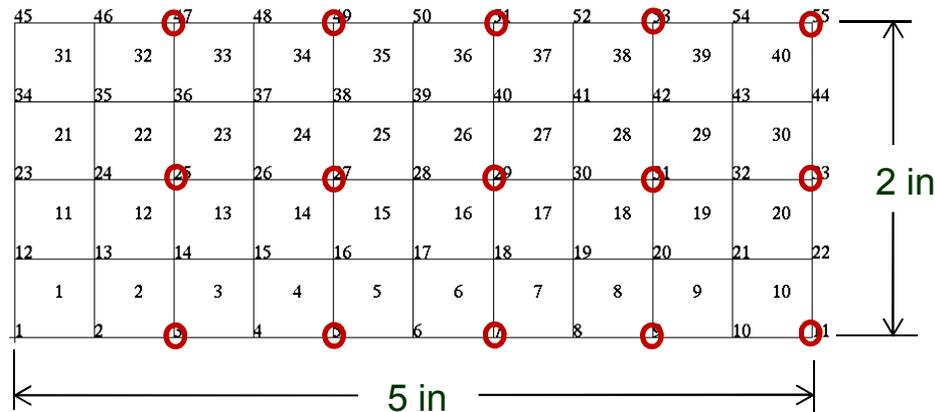
- plate.bdf
- wkshp3.dat

- **Problem Description:**

- The plate has the same structural data and boundary condition from workshop 1, shown on page 5 for your convenience.

- **Problem Description Continued.**
  - For the Guyan reduction, use the points indicated in figure below.

### Guyan Reduction Points



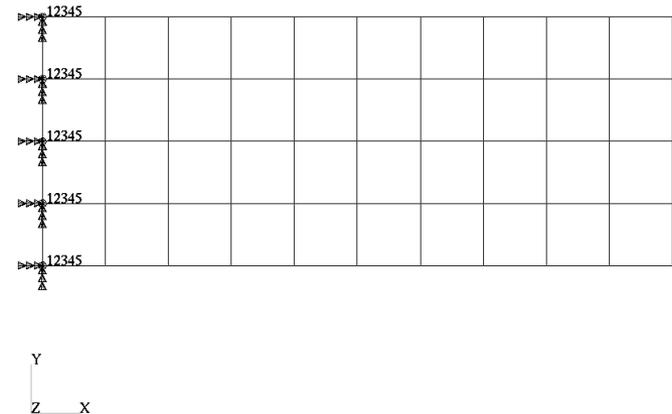
- **Problem Description Continued.**

### Structural Information

Table 3A.

Length (a)	5 in
Height (b)	2 in
Thickness	0.100 in
Weight Density	0.282 lbs/in <sup>3</sup>
Mass/Weight Factor	2.59E-3 sec <sup>2</sup> /in
Elastic Modulus	30.0E6 lbs/in <sup>2</sup>
Poisson's Ratio	0.3

### Boundary Condition



- **Suggested Steps**

1. Open and review the wkshp3.dat file.
2. Modify this input file to add Guyan Reduction.
3. Run the new input file in MSC Nastran.
4. Review the MSC Nastran results using the solution file soln3.f06.
5. Compare results of this workshop with workshop 1.

# Step 1. Open and Review the wkshp3.dat File

The workshp3.dat is the partial input file to be modified.

```
$
$   wkshp3.dat
$
SOL 103
CEND
TITLE = REDUCTION PROCEDURES, NORMAL MODES EXAMPLE
SUBTITLE = USING STATIC REDUCTION
ECHO = UNSORTED
SUBCASE 1
  SUBTITLE=USING LANCZOS
  METHOD = 1
  SPC = 1
  VECTOR=ALL
BEGIN BULK
PARAM,POST, 0
EIGR,1,AHOU,,,,5
PARAM,COUPMASS, 1
PARAM,WTMASS, 0.00259
INCLUDE 'plate.bdf'
$
$ SELECT A-SET, STATIC REDUCTION IS DONE AUTOMATICALLY
$
ENDDATA
```

# Step 2. Modify Input File to Add Guyan Reduction

Start with the input file `wkshp3.dat` and add the request for Guyan reduction.

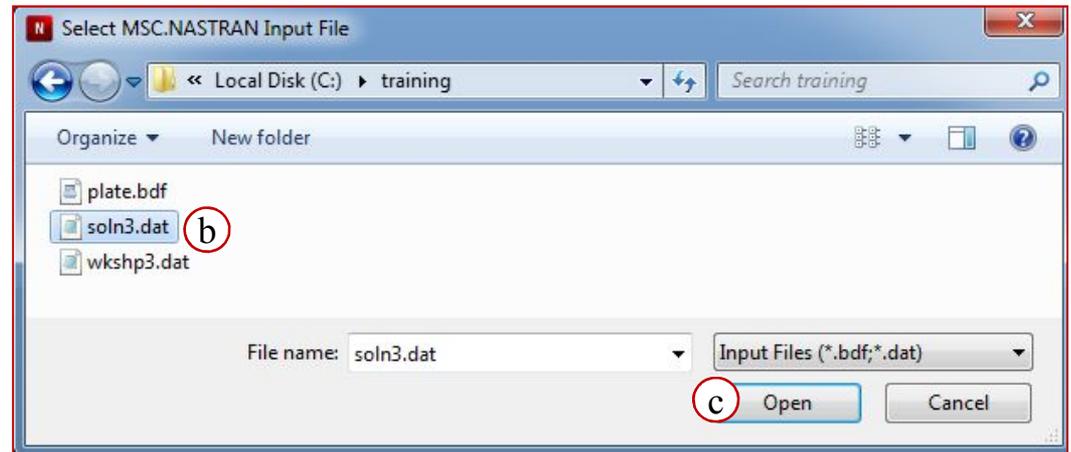
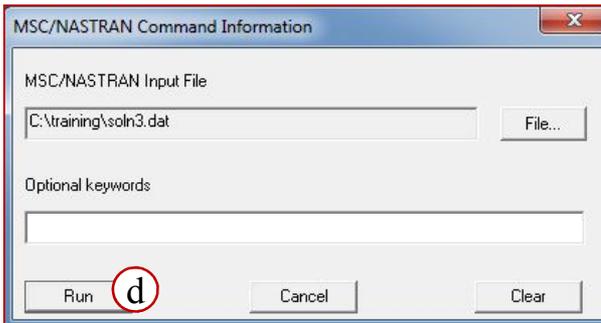
- a. Change the file name to **`soln3.dat`**.
- b. Change the **EIGR** entry to use the Lanczos method.
- c. Add the **ASET1** entry using the points shown on page WS3-4.
- d. Save the modified file as **`soln3.dat`**.

```
$
$  soln3.dat  a
$
SOL 103
CEND
TITLE = REDUCTION PROCEDURES, NORMAL MODES EXAMPLE
SUBTITLE = USING STATIC REDUCTION
ECHO = UNSORTED
SUBCASE 1
  SUBTITLE=USING LANCZOS
  METHOD = 1
  SPC = 1
  VECTOR=ALL
BEGIN BULK
PARAM, POST, 0
  b EIGR, 1, LAN, , , , 5
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
INCLUDE 'plate.bdf'
$
$ SELECT A-SET, STATIC REDUCTION IS DONE AUTOMATICALLY
$
  c ASET1, 345, 3, 5, 7, 9, 11
  ASET1, 345, 25, 27, 29, 31, 33
  ASET1, 345, 47, 49, 51, 53, 55
ENDDATA
```

# Step 3. Run the New Input File, soln3.dat

Run the soln3.dat file in MSC Nastran.

- a. Double click the **MSC Nastran** desktop icon to open Nastran.
- b. Navigate to the correct directory and select the file **soln3.dat**.
- c. Click **Open**.
- d. Click **Run**.



# Step 4. Review Results of Input File, soln3.dat

```

E I G E N V A L U E   A N A L Y S I S   S U M M A R Y   ( R E A D   M O D U L E )

                                BLOCK SIZE USED ..... 7
                                NUMBER OF DECOMPOSITIONS ..... 2
                                NUMBER OF ROOTS FOUND ..... 5
                                NUMBER OF SOLVES REQUIRED ..... 5

1  REDUCTION PROCEDURES, NORMAL MODES EXAMPLE                                PAGE 10
0  USING STATIC REDUCTION                                                    SUBCASE 1

MODE   EXTRACTION   EIGENVALUE   REAL EIGENVALUES
NO.    ORDER          RADIANS     CYCLES
1      1             7.056352E+05 8.400210E+02 1.336935E+02
2      2             1.879631E+07 4.335472E+03 6.900117E+02
3      3             2.817725E+07 5.308225E+03 8.448301E+02
4      4             1.953805E+08 1.397786E+04 2.224645E+03
5      5             2.367517E+08 1.538674E+04 2.448875E+03
1  REDUCTION PROCEDURES, NORMAL MODES EXAMPLE                                PAGE 11
0  USING LANCZOS                                                            SUBCASE 1

EIGENVALUE = 7.056352E+05
CYCLES = 1.336935E+02
REAL EIGENVECTOR NO. 1

POINT ID.  TYPE   T1      T2      T3      R1      R2      R3
1          G     0.0     0.0     0.0     0.0     0.0     0.0
2          G     0.0     0.0    -9.732642E-01 -1.099629E+00 4.004109E+00 0.0
3          G     0.0     0.0    -4.168889E+00 -1.599175E+00 8.687232E+00 0.0
4          G     0.0     0.0    -9.445539E+00 -1.529646E+00 1.230197E+01 0.0
5          G     0.0     0.0    -1.636362E+01 -1.365241E+00 1.522617E+01 0.0
6          G     0.0     0.0    -2.455527E+01 -1.077562E+00 1.740565E+01 0.0
7          G     0.0     0.0    -3.367999E+01 -8.040918E-01 1.895542E+01 0.0
8          G     0.0     0.0    -4.342918E+01 -5.415159E-01 1.993802E+01 0.0
9          G     0.0     0.0    -5.355521E+01 -3.472537E-01 2.046666E+01 0.0
10         G     0.0     0.0    -6.384790E+01 -2.065355E-01 2.066393E+01 0.0

```

To see the entire list of results, use the soln3.f06 file

# Step 5. Compare Results

Compare the results after the Guyan Reduction with workshop 1.

## Eigenvalue results from workshop 1

MODE NO.	EXTRACTION ORDER	EIGENVALUE	R E A L E I G E N V A L U E S		GENERALIZED MASS	GENERALIZED STIFFNESS
			RADIANS	CYCLES		
1	1	7.055894E+05	8.399937E+02	1.336891E+02	1.000000E+00	7.055894E+05
2	2	1.877186E+07	4.332651E+03	6.895628E+02	1.000000E+00	1.877186E+07
3	3	2.811177E+07	5.302053E+03	8.438480E+02	1.000000E+00	2.811177E+07
4	4	1.929422E+08	1.389036E+04	2.210720E+03	1.000000E+00	1.929422E+08
5	5	2.221657E+08	1.490523E+04	2.372240E+03	1.000000E+00	2.221657E+08
6	6	2.328451E+08	1.525926E+04	2.428587E+03	1.000000E+00	2.328451E+08
7	7	6.832397E+08	2.613885E+04	4.160127E+03	1.000000E+00	6.832397E+08
8	8	9.600053E+08	3.098395E+04	4.931249E+03	1.000000E+00	9.600053E+08
9	9	1.365293E+09	3.694987E+04	5.880754E+03	1.000000E+00	1.365293E+09
10	10	1.850317E+09	4.301531E+04	6.846099E+03	1.000000E+00	1.850317E+09

## Eigenvalue results from workshop 3

MODE NO.	EXTRACTION ORDER	EIGENVALUE	R E A L E I G E N V A L U E S		GENERALIZED MASS	GENERALIZED STIFFNESS
			RADIANS	CYCLES		
1	1	7.056352E+05	8.400210E+02	1.336935E+02	1.000000E+00	7.056352E+05
2	2	1.879631E+07	4.335472E+03	6.900117E+02	1.000000E+00	1.879631E+07
3	3	2.817725E+07	5.308225E+03	8.448301E+02	1.000000E+00	2.817725E+07
4	4	1.953805E+08	1.397786E+04	2.224645E+03	1.000000E+00	1.953805E+08
5	5	2.367517E+08	1.538674E+04	2.448875E+03	1.000000E+00	2.367517E+08



# **WORKSHOP 4**

## **DIRECT TRANSIENT RESPONSE**



- **Workshop Objectives**

- Using the direct method, determine the transient response of the flat rectangular plate (from Workshop 1) subject to time-varying excitation as described below.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

- plate.bdf
- wkshp4.dat

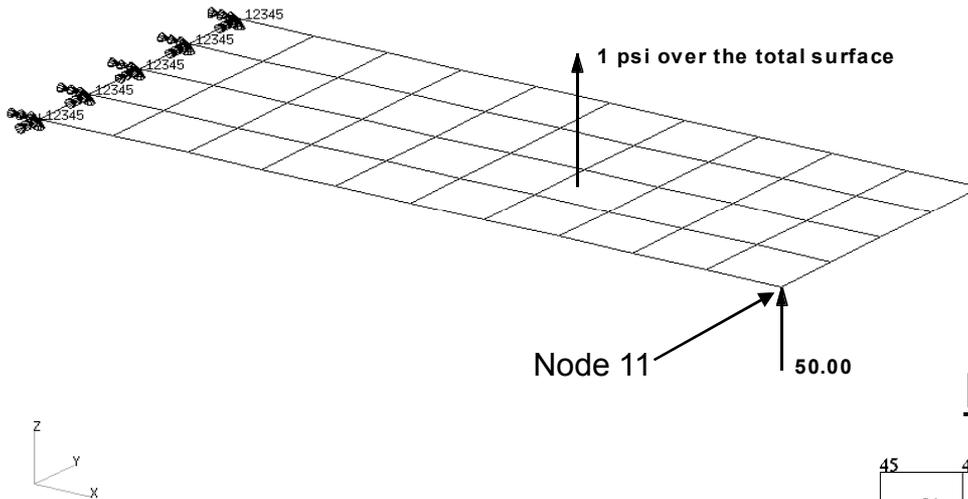
- **Problem Description**

- The structure is excited by 1 psi pressure load over the total surface of the plate varying at 250 Hz. In addition, a 50 lb force is applied at a corner of the tip also varying at 250 Hz, but 180° out-of-phase with the pressure load. Both time dependent dynamic loads are applied for the duration of 0.008 seconds only. Use structural damping of  $g=0.06$  and convert this damping to equivalent viscous damping at 250 Hz. Carry the analysis for 0.04 seconds.

- **Problem Description Continued**

- The diagrams below show the finite element representation of the flat plate and the loads and boundary condition.

### Loads and Boundary Condition



### Elements and Grid Coordinates

45	46	47	48	49	50	51	52	53	54	55
31	32	33	34	35	36	37	38	39	40	44
34	35	36	37	38	39	40	41	42	43	44
21	22	23	24	25	26	27	28	29	30	33
23	24	25	26	27	28	29	30	31	32	33
11	12	13	14	15	16	17	18	19	20	22
12	13	14	15	16	17	18	19	20	21	22
1	2	3	4	5	6	7	8	9	10	11
1	2	3	4	5	6	7	8	9	10	11

TIP  
↓

- **Suggested Steps**

1. Open and review the input file wkshp4.dat.
2. Add structural damping and convert to viscous damping.
3. Add the time dependent pressure load.
4. Add the time dependent point load.
5. Add the combined loads
6. Add the integration step.
7. Save and run the new input file in MSC Nastran.
8. Review the MSC Nastran results using the solution file soln4.f06
9. Convert results to graph.
10. View the graph results.

# Step 1. Open and Review the Input File wkshp4.dat

The file wkshp4.dat is the starting input file to be modified.

To complete input file add these entries

```
$
$ wkshp4.dat
$
$   add :   structural damping
$         loading
$         integration time step
$
SOL 109
CEND
TITLE= TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE= USE THE DIRECT METHOD
ECHO= PUNCH
SPC= 1
SET 1= 11, 33, 55
DISPLACEMENT= 1
SUBCASE 1
DLOAD= 700 $ SELECT TEMPORAL COMPONENT OF TRANSIENT LOADING
TSTEP= 100 $ SELECT INTEGRATION TIME STEPS
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT CENTER TIP
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
ENDDATA
```

Output displacement response graphs at grid points 11, 33,55

# Step 2. Add Structural Damping and Convert to Viscous Damping

Add the appropriate parameters in the Bulk Data section for damping.

- a. First rename the input file as **soln4.dat**.
- b. For structural damping, use **PARAM G** with a value of **.06**.
- c. To convert to viscous damping, use **PARAM W3**, for the value of this parameter, convert 250 Hz to radians/sec

```
$
$   soln4.dat a
$
SOL 109
CEND
TITLE= TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE= USE THE DIRECT METHOD
ECHO= PUNCH
SPC= 1
SET 1= 11, 33, 55
DISPLACEMENT= all
SUBCASE 1
DLOAD= 700 $ SELECT TEMPORAL COMPONENT OF TRANSIENT LOADING
TSTEP= 100 $ SELECT INTEGRATION TIME STEPS
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT CENTER TIP
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY DAMPING
$
b PARAM, G, 0.06
$
c PARAM, W3, 1571.
$
ENDDATA
```

# Step 3. Add Time Dependent Pressure Load

Add the time dependent pressure load of 1 psi over the entire plate varying at 250 HZ.

- a. Use a **TLOAD2** entry in combination with a **PLOAD2** and the given information on page WS4-3 to obtain:
  - Time = from 0 to .008 sec
  - Frequency = 250 HZ
  - Phase angle =  $-90^\circ$
- b. For the **PLOAD** entry, apply the pressure of 1 psi over all the elements of the plate. (1 through 40)

```
$
$   soln4.dat
$
SOL 109
CEND
TITLE= TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE= USE THE DIRECT METHOD
ECHO= PUNCH
SPC= 1
SET 1= 11, 33, 55
DISPLACEMENT= all
SUBCASE 1
DLOAD= 700 $ SELECT TEMPORAL COMPONENT OF TRANSIENT LOADING
TSTEP= 100 $ SELECT INTEGRATION TIME STEPS
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT CENTER TIP
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY DAMPING
$
PARAM, G, 0.06
$
PARAM, W3, 1571.
$
$ TIME VARYING PRESSURE LOAD (250 HZ)
$
a TLOAD2, 200, 400, , 0, 0., 8.E-3, 250., -90.
$
b PLOAD2, 400, 1., 1, THRU, 40
$
ENDDATA
```

# Step 4. Add Time Dependent Point Load

Add the time dependent point load at the corner of the tip of the plate (grid point 11) , also varying at 250 Hz but 180° out-of-phase with the pressure load.

- a. Use the **TLOAD2** entry in combination with a **DAREA** entry and the above information.
  - Time = **0 to .008 sec**
  - Frequency = **250 HZ**
  - Phase angle = **90°**
- b. For the **DAREA** entry, note that the **50 lb** force is applied at grid **11** in the **Z** direction.

```
$
$   soln4.dat
$
SOL 109
CEND
TITLE= TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE= USE THE DIRECT METHOD
ECHO= PUNCH
SPC= 1
SET 1= 11, 33, 55
DISPLACEMENT= all
SUBCASE 1
DLOAD= 700 $ SELECT TEMPORAL COMPONENT OF TRANSIENT LOADING
TSTEP= 100 $ SELECT INTEGRATION TIME STEPS
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT CENTER TIP
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY DAMPING
$
PARAM, G, 0.06
$
PARAM, W3, 1571.
$
$ TIME VARYING PRESSURE LOAD (250 HZ)
$
TLOAD2, 200, 400, , 0, 0., 8.E-3, 250., -90.
$
PLOAD2, 400, 1., 1, THRU, 40
$
$ APPLY POINT LOAD OUT OF PHASE WITH PRESSURE LOAD
$
a TLOAD2, 500, 600, , 0, 0., 8.E-3, 250., 90.
$
b DAREA, 600, 11, 3, 50.
$
ENDDATA
```

# Step 5. Add the Combined Loads

Combine the pressure and point loads using a DLOAD entry.

- a. For the **DLOAD** entry, define the scale as **1.** for both loads.
- b. Make sure the **DLOAD** Case Control identification matches the SID for the **DLOAD** entry in the Bulk Data section.

```
$
$   soln4.dat
$
SOL 109
CEND
TITLE= TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE= USE THE DIRECT METHOD
ECHO= PUNCH
SPC= 1
SET 1= 11, 33, 55
DISPLACEMENT= all
SUBCASE 1
DLOAD= 700 $ b SELECT TEMPORAL COMPONENT OF TRANSIENT LOADING
TSTEP= 100 $ SELECT INTEGRATION TIME STEPS
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT CENTER TIP
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY DAMPING
$
PARAM, G, 0.06
$
PARAM, W3, 1571.
$
$ TIME VARYING PRESSURE LOAD (250 HZ)
$
TLOAD2, 200, 400, , 0, 0., 8.E-3, 250., -90.
$
PLOAD2, 400, 1., 1, THRU, 40
$
$ APPLY POINT LOAD OUT OF PHASE WITH PRESSURE LOAD
$
TLOAD2, 500, 600, , 0, 0., 8.E-3, 250., 90.
$
DAREA, 600, 11, 3, 50.
$
$ COMBINE LOADS
$
DLOAD, 700, 1., 1., 200, 1., 500
$
ENDDATA
```

# Step 6. Add the Integration Time Step

To add the Time step:

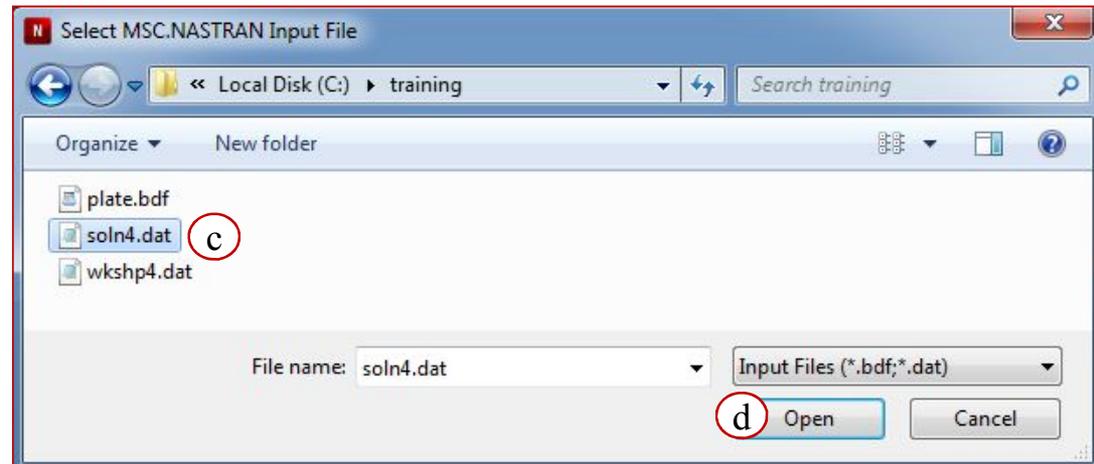
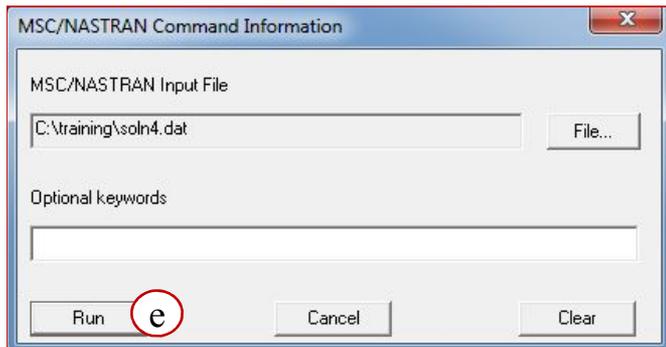
- a. For the **TSTEP** entry, use **100** steps and a time increment of **.0004** seconds, so that the total time will be **.04** seconds.
- b. Make sure that the **TSTEP** Case Control command identification matches the SID for the **TSTEP** entry in the Bulk Data section.

```
$
$   soln4.dat
$
SOL 109
CEND
TITLE= TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE= USE THE DIRECT METHOD
ECHO= PUNCH
SPC= 1
SET 1= 11, 33, 55
DISPLACEMENT= all
SUBCASE 1
$
DLOAD= 700 $ SELECT TEMPORAL COMPONENT OF TRANSIENT LOADING
TSTEP= 100 $ SELECT INTEGRATION TIME STEPS
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT CENTER TIP
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY DAMPING
$
PARAM, G, 0.06
$
PARAM, W3, 1571.
$
$ TIME VARYING PRESSURE LOAD (250 HZ)
$
TLOAD2, 200, 400, , 0, 0., 8.E-3, 250., -90.
$
PLOAD2, 400, 1., 1, THRU, 40
$
$ APPLY POINT LOAD OUT OF PHASE WITH PRESSURE LOAD
$
TLOAD2, 500, 600, , 0, 0., 8.E-3, 250., 90.
$
DAREA, 600, 11, 3, 50.
$
$ COMBINE LOADS
$
DLOAD, 700, 1., 1., 200, 1., 500
$
$ SPECIFY INTERGRATION TIME STEPS
$
TSTEP, 100, 100, 4.0E-4, 1
$
ENDDATA
```

# Step 7. Save and Run the New Input File

Save and run the modified file in Nastran.

- a. Save the modified file as **soln4.dat**.
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln4.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 8. Review the Results

To see the results open the soln4.f06 file. The three grid points of interest lie along the tip of the plate, grid points 11, 33, 55.

Elements and Grid Coordinates

45	46	47	48	49	50	51	52	53	54	55
31	32	33	34	35	36	37	38	39	40	
34	35	36	37	38	39	40	41	42	43	44
21	22	23	24	25	26	27	28	29	30	
23	24	25	26	27	28	29	30	31	32	33
11	12	13	14	15	16	17	18	19	20	
12	13	14	15	16	17	18	19	20	21	22
1	2	3	4	5	6	7	8	9	10	
1	2	3	4	5	6	7	8	9	10	11

TIP  
↓

POINT-ID = 55

DISPLACEMENT VECTOR

TIME	TYPE	T1	T2	T3	R1	R2	R3
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0
4.000000E-04	G	0.0	0.0	-2.850083E-03	7.786633E-03	4.615276E-03	0.0
8.000000E-04	G	0.0	0.0	-1.992840E-02	2.321643E-02	1.681915E-02	0.0
1.200000E-03	G	0.0	0.0	-6.642522E-02	3.539676E-02	3.502940E-02	0.0
1.600000E-03	G	0.0	0.0	-1.471612E-01	2.773868E-02	5.294653E-02	0.0
2.000000E-03	G	0.0	0.0	-2.423338E-01	2.135641E-03	6.749530E-02	0.0
2.400000E-03	G	0.0	0.0	-3.115154E-01	-2.225372E-02	7.683348E-02	0.0
2.800000E-03	G	0.0	0.0	-3.166115E-01	-3.073159E-02	7.507210E-02	0.0
3.200000E-03	G	0.0	0.0	-2.453424E-01	-2.541673E-02	5.638634E-02	0.0
3.600000E-03	G	0.0	0.0	-1.149021E-01	-1.575294E-02	2.329719E-02	0.0
4.000000E-03	G	0.0	0.0	4.357039E-02	-4.375043E-03	-1.451847E-02	0.0
4.400000E-03	G	0.0	0.0	1.974865E-01	1.144615E-02	-4.834513E-02	0.0
4.800000E-03	G	0.0	0.0	3.126070E-01	2.789536E-02	-7.316789E-02	0.0
5.200000E-03	G	0.0	0.0	3.570641E-01	3.339712E-02	-8.473742E-02	0.0
5.600000E-03	G	0.0	0.0	3.190163E-01	2.160002E-02	-7.985147E-02	0.0

POINT-ID = 33

DISPLACEMENT VECTOR

TIME	TYPE	T1	T2	T3	R1	R2	R3
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0
4.000000E-04	G	0.0	0.0	-1.122321E-02	9.220317E-03	6.136194E-03	0.0
8.000000E-04	G	0.0	0.0	-4.424644E-02	2.577100E-02	2.014592E-02	0.0
1.200000E-03	G	0.0	0.0	-1.030766E-01	3.820221E-02	3.921979E-02	0.0
1.600000E-03	G	0.0	0.0	-1.756299E-01	2.929390E-02	5.577315E-02	0.0
2.000000E-03	G	0.0	0.0	-2.443358E-01	1.775214E-03	6.761315E-02	0.0
2.400000E-03	G	0.0	0.0	-2.882814E-01	-2.449635E-02	7.435711E-02	0.0
2.800000E-03	G	0.0	0.0	-2.843486E-01	-3.428704E-02	7.112917E-02	0.0
3.200000E-03	G	0.0	0.0	-2.184738E-01	-2.883632E-02	5.265180E-02	0.0
3.600000E-03	G	0.0	0.0	-9.830756E-02	-1.773140E-02	2.099964E-02	0.0
4.000000E-03	G	0.0	0.0	4.799469E-02	-4.455216E-03	-1.487336E-02	0.0
4.400000E-03	G	0.0	0.0	1.852531E-01	1.333487E-02	-4.646942E-02	0.0
4.800000E-03	G	0.0	0.0	2.832549E-01	3.130046E-02	-6.939592E-02	0.0
5.200000E-03	G	0.0	0.0	3.220591E-01	3.711201E-02	-8.055533E-02	0.0
5.600000E-03	G	0.0	0.0	2.962765E-01	2.425858E-02	-7.710429E-02	0.0

POINT-ID = 11

DISPLACEMENT VECTOR

TIME	TYPE	T1	T2	T3	R1	R2	R3
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0
4.000000E-04	G	0.0	0.0	-2.173954E-02	1.105127E-02	1.051570E-02	0.0
8.000000E-04	G	0.0	0.0	-7.205779E-02	2.849259E-02	2.853552E-02	0.0
1.200000E-03	G	0.0	0.0	-1.433632E-01	4.084704E-02	4.916111E-02	0.0
1.600000E-03	G	0.0	0.0	-2.060064E-01	3.055025E-02	6.223300E-02	0.0
2.000000E-03	G	0.0	0.0	-2.459063E-01	1.403891E-03	6.812792E-02	0.0
2.400000E-03	G	0.0	0.0	-2.623262E-01	-2.646279E-02	6.920423E-02	0.0
2.800000E-03	G	0.0	0.0	-2.475191E-01	-3.775539E-02	6.212135E-02	0.0
3.200000E-03	G	0.0	0.0	-1.870294E-01	-3.243333E-02	4.357094E-02	0.0
3.600000E-03	G	0.0	0.0	-7.902250E-02	-1.985359E-02	1.527561E-02	0.0
4.000000E-03	G	0.0	0.0	5.249596E-02	-4.463858E-03	-1.566547E-02	0.0
4.400000E-03	G	0.0	0.0	1.704333E-01	1.542631E-02	-4.175911E-02	0.0
4.800000E-03	G	0.0	0.0	2.494407E-01	3.474316E-02	-6.052255E-02	0.0
5.200000E-03	G	0.0	0.0	2.823412E-01	4.064508E-02	-7.116906E-02	0.0
5.600000E-03	G	0.0	0.0	2.701626E-01	2.682153E-02	-7.190715E-02	0.0

# Step 9. Convert Results to Graph

After submitting the solution file in Nastran, it will create a soln4.plt file. This file need to convert to a soln4.ps that can then be read with any postscript viewer to create a graph file.

- Open a cmd window. (CMD.exe)
- Change the current directory to the one in which the **soln4.plt** file is located. (for this this example *c:\training*)
- Need to use the file **plotps.exe** in the directory  
**C:\MSC.Software\MSC\_Nastran\20130\msc20130\win64**. Check to make sure this file exists there.
- In the cmd window, type in the following.
  - C:\MSC.Software\MSC\_Nastran\20130\msc20130\win64\plotps.exe soln4.plt**
- This should have created a new file **soln4.ps**. Check to make sure that it is now in your directory.
- Open the file, it should automatically use *Acrobat Distiller* to create the **soln10a.pdf** file. This file contains the 3 graph results requested in XY Plot.

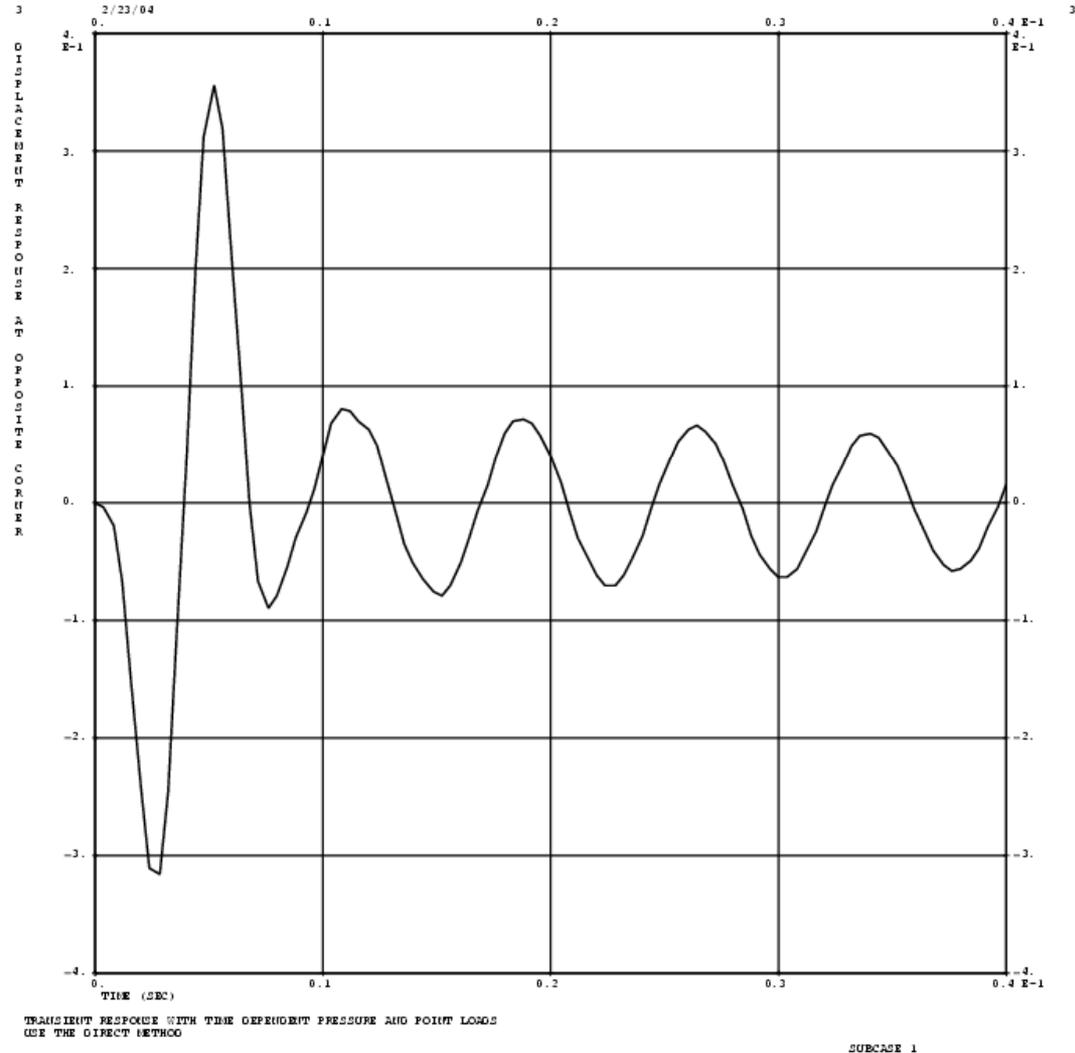
The screenshots show the following steps:

- Opening a command prompt window (CMD.exe).
- Changing the current directory to `C:\training`.
- Navigating to the directory `C:\MSC.Software\MSC_Nastran\20130\msc20130\win64` where `plotps.exe` is located.
- Running the command `C:\training>C:\MSC.Software\MSC_Nastran\20130\msc20130\win64\plotps.exe soln4.plt` in the command prompt.
- Viewing the resulting files in a file explorer, including `soln4.ps`.

Refer to the process described on this page in the following workshops to see the graph results.

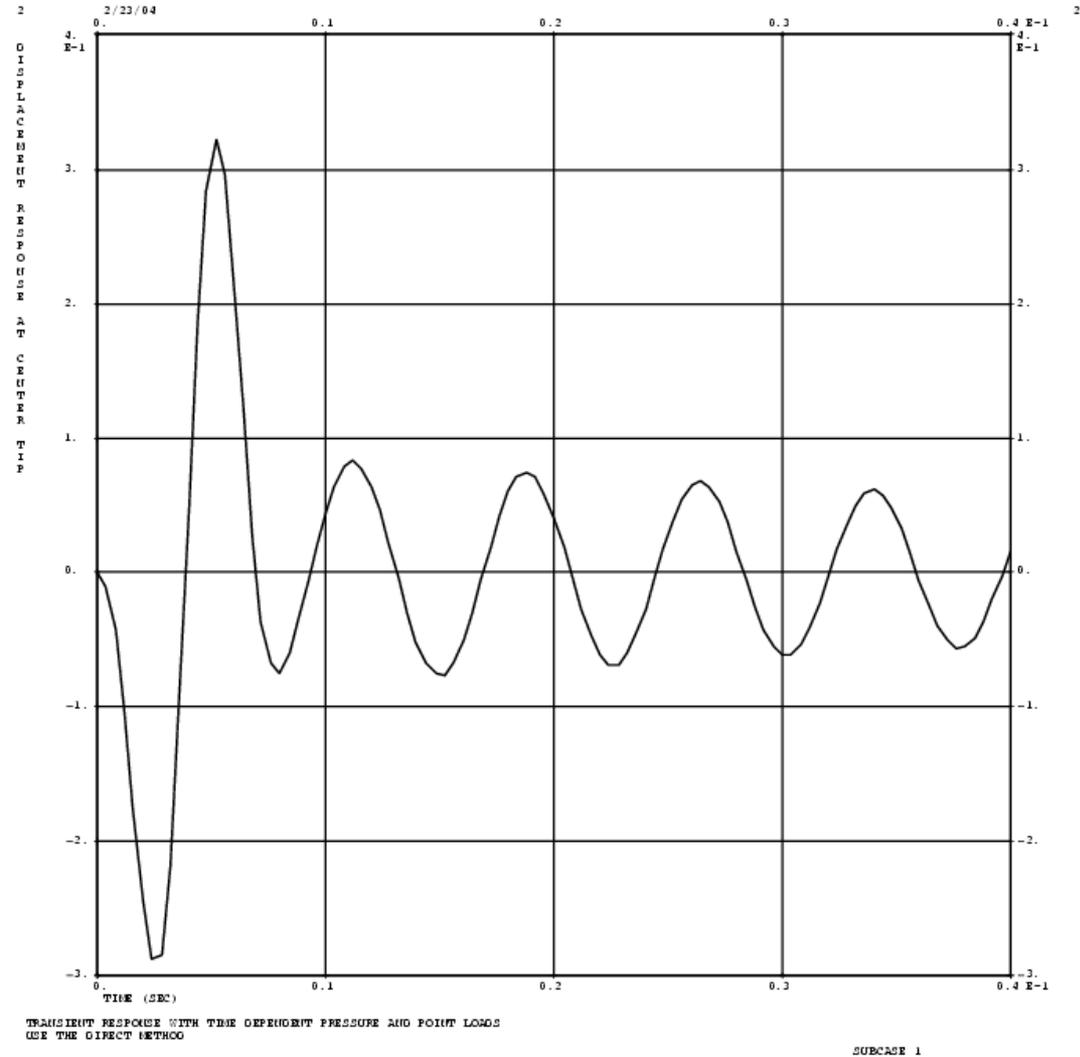
# Step 10. View the Graph Results

Review the displacement response graph at the opposite corner of the point load. (grid 55)



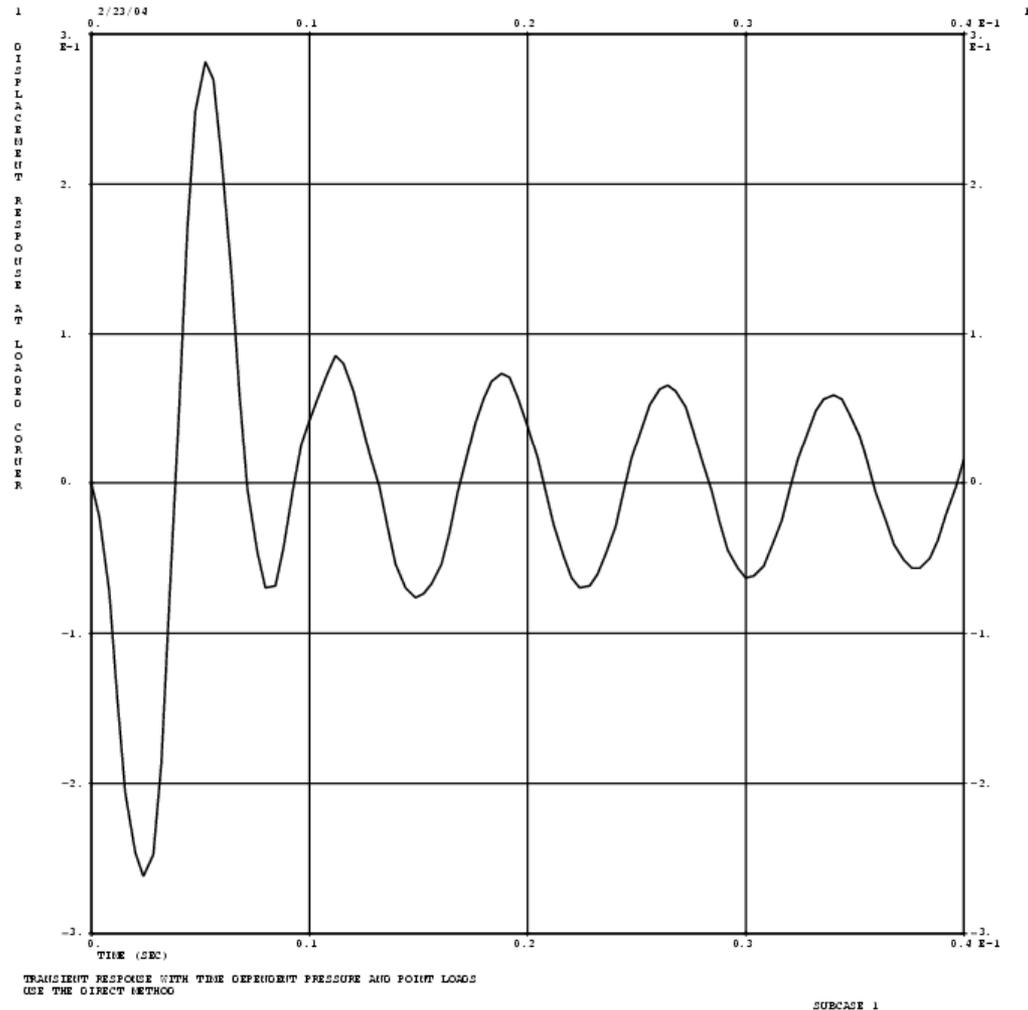
# Step 10. View the Graph Results (Cont.)

Review the displacement response graph at the center of the tip (grid 33)



# Step 10. View the Graph Results (Cont.)

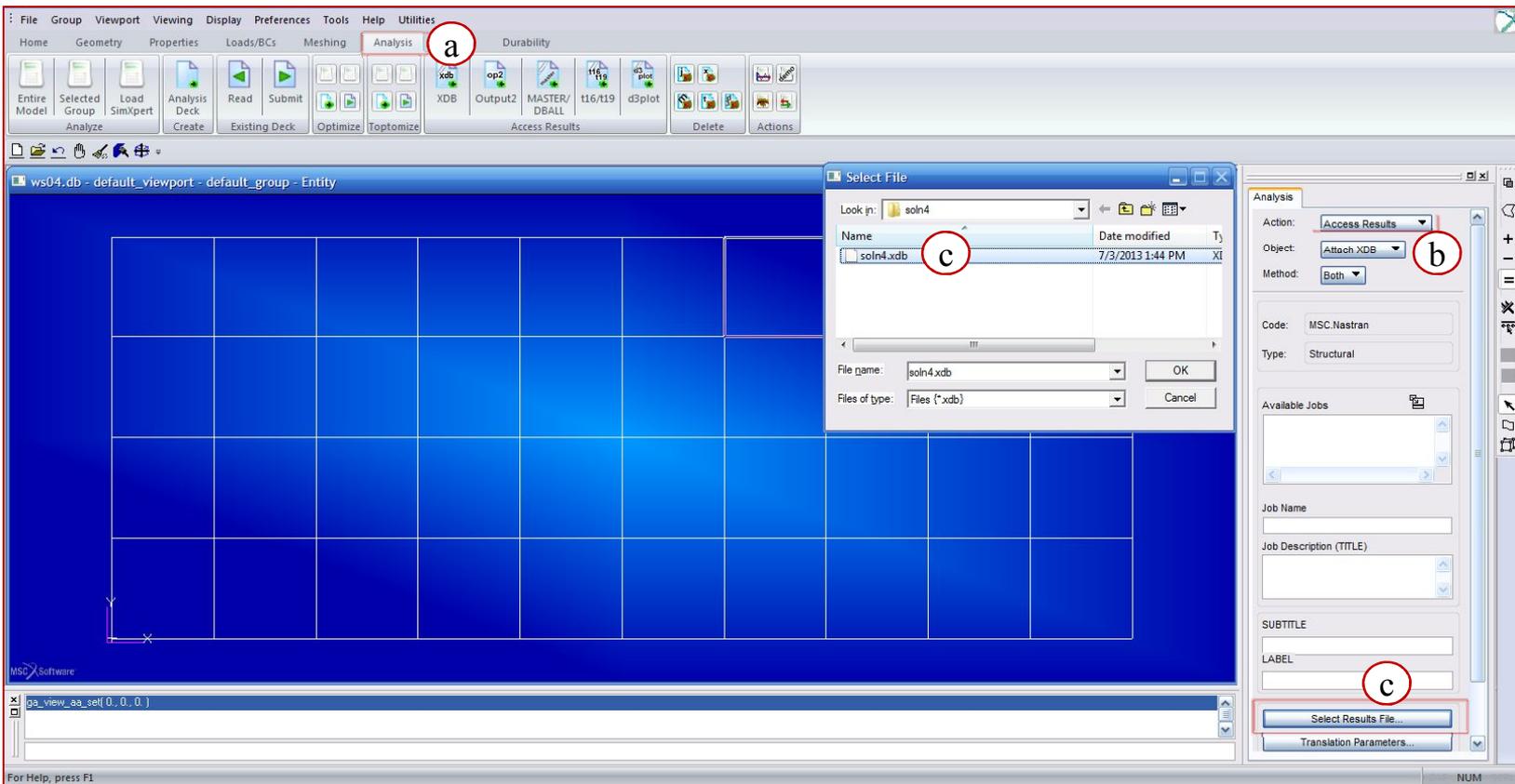
Review the displacement response graph at the loaded corner. (grid point 11)



# Step 11. XY Plot Using Patran

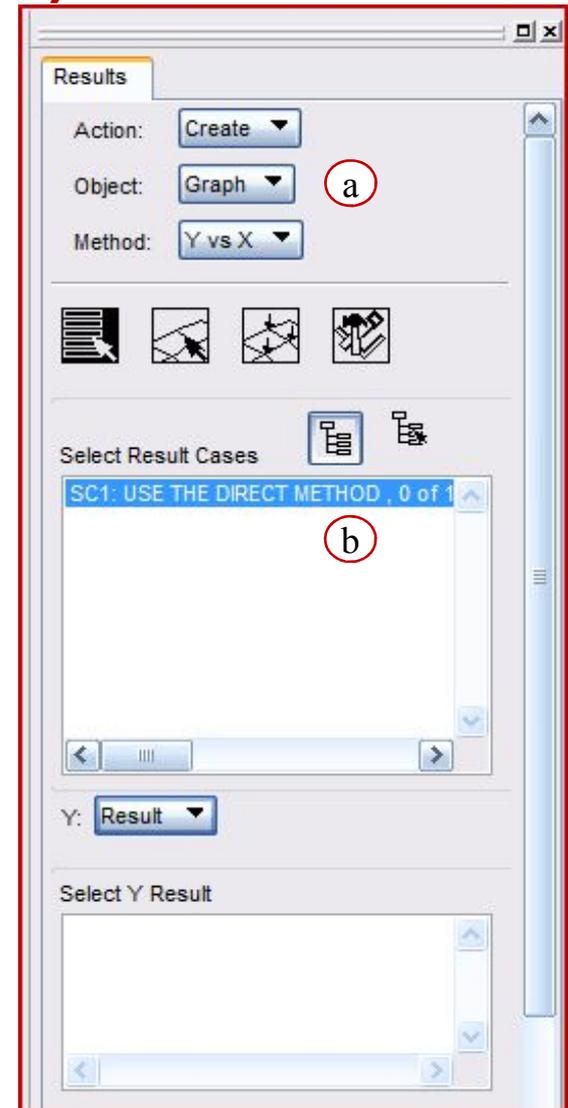
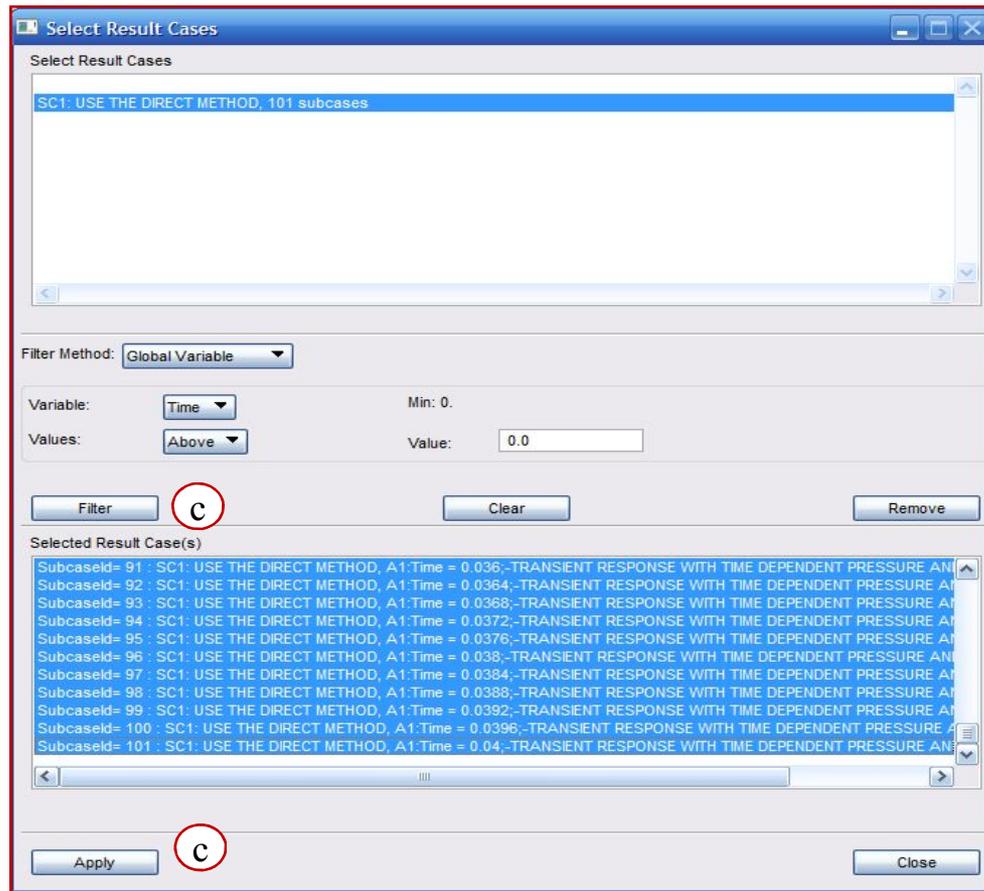
Open New Patran DB then Go to

- a. Analysis
- b. Access Results>Attach XDB>Both
- c. Select Results File>Soln4.xdb



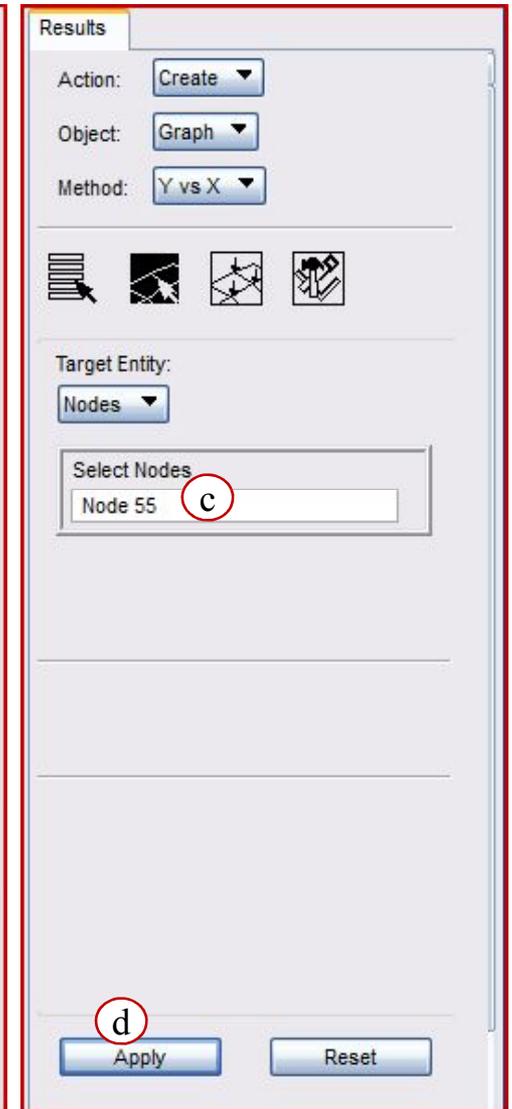
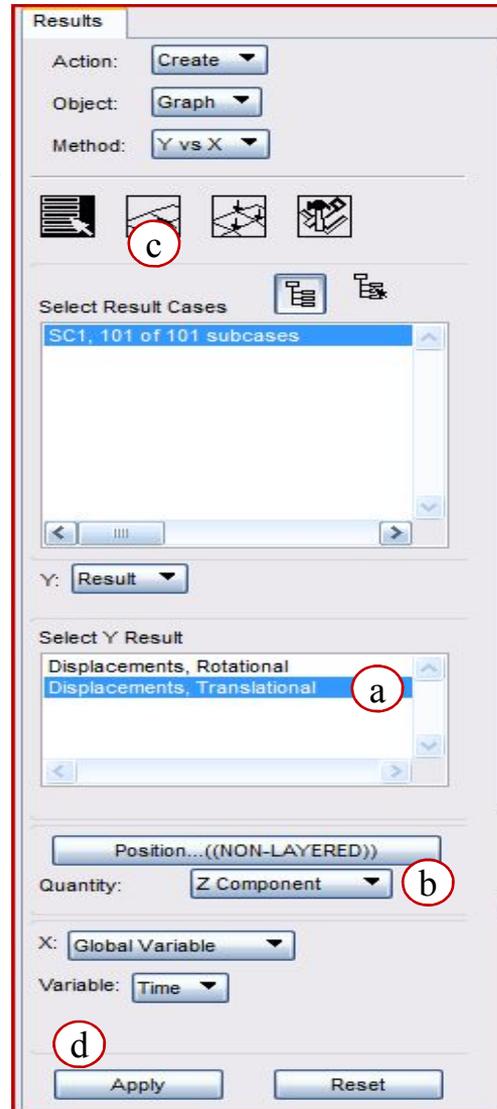
# Step 11. XY Plot Using Patran (Cont.)

- Go to Results – Create>Graph>Y vs X
- Click on the Result Case.
- Click on Filter and select all Result Cases. Hit Apply.



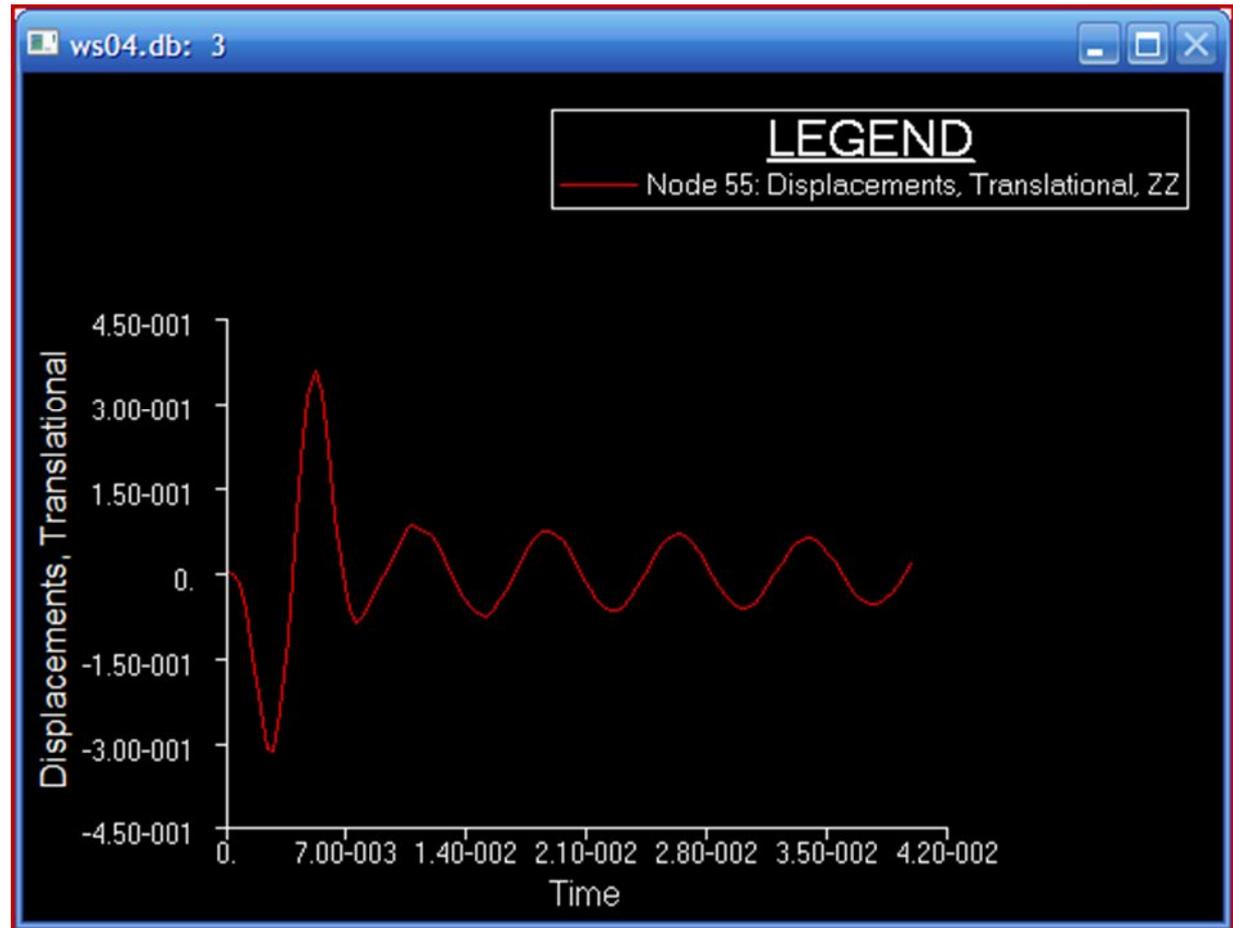
# Step 11. XY Plot Using Patran (Cont.)

- a. Select Y: Result - Displacement, Translational
- b. Select Quantity – Z Component
- c. Click on Icon “Target Entities” and select Node 55
- d. Hit Apply.



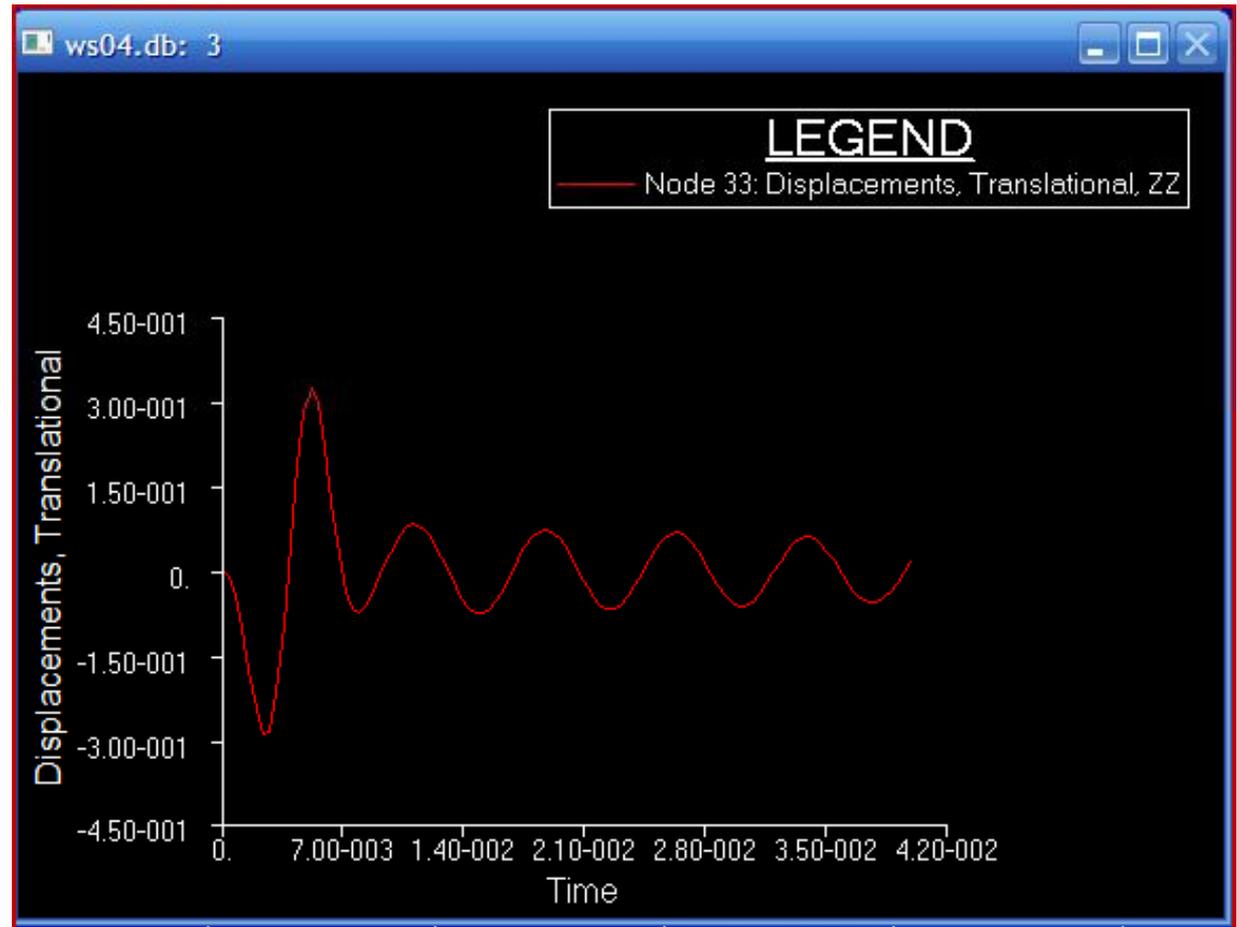
# Step 11. XY Plot Using Patran (Cont.)

Review the displacement response graph at the opposite corner of the point load. (grid 55)



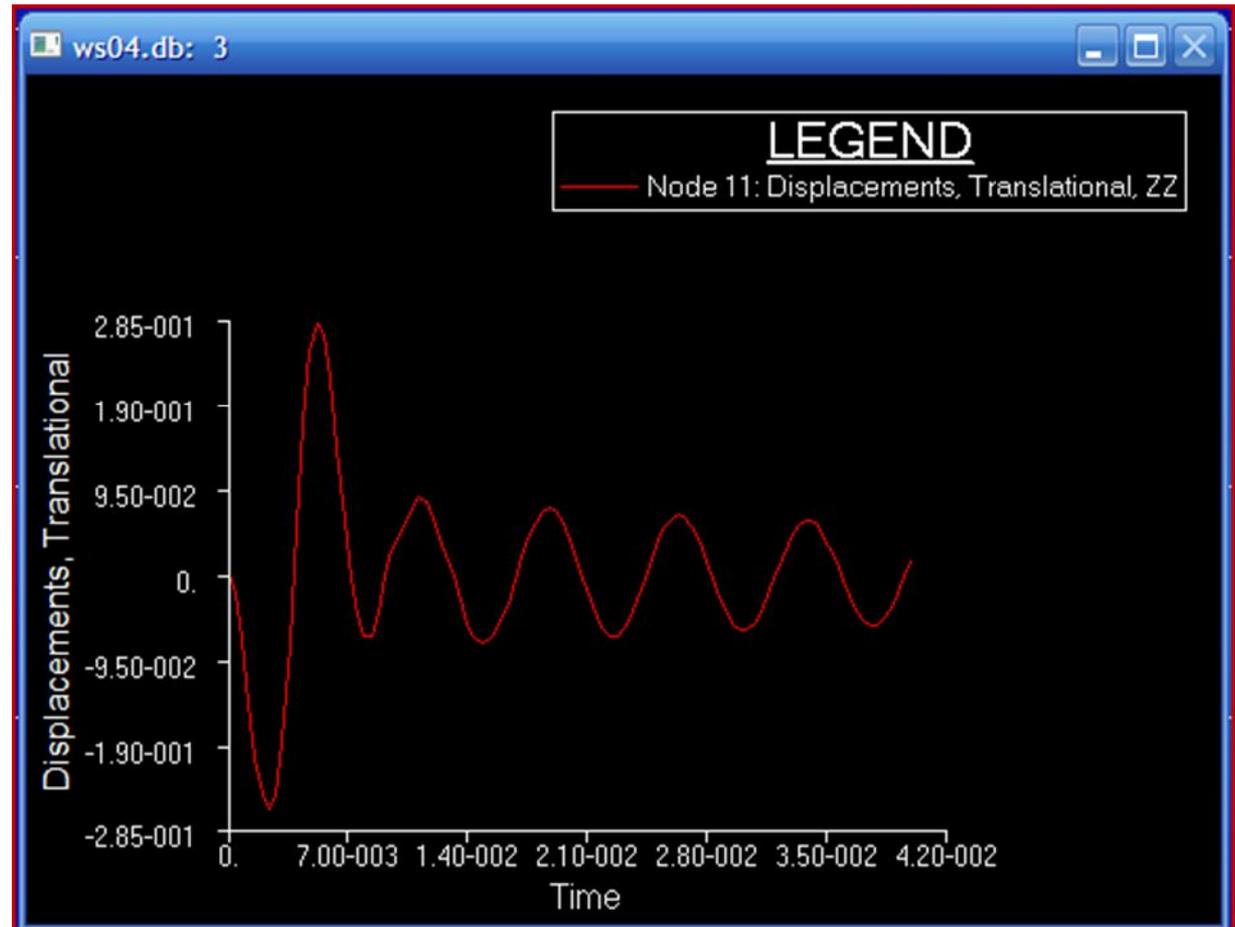
# Step 11. XY Plot Using Patran (Cont.)

Similarly, review the displacement response graph at the center of the tip (grid 33)



# Step 11. XY Plot Using Patran (Cont.)

Similarly, review the displacement response graph at the loaded corner. (grid point 11)





# **WORKSHOP 5**

## **MODAL TRANSIENT RESPONSE**



- **Workshop Objective**

- Using the modal method, determine the transient response of the flat rectangular plate (from Workshop 1) subject to time-varying excitation as described below.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

- plate.bdf
- wkshp5.dat

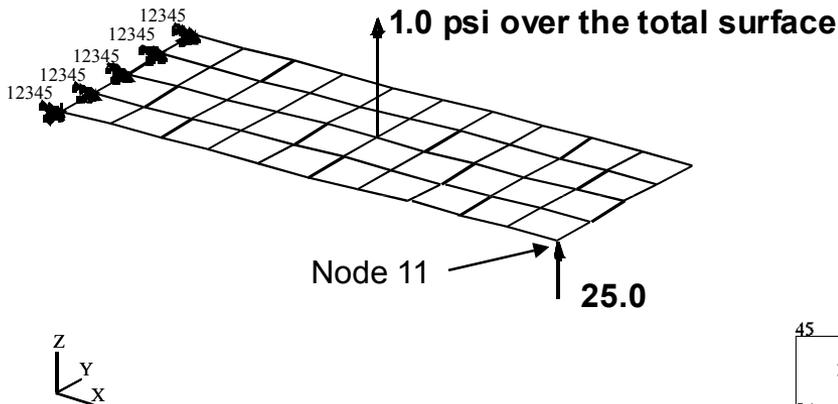
- **Problem Description**

- This structure is excited by a 1 psi pressure load over the total surface of the plate varying at 250 Hz. In addition, a 25 lb force is applied at a corner of the tip also varying at 250 Hz, but starting 0.004 seconds after the pressure load begins. Both time-dependent dynamic loads are applied for duration of 0.008 seconds. Use a modal damping of  $\zeta = 0.03$  for all modes. Carry out the analysis for 0.04 seconds.

- **Problem Description Continued:**

- The figures below show the finite element representation of the flat plate and the loads and boundary condition.

### Loads and Boundary Condition



### Elements and Grid Coordinates

45	46	47	48	49	50	51	52	53	54	55
31	32	33	34	35	36	37	38	39	40	44
34	35	36	37	38	39	40	41	42	43	44
21	22	23	24	25	26	27	28	29	30	33
23	24	25	26	27	28	29	30	31	32	33
11	12	13	14	15	16	17	18	19	20	22
12	13	14	15	16	17	18	19	20	21	22
1	2	3	4	5	6	7	8	9	10	11
1	2	3	4	5	6	7	8	9	10	11

TIP  
↓

- **Suggested Steps**

1. Open and review the input file wkshp5.dat.
2. Add XY plot commands for displacement transient graph.
3. Add eigenvalue method.
4. Add modal damping.
5. Add time dependent pressure load.
6. Add time dependent point load.
7. Add combined loads.
8. Add the time integration step.
9. Save and run the new input file in MSC Nastran.
10. Review the MSC Nastran results using the solution file soln5.f06.
11. Review the graph results.

# Step 1. Open and Review the Input File wkshp5.dat

The file wkshp5.dat is the starting input file to be modified.

```
$
$ wkshp5.dat
$
$ for case control add      :  xyplot commands
$
$ for bulk data add       :  eigenvalue method
$                          modal damping
$                          loading
$                          time integration
$
SOL 112
diag 8
CEND
TITLE = TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE = USE THE MODAL METHOD
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2) = 111
SUBCASE 1
METHOD = 100
TSTEP = 200
SDAMPING = 300
DLOAD = 400
$
OUTPUT (XYPLOT)
$
BEGIN BULK
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE PROBLEM
$
INCLUDE 'plate.bdf'
$
ENDDATA
```

## Step 2. Add XY Plot Commands for Graph

Change file name to **soln5. dat** and add the XY plot commands to graph the displacement response at grid points **11, 33, and 55**, as shown to the right.

```
$
$ soln5.dat
$
SOL 112
diag 8
CEND
TITLE = TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE = USE THE MODAL METHOD
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2) = 111
SUBCASE 1
METHOD = 100
TSTEP = 200
SDAMPING = 300
DLOAD = 400
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE PROBLEM
$
INCLUDE 'plate.bdf'
$
ENDDATA
```

# Step 3. Add Eigenvalue Method

Add the eigenvalue Method:

- a. Use the **EIGRL** entry specifying **5** roots.
- b. Make sure that the **METHOD** Case Control command identification number matches the **EIGRL** SID.

```
$
$   soln5.dat
$
SOL 112
diag 8
CEND
TITLE = TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE = USE THE MODAL METHOD
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2) = 111
SUBCASE 1
METHOD = 100
TSTEP = 200
SDAMPING = 300
DLOAD = 400
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE PROBLEM
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
a EIGRL, 100, , 5
$
ENDDATA
```

# Step 4. Add Modal Damping

Add the modal damping:

- a. Use the **TABDMP1** entry and the given information on page WS-3:
- TID = **300** (note must match identification number from SDAMPING in Case Control)
  - Type = **CRIT**
  - First Natural Freq. = **0.0**
  - Damping Value = **.03**
  - Last Natural Freq. = **10.0** (see note below)
  - Damping Value = **.03**

```
$
$   soln5.dat
$
SOL 112
diag 8
CEND
TITLE = TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE = USE THE MODAL METHOD
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2) = 111
SUBCASE 1
METHOD = 100
TSTEP = 200
SDAMPING = 300
DLOAD = 400
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE PROBLEM
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, , ,5
$
$ SPECIFY MODAL DAMPING
$
TABDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
ENDDATA
```

a

# Step 5. Add Time Dependent Pressure Load

Add the time dependent pressure load of 1 psi over the entire plate varying at 250 HZ.

- a. Use a **TLOAD2** entry in combination with a **PLOAD2** and the given information on page WS5-3:
  - Time = **0 to .008 sec**
  - Frequency = **250 HZ**
  - Phase angle = **-90°**
- b. For the **PLOAD** entry, apply the pressure of **1 psi** over all the elements of the plate. (**1 through 40**)

```
$
$   soln5.dat
$
SOL 112
diag 8
CEND
TITLE = TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE = USE THE MODAL METHOD
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2) = 111
SUBCASE 1
METHOD = 100
TSTEP = 200
SDAMPING = 300
DLOAD = 400
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE PROBLEM
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, , , 5
$
$ SPECIFY MODAL DAMPING
$
TABDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
a $ TIME VARYING PRESSURE LOAD (250 HZ)
$
b TLOAD2, 200, 400, , 0, 0., 8.E-3, 250., -90.
PLOAD2, 400, 1., 1, THRU, 40
$
ENDDATA
```

# Step 6. Add Time Dependent Point Load

Add the time dependent 25 lb point load at the corner of tip of the plate (grid 11) varying at 250 Hz, but starting 0.004 seconds after the pressure load begins.

- a. Use the **TLOAD2** entry in combination with **DAREA** and **DELAY** entries and the above information.
  - Time = **0 to .008 sec**
  - Frequency = **250 HZ**
  - Phase angle = **-90°**
- b. For the **DAREA** entry, note that the **25 lb** force is applied at Grid point **11** in the Z direction.
- c. The **DELAY** entry will define the time delay of **.004** secs for this load.

```
$
$   soln5.dat
$
SOL 112
diag 8
CEND
TITLE = TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE = USE THE MODAL METHOD
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2) = 111
SUBCASE 1
METHOD = 100
TSTEP = 200
SDAMPING = 300
DLOAD = 400
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE PROBLEM
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, , , 5
$
$ SPECIFY MODAL DAMPING
$
TABDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
$ TIME VARYING PRESSURE LOAD (250 HZ)
$
TLOAD2, 200, 400, , 0, 0., 8.E-3, 250., -90.
PLOAD2, 400, 1., 1, THRU, 40
$
$ APPLY POINT LOAD (250 HZ)
$
a TLOAD2, 500, 600,610, 0, 0.0, 8.E-3, 250., -90.
$
b DAREA, 600, 11, 3, 25.
$
c DELAY, 610, 11, 3, 0.004
$
ENDDATA
```

# Step 7. Add Combined Loads

Combine the pressure and point loads using a DLOAD entry.

- a. For the **DLOAD** entry, define the scale as **1.0** for both loads.
- b. Make sure the **DLOAD** Case Control command identification matches the SID for the **DLOAD** entry in the Bulk Data section.

```
$ so1n5.dat
$
$ SOL 112
diag 8
CEND
TITLE = TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE = USE THE MODAL METHOD
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2) = 111
SUBCASE 1
METHOD = 100
TSTEP = 200
SDAMPING = .000
DLOAD = 400
$
OUTPUT (XYPLO b)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XYPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER
XYPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XYPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, COUPLMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE PROBLEM
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, , ,5
$
$ SPECIFY MODAL DAMPING
$
TABDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
$ TIME VARYING PRESSURE LOAD (250 HZ)
$
TLOAD2, 200, 400, , 0, 0., 8.E-3, 250., -90.
PLOAD2, 400, 1., 1, THRU, 40
$
$ APPLY POINT LOAD (250 HZ)
$
TLOAD2, 600, 600,610, 0, 0.0, 8.E-3, 250., -90.
$
DAREA, 600, 11, 3, 25.
$
DELAY, 610, 11, 3, 0.004
$
$ COMBINE LOADS
DLOAD, 400, 1., 1., 200, 1., 500
$
ENDDATA
```

# Step 8. Add Time Integration Step

Add the time step:

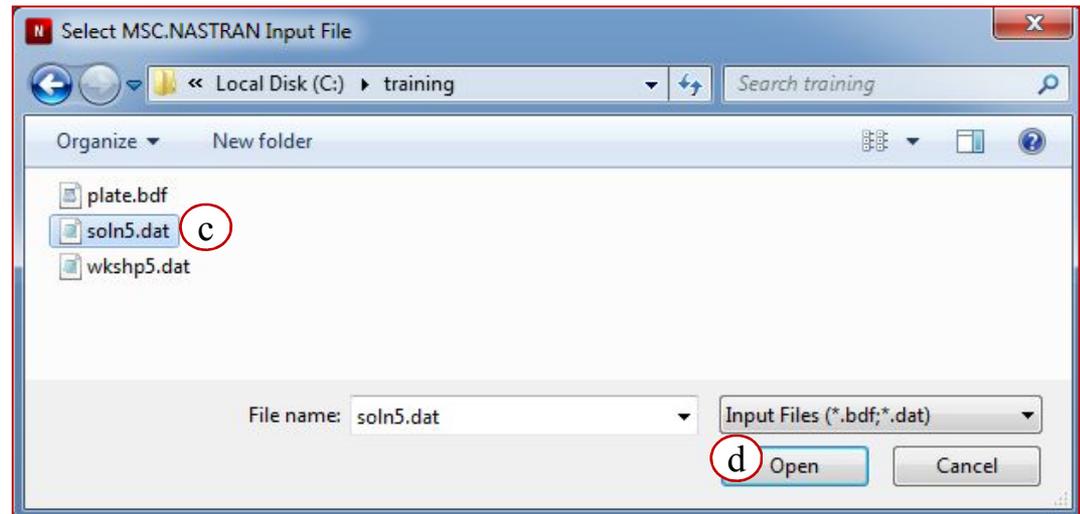
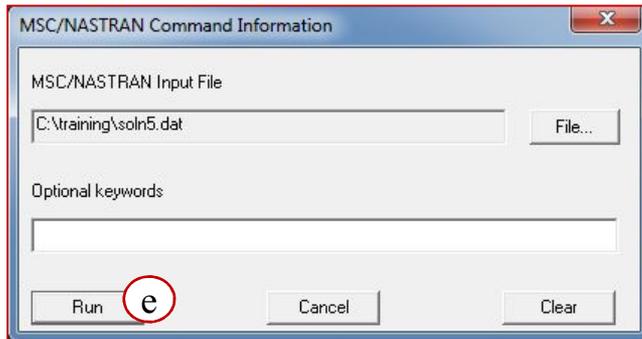
- a. For the **TSTEP** entry, use **200** steps and a time increment of **.0004** seconds, so that the total time will be .04 seconds.
- b. Make sure that the **TSTEP** case control command identification matches the SID for the **TSTEP** entry in the Bulk Data section.

```
$
$   soln5.dat
$
SOL 112
diag 8
CEND
TITLE = TRANSIENT RESPONSE WITH TIME DEPENDENT PRESSURE AND POINT LOADS
SUBTITLE = USE THE MODAL METHOD
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2) = 111
SUBCASE 1
METHOD = 100
TSTEP = 200
SDAMPING = 200
DLOAD = 40
$
OUTPUT (XPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER
XPLOT DISP RESPONSE / 11 (T3)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER
XPLOT DISP RESPONSE / 33 (T3)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER
XPLOT DISP RESPONSE / 55 (T3)
$
BEGIN BULK
PARAM, COMPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE PROBLEM
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, , ,5
$
$ SPECIFY MODAL DAMPING
$
TABDMP1, 100, CRIT,
+, 0., .03, 10., .03, ENDT
$
$ TIME VARYING PRESSURE LOAD (250 HZ)
$
TLOAD2, 200, 400, , 0, 0., 8.E-3, 250., -90.
PLOAD2, 400, 1., 1, THRU, 40
$
$ APPLY POINT LOAD (250 HZ)
$
TLOAD2, 500, 600,610, 0, 0.0, 8.E-3, 250., -90.
$
DAREA, 600, 11, 3, 25.
$
DELAY, 610, 11, 3, 0.004
$
$ COMBINE LOADS
$
DLOAD, 400, 1., 1., 200, 1., 500
$
$ SPECIFY INTERGRATION TIME STEPS
$
TSTEP, 200, 100, 4.0E-4, 1
$
ENDDATA
```

# Step 9. Save and Run the New Input File

Save and run the modified file in MSC Nastran.

- a. Save the modified file as **soln5.dat**.
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln5.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 10. Review the Results in the Solution File

Open the soln5.f06 file to see the results

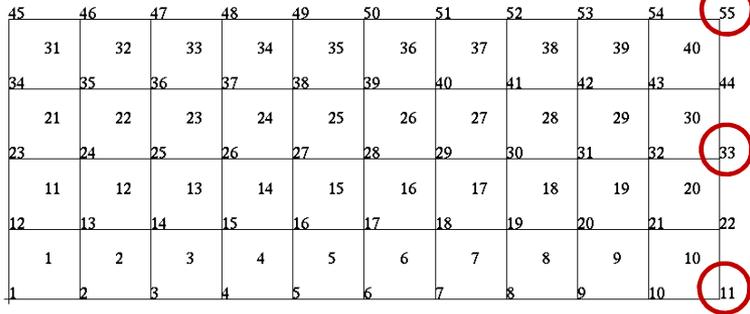
MODE NO.	EXTRACTION ORDER	EIGENVALUE	REAL EIGENVALUES (BEFORE AUGMENTATION OF RESIDUAL VECTORS)		GENERALIZED MASS	GENERALIZED STIFFNESS
			RADIANS	CYCLES		
1	1	7.055894E+05	8.399937E+02	1.336891E+02	1.000000E+00	7.055894E+05
2	2	1.877186E+07	4.332651E+03	6.895628E+02	1.000000E+00	1.877186E+07
3	3	2.811177E+07	5.302053E+03	8.438480E+02	1.000000E+00	2.811177E+07
4	4	1.929422E+08	1.389036E+04	2.210720E+03	1.000000E+00	1.929422E+08
5	5	2.221657E+08	1.490523E+04	2.372240E+03	1.000000E+00	2.221657E+08

MODE NO.	EXTRACTION ORDER	EIGENVALUE	REAL EIGENVALUES (AFTER AUGMENTATION OF RESIDUAL VECTORS)		GENERALIZED MASS	GENERALIZED STIFFNESS
			RADIANS	CYCLES		
1	1	7.055894E+05	8.399937E+02	1.336891E+02	1.000000E+00	7.055894E+05
2	2	1.877186E+07	4.332651E+03	6.895628E+02	1.000000E+00	1.877186E+07
3	3	2.811176E+07	5.302053E+03	8.438479E+02	1.000000E+00	2.811176E+07
4	4	1.929422E+08	1.389036E+04	2.210720E+03	1.000000E+00	1.929422E+08
5	5	2.221657E+08	1.490523E+04	2.372240E+03	1.000000E+00	2.221657E+08
6	6	2.351324E+08	1.533403E+04	2.440486E+03	1.000000E+00	2.351324E+08
7	7	7.974902E+08	2.823987E+04	4.494515E+03	1.000000E+00	7.974902E+08
8	8	1.453224E+09	3.812117E+04	6.067173E+03	1.000000E+00	1.453224E+09
9	9	2.625274E+09	5.123743E+04	8.154690E+03	1.000000E+00	2.625274E+09
10	10	4.154733E+09	6.445722E+04	1.025868E+04	1.000000E+00	4.154733E+09
11	11	4.205890E+09	6.485284E+04	1.032165E+04	1.000000E+00	4.205890E+09
12	12	3.216783E+10	1.793539E+05	2.854506E+04	1.000000E+00	3.216783E+10

# Step 10. Review the Results in the Solution File (Cont.)

The three grid points of interest for the displacement vector lie along the tip of the plate, grid points 55, 33, 11.

Elements and Grid Coordinates



POINT ID = 55									
DISPLACEMENT VECTOR									
TIME	TYPE	T1	T2	T3	R1	R2	R3		
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0		
4.000000E-04	G	2.313504E-15	1.270176E-15	2.038511E-04	3.216275E-06	2.622230E-05	1.866210E-14		
8.000000E-04	G	-1.737935E-14	1.430908E-14	1.980840E-03	1.514255E-05	-2.074704E-04	1.465395E-14		
1.200000E-03	G	-9.910111E-14	4.294976E-14	6.911171E-03	-5.569034E-07	-1.653289E-03	4.203785E-14		
1.600000E-03	G	-9.446632E-14	8.440153E-14	1.407446E-02	-2.646987E-05	-3.815674E-03	8.127371E-14		
2.000000E-03	G	-1.412563E-13	1.273749E-13	2.121054E-02	-4.360946E-05	-5.847335E-03	1.216690E-13		
2.400000E-03	G	1.707517E-13	1.548096E-13	2.611754E-03	6.863064E-05	7.455783E-03	1.473008E-13		
2.800000E-03	G	-1.686413E-13	1.534098E-13	2.608514E-02	-7.741245E-05	-7.598883E-03	1.456184E-13		
3.200000E-03	G	-1.287308E-13	1.173609E-13	1.986141E-02	-5.680266E-05	-5.762664E-03	1.111531E-13		
3.600000E-03	G	-5.511563E-14	5.047610E-14	8.672326E-03	-2.997876E-05	-2.603049E-03	4.766625E-14		
4.000000E-03	G	3.514827E-14	-3.173204E-14	-5.221079E-03	8.848282E-06	1.410855E-03	-3.025671E-14		
4.400000E-03	G	1.658824E-13	2.540990E-13	1.854531E-02	3.727285E-03	3.537802E-03	-1.417560E-13		
4.800000E-03	G	-1.968213E-13	-3.478864E-13	-2.088837E-02	-1.529782E-02	-1.366687E-03	-1.707394E-13		

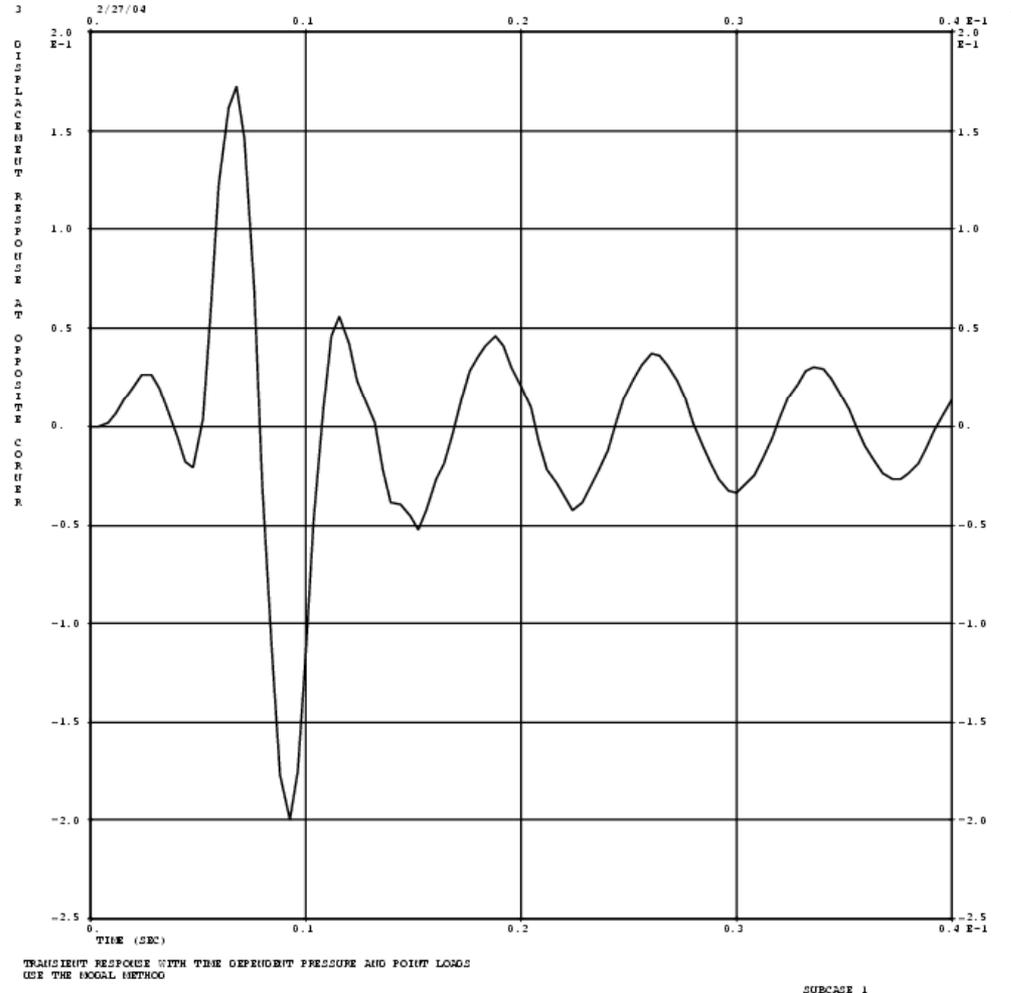
POINT-ID = 33									
DISPLACEMENT VECTOR									
TIME	TYPE	T1	T2	T3	R1	R2	R3		
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0		
4.000000E-04	G	-8.129837E-16	5.780443E-16	2.019039E-04	1.682611E-08	2.577562E-05	8.782824E-16		
8.000000E-04	G	-5.437351E-15	9.429436E-15	1.971792E-03	-1.131780E-09	-2.092973E-04	7.575267E-15		
1.200000E-03	G	-1.469813E-14	2.927401E-14	6.911632E-03	-3.468305E-08	-1.653002E-03	2.206328E-14		
1.600000E-03	G	-2.785020E-14	5.818323E-14	1.409060E-02	-1.660808E-08	-3.811871E-03	4.289858E-14		
2.000000E-03	G	-4.146658E-14	8.826009E-14	2.123710E-02	-1.844668E-10	-5.841007E-03	6.439060E-14		
2.400000E-03	G	-4.989096E-14	1.075618E-13	2.615920E-02	1.753987E-08	-7.446125E-03	7.806433E-14		
2.800000E-03	G	-4.913178E-14	1.067672E-13	2.613206E-02	2.261718E-08	-7.588134E-03	7.723877E-14		
3.200000E-03	G	-3.749043E-14	8.178410E-14	1.989586E-02	1.935897E-08	-5.754695E-03	5.900108E-14		
3.600000E-03	G	-1.597640E-14	3.523036E-14	8.690471E-03	1.195476E-08	-2.598933E-03	2.532892E-14		
4.000000E-03	G	1.033014E-11	-2.200721E-11	-5.226488E-03	-1.555539E-10	1.109517E-03	-1.602123E-11		
4.400000E-03	G	4.430020E-14	-2.191627E-13	-1.444897E-02	-4.622429E-03	2.613301E-03	-9.125456E-14		
4.800000E-03	G	4.852553E-14	-3.087126E-13	-4.958413E-03	-1.673921E-02	-3.303262E-03	-1.161244E-13		
5.200000E-03	G	-8.218304E-15	-1.898447E-13	2.235487E-02	-1.968060E-02	-1.012875E-02	-3.180895E-14		

POINT-ID = 11									
DISPLACEMENT VECTOR									
TIME	TYPE	T1	T2	T3	R1	R2	R3		
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0		
4.000000E-04	G	-5.468724E-16	8.285983E-17	2.038250E-04	-3.199117E-06	2.623944E-05	2.229172E-16		
8.000000E-04	G	-2.153063E-15	6.017427E-15	1.980818E-03	-1.510275E-05	-2.074038E-04	3.009406E-15		
1.200000E-03	G	-4.732603E-15	1.876118E-14	6.911292E-03	4.029351E-07	-1.653521E-03	9.214503E-15		
1.600000E-03	G	-6.821115E-15	3.897766E-14	1.407446E-02	2.646134E-05	-3.815677E-03	1.823616E-14		
2.000000E-03	G	-1.175393E-14	6.110972E-14	2.121053E-02	4.361140E-05	-5.847335E-03	2.758160E-14		
2.400000E-03	G	-1.374123E-14	7.478438E-14	2.611749E-02	6.869039E-05	-7.455696E-03	3.359488E-14		
2.800000E-03	G	-1.328659E-14	7.442078E-14	2.608508E-02	7.748552E-05	-7.598778E-03	3.32740E-14		
3.200000E-03	G	-1.006076E-14	5.711146E-14	1.986136E-02	5.686198E-05	-5.762578E-03	2.550997E-14		
3.600000E-03	G	-4.168126E-15	2.469733E-14	8.672293E-03	3.001545E-05	-2.602997E-03	1.098888E-14		
4.000000E-03	G	2.927909E-15	-1.525175E-14	-5.221079E-03	-9.018792E-06	1.410939E-03	-6.874774E-15		
4.400000E-03	G	-1.632934E-14	-1.940992E-13	-9.066898E-03	-5.62542E-03	9.466209E-03	-8.908224E-14		
4.800000E-03	G	-3.433218E-14	-2.813239E-13	1.286251E-02	-1.815789E-02	-7.924688E-03	-8.140870E-14		

# Step 11. Review the Graph Results

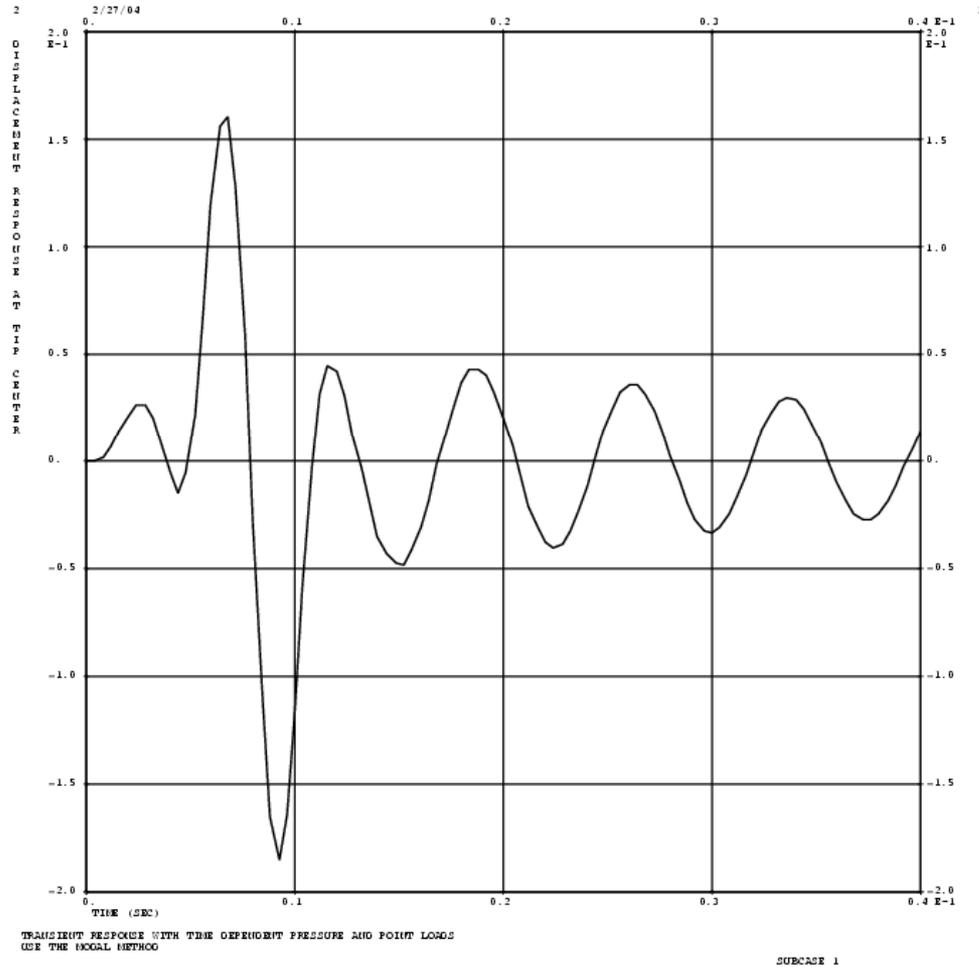
Recall that to obtain the graphs you will need to convert the **.plt** file to a **.ps** file, if needed, use the directions given in workshop 4, step 9

Review the displacement response graph at the opposite corner of the point load. (grid 55)



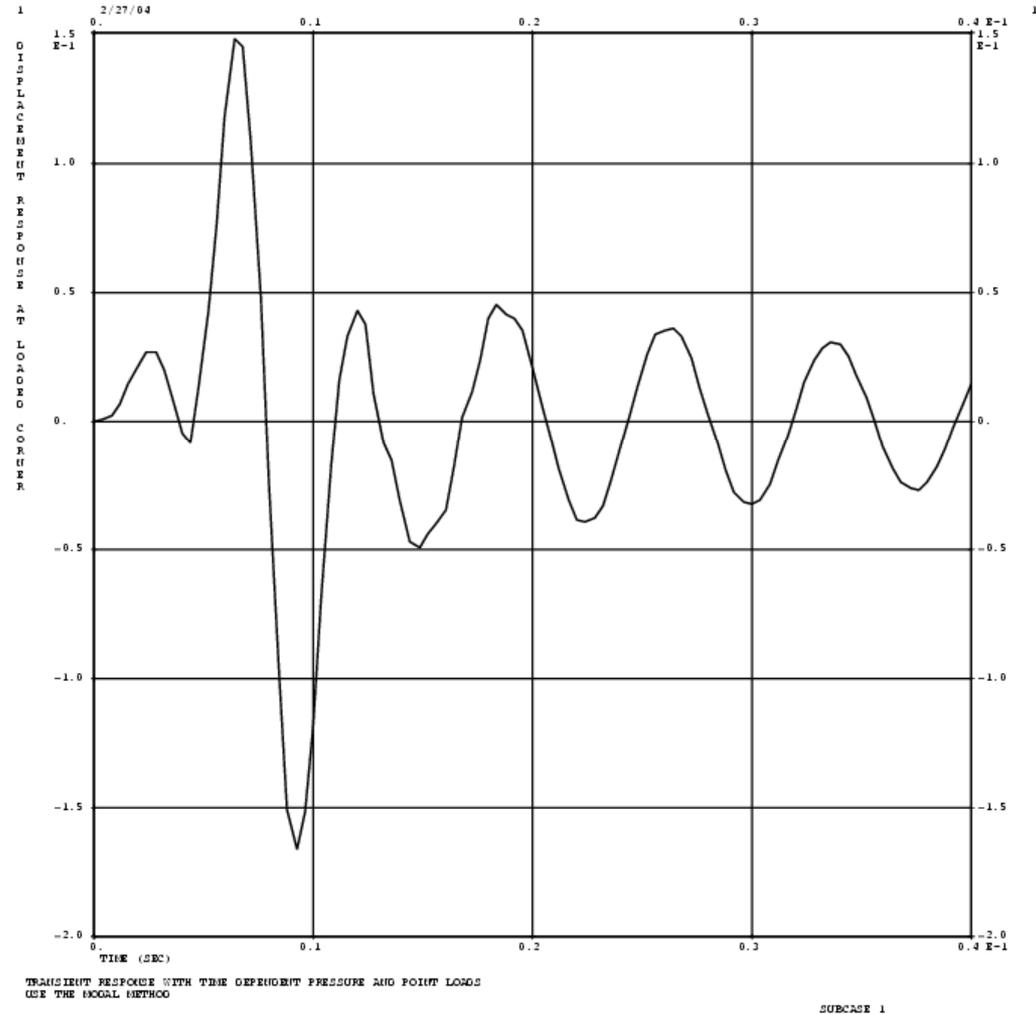
# Step 11. Review the Graph Results (Cont.)

Review the displacement response graph at the center of the tip of the plate. (grid 33)



# Step 11. Review the Graph Results (Cont.)

Review the displacement response graph at the loaded corner. (grid 11)





# **WORKSHOP 6**

## **DIRECT FREQUENCY RESPONSE**



- **Workshop Objective**

- Using the direct method, determine the frequency response of the flat rectangular plate (from Workshop 1) subject to frequency-varying excitation as described below.

- **Software Version**

- MSC Nastran 2013

- **Required Files**

- plate.bdf
- wkshp6.dat

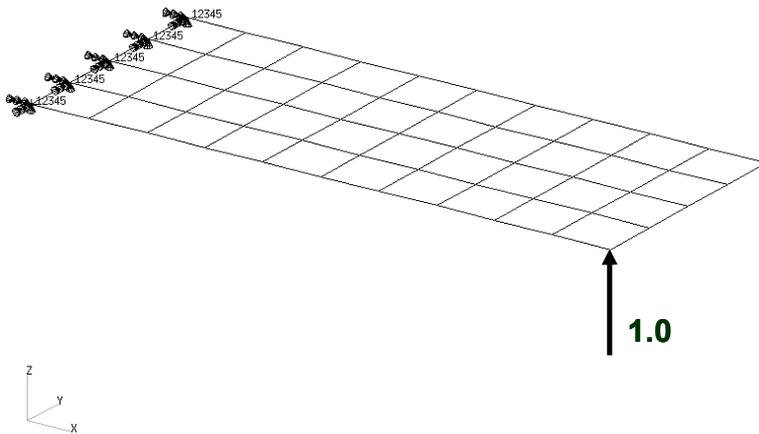
- **Problem Description**

- The structure is excited by a unit load at a corner of the tip. Use a frequency step of 20 Hz between a range of 20 and 1000 Hz. Use structural damping of  $g=0.06$ .

- **Problem Description Continued**

- The figures below show the finite element representation of the flat plate and the loads and boundary condition.

Loads and Boundary Condition



Elements and Grid Coordinates

45	46	47	48	49	50	51	52	53	54	55
31	32	33	34	35	36	37	38	39	40	44
34	35	36	37	38	39	40	41	42	43	44
21	22	23	24	25	26	27	28	29	30	33
23	24	25	26	27	28	29	30	31	32	33
11	12	13	14	15	16	17	18	19	20	22
12	13	14	15	16	17	18	19	20	21	22
1	2	3	4	5	6	7	8	9	10	11
1	2	3	4	5	6	7	8	9	10	11

TIP  
↓

- **Suggested Steps**

1. Open and review the input file wkshp6.dat.
2. Add structural damping.
3. Add the point load.
4. Add frequencies of applied loading.
5. Save and run the new input file in MSC Nastran.
6. Review the MSC Nastran results using the solution file soln6.f06.
7. Review the graph results.

# Step 1. Open and Review the Input File wkshp6.dat

The file wkshp6.dat is the starting input file to be modified.

To complete input file add these entries

```
$
$ wkshp6.dat
$
$ add      :      structural damping
$          :      loading
$          :      frequencies of applied loadings
$
$
$ SOL 108
$ CEND
$ TITLE = FREQUENCY RESPONSE DUE TO UNIT FORCE AT TIP
$ ECHO = UNSORTED
$ SPC = 1
$ SET 111 = 11, 33, 55
$ DISPLACEMENT(SORT2, PHASE) = 111
$ SUBCASE 1
$ DLOAD = 500
$ FREQUENCY = 100
$
$ OUTPUT (XYPLOT)
$
```

Output displacement response graphs at grid points 11, 33,55

```
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
VTLOG= YES
VBLOG= NO
XTITLE= FREQUENCY (HZ)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
$ BEGIN BULK
$ param,post,0
$ PARAM, COUPMASS, 1
$ PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
$ INCLUDE 'plate.bdf'
$
$ ENDDATA
```

# Step 2. Add Structural Damping

Add the appropriate parameters in the Bulk Data section for damping.

- a. First rename the input file as **soln6.dat**.
- b. Use **PARAM, G** with a value of **.06**.

```
$
$ soln6.dat (a)
$
SOL 108
CEND
TITLE = FREQUENCY RESPONSE DUE TO UNIT FORCE AT TIP
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2, PHASE) = 111
SUBCASE 1
DLOAD = 500
FREQUENCY = 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
(b) PARAM, G, 0.06
$
ENDDATA
```

# Step 3. Add the Point Load

Add unit point load at the corner of the tip of the plate (grid point 11).

- a. Use the **RLOAD2** entry in combination with **DAREA** and **TABLED1** entries.
- b. For the **DAREA** entry, note that the unit load is applied at grid point **11** in the Z direction.
- c. The **TABLED1** entry defines the load as **1 psi** for all frequencies.

```
$
$   soln6.dat
$
SOL 108
CEND
TITLE = FREQUENCY RESPONSE DUE TO UNIT FORCE AT TIP
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2, PHASE) = 111
SUBCASE 1
DLOAD = 500
FREQUENCY = 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
a $ APPLY UNIT FORCE AT TIP POINT
$
b RLOAD2, 500, 600, , , 310
$
c DAREA, 600, 11, 3, 1.0
$
TABLED1, 310,
, 0., 1., 1000., 1., ENDT
$
ENDDATA
```

# Step 4. Add Frequencies of Applied Loading

To add the frequency of the applied load use the **FREQ1** entry.

- a. From the given information you can obtain for the **FREQ1** entry:
- First freq. = **20.0**
  - Frequency incr = **20.0**
  - Number of freq. increments = **49**

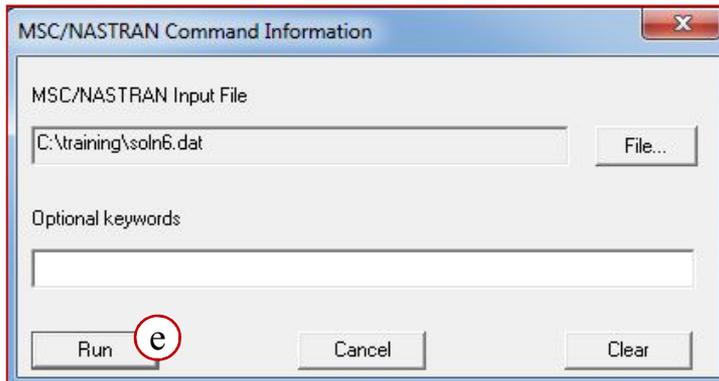
```
$
$   soln6.dat
$
ID SEMINAR, PROBS
SOL 108
CEND
TITLE = FREQUENCY RESPONSE DUE TO UNIT FORCE AT TIP
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(SORT2, PHASE) = 111
SUBCASE 1
DLOAD = 500
FREQUENCY = 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$ APPLY UNIT FORCE AT TIP POINT
$
RLOAD2, 500, 600, ., ., 310
$
DAREA, 600, 11, 3, 1.0
$
TABLED1, 310,
, 0., 1., 1000., 1., ENDT
$
$ SPECIFY FREQUENCY STEPS
$
FREQ1, 100, 20., 20., 49
$
ENDDATA
```

a

# Step 5. Save and Run the New Input File

Save and run the modified file in Nastran.

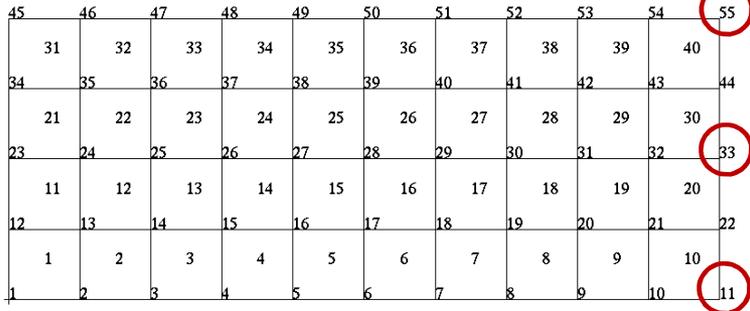
- a. Save the modified file as **soln6.dat**.
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln6.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 6. Review the Results in the Solution File

To see the results open the soln6.f06 file. The three grid points of interest lie along the tip of the plate, grid points 11, 33, 55.

Elements and Grid Coordinates



POINT-ID = 11

COMPLEX DISPLACEMENT VECTOR (MAGNITUDE/PHASE)

FREQUENCY	TYPE	T1	T2	T3	R1	R2	R3
2.000000E+01	G	0.0	0.0	8.819408E-03	6.441100E-04	2.632465E-03	0.0
4.000000E+01	G	0.0	0.0	356.4954	176.5664	176.5000	0.0
6.000000E+01	G	0.0	0.0	9.405909E-03	6.440273E-04	2.796052E-03	0.0
8.000000E+01	G	0.0	0.0	356.2596	176.5676	176.2785	0.0
1.000000E+02	G	0.0	0.0	1.060028E-02	6.434119E-04	3.129193E-03	0.0
1.200000E+02	G	0.0	0.0	355.7716	176.5759	175.8153	0.0
1.400000E+02	G	0.0	0.0	1.296266E-02	6.410197E-04	3.788116E-03	0.0
1.600000E+02	G	0.0	0.0	354.7845	176.6117	174.8655	0.0
1.800000E+02	G	0.0	0.0	1.841381E-02	6.325896E-04	5.308459E-03	0.0
2.000000E+02	G	0.0	0.0	352.4442	176.7802	172.5776	0.0
2.200000E+02	G	0.0	0.0	3.921209E-02	5.927568E-04	1.110665E-02	0.0
2.400000E+02	G	0.0	0.0	343.1410	178.4757	163.3465	0.0
2.600000E+02	G	0.0	0.0	6.786681E-02	8.151206E-04	1.879545E-02	0.0
2.800000E+02	G	0.0	0.0	212.2654	182.8153	32.5699	0.0
3.000000E+02	G	0.0	0.0	1.700927E-02	7.266111E-04	4.576244E-03	0.0

POINT-ID = 33

COMPLEX DISPLACEMENT VECTOR (MAGNITUDE/PHASE)

FREQUENCY	TYPE	T1	T2	T3	R1	R2	R3
3.400000E+02	G	0.0	0.0	1.183179E-03	7.619375E-04	1.388168E-04	0.0
3.600000E+02	G	0.0	0.0	181.6065	175.5985	9.4012	0.0
3.800000E+02	G	0.0	0.0	9.985925E-04	7.889073E-04	8.470200E-05	0.0
4.000000E+02	G	0.0	0.0	181.7391	175.4331	15.3672	0.0
4.200000E+02	G	0.0	0.0	8.462477E-04	8.198517E-04	4.161508E-05	0.0
4.400000E+02	G	0.0	0.0	181.9362	175.2419	32.9193	0.0
4.600000E+02	G	0.0	0.0	7.182849E-04	8.555513E-04	2.375532E-05	0.0
4.800000E+02	G	0.0	0.0	182.2111	175.0196	103.4062	0.0
5.000000E+02	G	0.0	0.0	6.090629E-04	8.970169E-04	4.769354E-05	0.0
5.200000E+02	G	0.0	0.0	182.5852	174.7594	149.9471	0.0
5.400000E+02	G	0.0	0.0	5.144193E-04	9.455804E-04	7.773183E-05	0.0
5.600000E+02	G	0.0	0.0	183.0934	174.4521	161.2894	0.0
5.800000E+02	G	0.0	0.0	4.312082E-04	1.003090E-03	1.067849E-04	0.0

POINT-ID = 55

COMPLEX DISPLACEMENT VECTOR (MAGNITUDE/PHASE)

FREQUENCY	TYPE	T1	T2	T3	R1	R2	R3
2.000000E+01	G	0.0	0.0	7.607307E-03	5.586302E-04	2.371588E-03	0.0
4.000000E+01	G	0.0	0.0	356.4844	176.5612	176.4928	0.0
6.000000E+01	G	0.0	0.0	8.191263E-03	5.612382E-04	2.535021E-03	0.0
8.000000E+01	G	0.0	0.0	356.2155	176.5443	176.2491	0.0
1.000000E+02	G	0.0	0.0	9.381446E-03	5.660907E-04	2.867918E-03	0.0
1.200000E+02	G	0.0	0.0	355.6711	176.5091	175.7475	0.0
1.400000E+02	G	0.0	0.0	1.173825E-02	5.744757E-04	3.526566E-03	0.0
1.600000E+02	G	0.0	0.0	354.6027	176.4334	174.7402	0.0
1.800000E+02	G	0.0	0.0	1.718416E-02	5.907269E-04	5.046961E-03	0.0
2.000000E+02	G	0.0	0.0	352.1532	176.2103	172.3715	0.0
2.200000E+02	G	0.0	0.0	3.800388E-02	6.409441E-04	1.085099E-02	0.0
2.400000E+02	G	0.0	0.0	342.7088	174.6286	163.0298	0.0
2.600000E+02	G	0.0	0.0	6.888805E-02	4.439450E-04	1.900915E-02	0.0
2.800000E+02	G	0.0	0.0	212.5546	182.8153	32.5699	0.0

# Step 7. Review the Graph Results

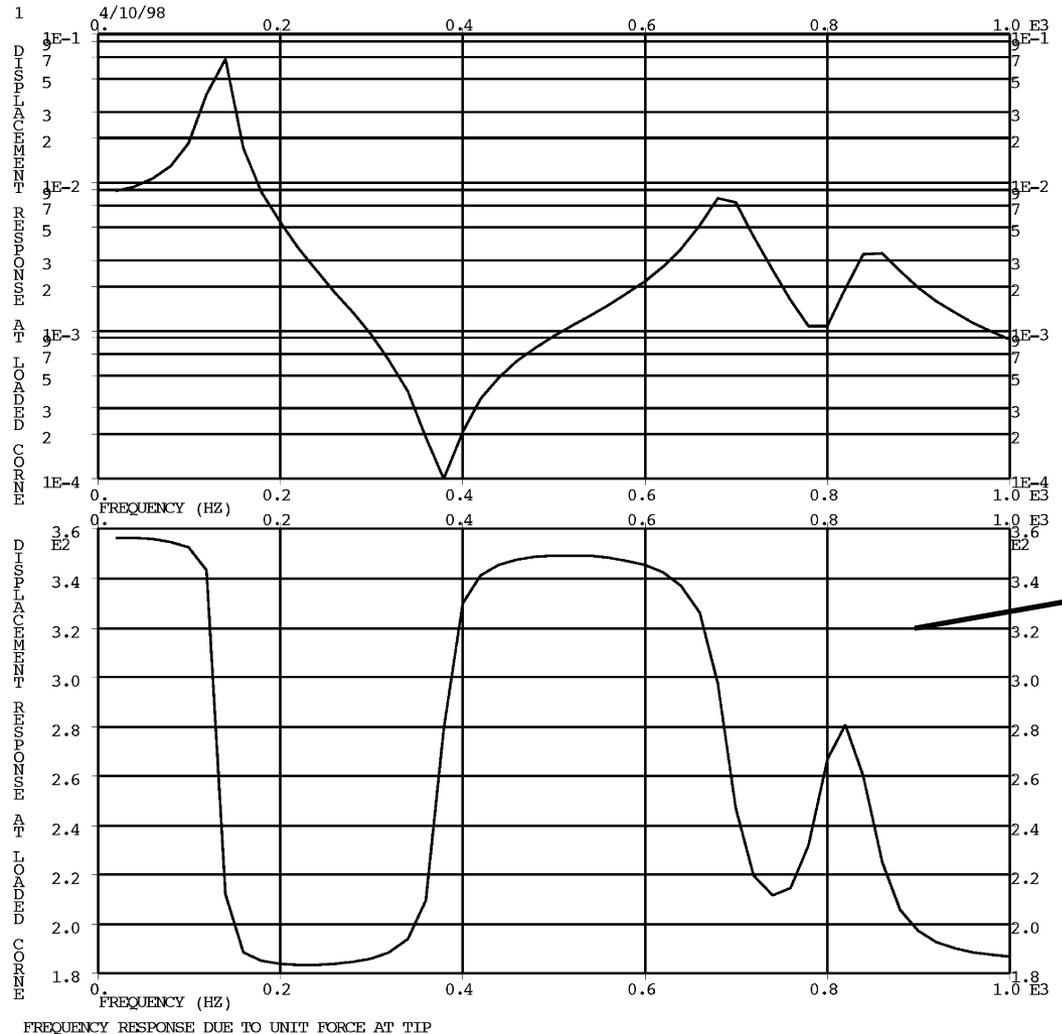
Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions given in workshop 4, step 9

Review the displacement response graph at the loaded corner. (grid point 11)

The display of Phase will be different in Patran

$-180^\circ < \text{Phase} < 180^\circ$

Any Phase Lead larger  $180^\circ$  will be displayed as ( Phase -  $360^\circ$  )



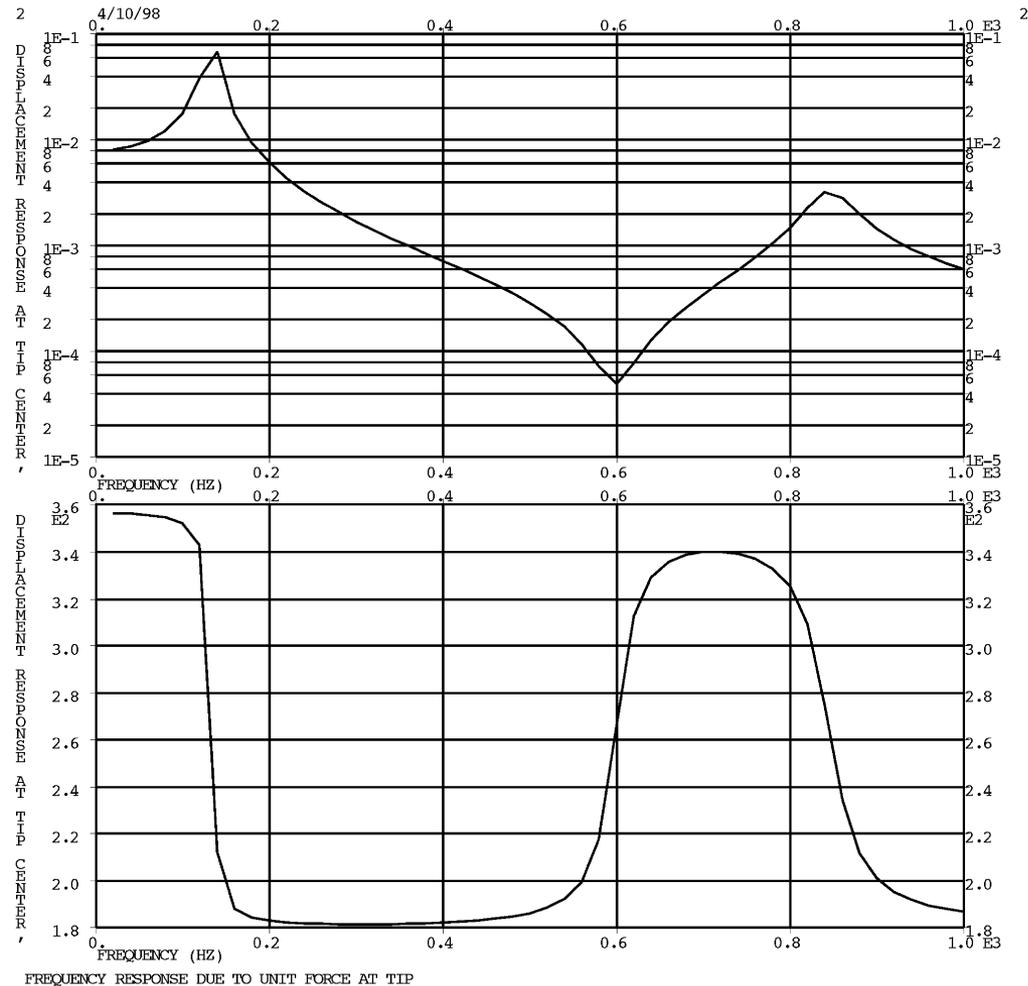
FREQUENCY RESPONSE DUE TO UNIT FORCE AT TIP

SUBCASE 1

Phase Lead calculated by MSC Nastran:  
 $0^\circ < \text{Phase} < 360^\circ$

# Step 7. Review the Graph Results (Cont.)

Review the displacement response graph at the center of tip of the plate. (grid 33)

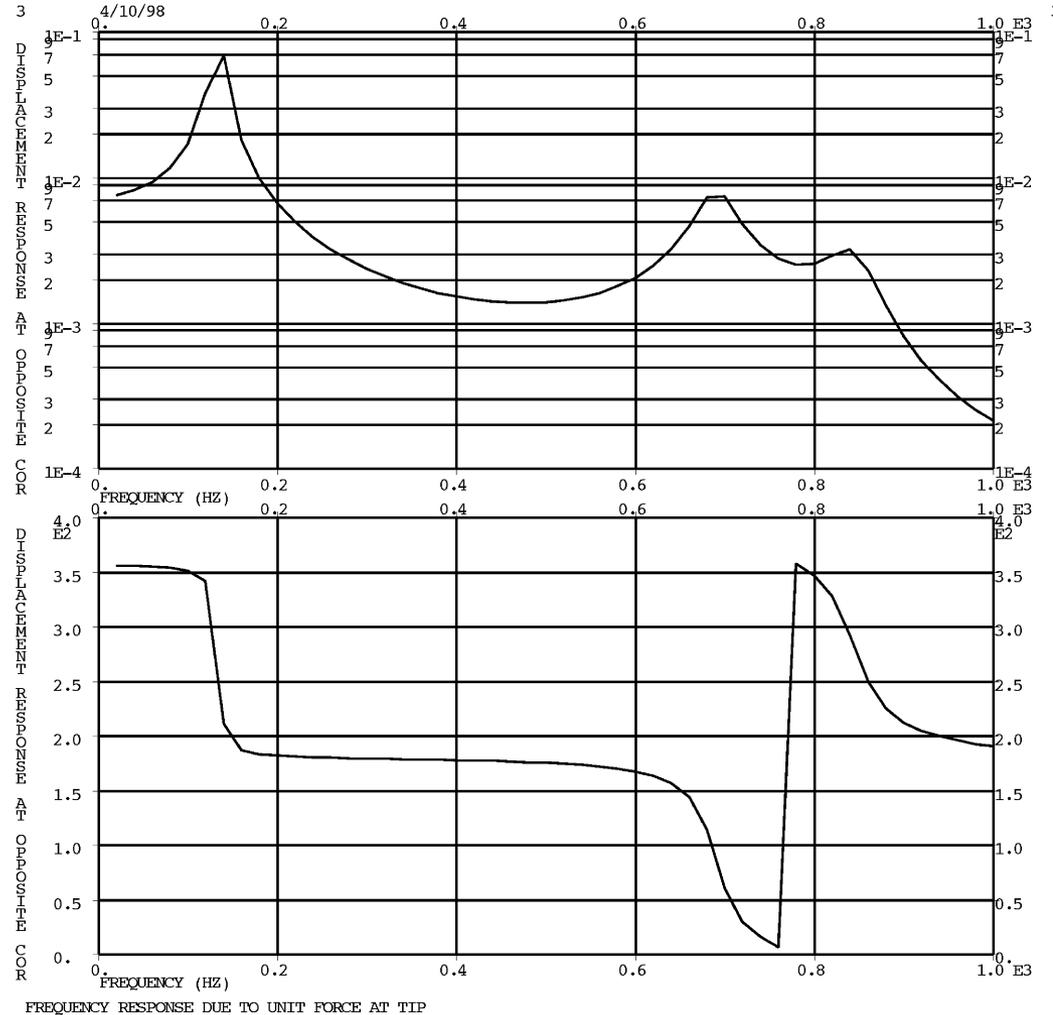


FREQUENCY RESPONSE DUE TO UNIT FORCE AT TIP

SUBCASE 1

# Step 7. Review the Graph Results (Cont.)

Review the displacement response graph at the opposite corner of the point load. (grid point 55)



FREQUENCY RESPONSE DUE TO UNIT FORCE AT TIP

SUBCASE 1

# WORKSHOP 7

## MODAL FREQUENCY RESPONSE



- **Workshop Objective**

- Using the modal method, determine the frequency response of the flat rectangular plate (from Workshop 1) subject to a time varying excitation as described below.

- **Software Version**

- MSC Nastran 2013

- **Required Files**

- plate.bdf
- wkshop7.dat

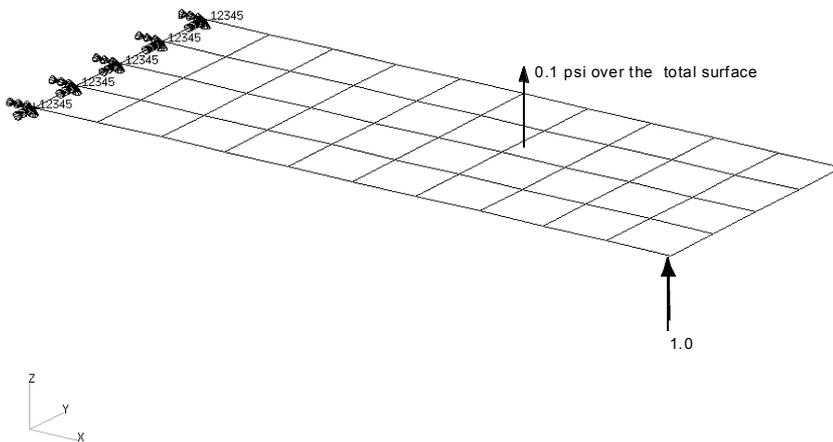
- **Problem Description**

- The structure is excited by a 0.1 psi pressure load over the total surface of the plate and a 1.0 lb. force at a corner of the tip lagging 45°. Use a modal damping ratio of  $\zeta = 0.03$ . Use a frequency step of 20 Hz between a range of 20 and 1000 Hz; in addition, specify five evenly spaced excitation frequencies between the half power points of each resonant frequency between the range of 20-1000 Hz.

- **Problem Description Continued**

- The figures below show the finite element representation of the flat plate and the loads and boundary condition.

### Loads and Boundary Condition



### Elements and Grid Coordinates

45	46	47	48	49	50	51	52	53	54	55
31	32	33	34	35	36	37	38	39	40	44
34	35	36	37	38	39	40	41	42	43	44
21	22	23	24	25	26	27	28	29	30	33
23	24	25	26	27	28	29	30	31	32	33
11	12	13	14	15	16	17	18	19	20	22
12	13	14	15	16	17	18	19	20	21	22
1	2	3	4	5	6	7	8	9	10	11
1	2	3	4	5	6	7	8	9	10	11

TIP  
↓

- **Suggested Steps**

1. Open and review the input file wkshp7.dat
2. Add Executive Control command for modal response solution sequence.
3. Add the XY Plot commands to graph the displacement transient response.
4. Add the other Case Control commands
  - METHOD
  - FREQUENCY
  - SDAMPING
5. Add the eigenvalue method
6. Add the modal damping.
7. Add the pressure load.
8. Add the point load.
9. Add the combined loads.
10. Add frequency of load application.
11. Save and run the new input file in MSC Nastran.
12. Review the MSC Nastran results using the solution file soln7.f06.
13. Review the graph results.

# Step 1. Open and Review the Input File wkshp7.dat

The file wkshp7.dat is the starting input file to be modified.

```
$
$ wkshp7.dat
$
$ executive control add : modal frequency response solution sequence
$
$ case control, add : eigenvalue callout
$ frequency selection
$ modal damping selection
$ xyplot commands
$
$ bulk data, add : eigenvalue method
$ modal damping
$ loading
$ frequencies of load application
$
$
$ CEND
$ TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
$ SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
$ ECHO = UNSORTED
$ SEALL = ALL
$ SPC = 1
$ SET 111 = 11, 33, 55
$ DISPLACEMENT(PHASE, PLOT) = 111
$ SUBCASE 1
$ DLOAD = 400
$
$ OUTPUT (XYPLOT)
$
$ BEGIN BULK
$ PARAM,COUPMASS,1
$ PARAM,WTMASS,0.00259
$ PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
$ INCLUDE 'plate.bdf'
$
$ ENDDATA
```

## Step 2. Add Executive Control Command

Change the file name to **soln7.dat** and add the modal response solution sequence, **SOL 111**

```
$
$   soln7.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
ECHO = UNSORTED
SEALL = ALL
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE,PLOT ) = 111
SUBCASE 1
DLOAD = 400
OUTPUT (XYPLOT)
$
BEGIN BULK
PARAM,COUPMASS,1
PARAM,WTMASS,0.00259
PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
ENDDATA
```

# Step 3. Add the XY Plot Commands for Graph

Add the **XYPLOT** commands to graph the displacement response at **Grid points 11, 33, and 55**, as shown to the right.

```
$
$   soln7.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
ECHO = UNSORTED
SEALL = ALL
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE,PLOT ) = 111
SUBCASE 1
DLOAD = 400
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM,COUPMASS,1
PARAM,WTMASS,0.00259
PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
ENDDATA
```

# Step 4. Add Other Case Control Commands

You will need the following additional case control commands

- **METHOD** – eigenvalue callout
- **FREQUENCY** – frequency selection
- **SDAMPING** – modal damping selection

```
$
$   soln7.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
ECHO = UNSORTED
SEALL = ALL
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE,PLOT ) = 111
$
METHOD = 100
FREQUENCY = 200
SDAMPING = 300
$
SUBCASE 1
DLOAD = 400
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM,COUPMASS,1
PARAM,WTMASS,0.00259
PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
ENDDATA
```

# Step 5. Add Eigenvalue Method

To add the eigenvalue Method:

- a. Use the **EIGRL** entry with a frequency range of interest from **10 to 2000**.
- b. Make sure that the **METHOD** Case Control command identification number matches the **EIGRL** SID.

```
$
$   soln7.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
ECHO = UNSORTED
SEALL = ALL
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE,PLOT) = 111
$
METHOD = 100
FREQUENCY = 200
SDAMPING = 300
$
SUBCASE 1
DLOAD = 400
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM,COUPMASS,1
PARAM,WTMASS,0.00259
PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, 10., 2000.
$
ENDDATA
```

a

b

# Step 6. Add Modal Damping

To add the modal damping:

- a. Use the **TABDMP1** entry and the given information on page WS-3
  - TID = **300** (note must match identification number from SDAMPING in Case Control)
  - Type = **CRIT**
  - First Natural Freq. = **0.0**
  - Damping Value = **.03**
  - Last Natural Freq. = **10.0** (see note below)
  - Damping Value = **.03**

Tables in MSC Nastran are extrapolated. Since in this case, the table represents a straight line, then any two points on that line will work.

```
$
$   soln7.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
ECHO = UNSORTED
SEALL = ALL
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE,PLOT ) = 111
$
METHOD = 100
FREQUENCY = 200
SDAMPING = 300
$
SUBCASE 1
DLOAD = 400
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM,COUPMASS,1
PARAM,WTMASS,0.00259
PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, 10., 2000.
$
$ SPECIFY MODAL DAMPING
$
TABDMP1 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
ENDDATA
```

a

# Step 7. Add the Pressure Load

Add the 0.1 psi pressure load over the total surface of the plate.

- a. Use a **RLOAD2** entry in combination with a **PLOAD2** and **TABLED1** entries.
- b. For the **PLOAD2** entry, apply the pressure load of .1 psi over the elements of the plate. (1 through 40)
- c. The **TABLED1** entry specifies the scale factor to be applied to the **PLOAD2** which then defines the load as .1 psi for all frequencies.

```
$
$   so1n7.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
ECHO = UNSORTED
SEALL = ALL
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE,PLOT ) = 111
$
METHOD = 100|
FREQUENCY = 200
SDAMPING = 300
$
SUBCASE 1
DLOAD = 400
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM,COUPMASS,1
PARAM,WTMASS,0.00259
PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, 10., 2000.
$
$ SPECIFY MODAL DAMPING
$
TABDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
$ APPLY PRESSURE LOAD
$
RLOAD2, 600, 300, , , ,310
$
PLOAD2, 300, .1, 1, THRU, 40
$
TABLED1, 310,
, 10., 1., 1000., 1., ENDT
$
ENDDATA
```

a  
b  
c

# Step 8. Add the Point Load

Apply the 1 lb point load at the corner of the tip of the plate at grid point 11, lagging 45°.

- Use the **RLOAD2** entry in combination with the **FORCE** entry, and the **TABLED1** entry already defined from previous step.
- For the **FORCE** entry, note that the **1 lb** force is applied at grid point **11** in the **Z** direction.

```
$
$ soln7.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
ECHO = UNSORTED
SEALL = ALL
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE,PLOT ) = 111
$
METHOD = 100
FREQUENCY = 200
SDAMPING = 300
$
SUBCASE 1
DLOAD = 400
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM,COUPMASS,1
PARAM,WTMASS,0.00259
PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, 10., 2000.
$
$ SPECIFY MODAL DAMPING
$
TABDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
$ APPLY PRESSURE LOAD
$
RLOAD2, 600, 300, , ,310
$
PLOAD2, 300, .1, 1, THRU, 40
$
TABLED1, 310,
, 10., 1., 1000., 1., ENDT
$
$ POINT LOAD
$
RLOAD2, 500, 600, , -45., 310
$
FORCE,600,11,,1.0,,1.0
$
ENDDATA
```

a

b

# Step 9. Add the Combined Loads

Combine the pressure and point loads using a DLOAD entry.

- For the **DLOAD** entry, define the scale as **1.0** for both loads.
- Make sure the **DLOAD** Case Control command identification matches the SID for the **DLOAD** entry in the Bulk Data section.

```
METHOD = 10
FREQUENCY = 200
SDAMPING = 300
$
SUBCASE 1
DLOAD = 400
OUTPUT (XY,PLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
PARAM,COUPMASS,1
PARAM,WIMASS,0.00259
PARAM,POST,0
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdt'
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, 10., 2000.
$
$ SPECIFY MODAL DAMPING
$
TARDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
$ APPLY PRESSURE LOAD
$
RLOAD1, 600, 300, , , 310
$
PLOAD2, 300, .1, 1, THRU, 40
$
TABLED1, D10,
, 10., 1., 1000., 1., ENDT
$
$ POINT LOAD
$
RLOAD2, 100, 600, , -45., 310
$
FORCE, 600, 11., 1.0., 1.0
$
$ COMBINE LOADS
DLOAD, 400, 1., 1., 600, 1.0, 500
$
ENDDATA
```

# Step 10. Add Frequency of Load Application

To add the frequency of the applied load use the **FREQ1** and **FREQ4** entries.

- a. For **FREQ1** entry, from the given information you can obtain:
  - First freq. = **20.0**
  - Frequency incr = **20.0**
  - Number of freq. increments = **49**
- b. For **FREQ4** entry, from the given information you can obtain:
  - Lower bound freq. = **20.0**
  - Upper bound freq = **1000.0**
  - Frequency spread (in this case it is defined as the half power point so it is equal to the damping ratio) = **.03**
  - Number of equally spaced frequencies = **5**
- c. Make sure the **FREQUENCY** Case Control command identification matches the **SID** for the **FREQ1** and **FREQ4** entries in the Bulk Data section.

```
$
$   soln7.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE = USING THE MODAL METHOD WITH LANCZOS
ECHO = UNSORTED
SEALL = ALL
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE,PLOT ) = 111
$
METHOD = 100
FREQUENCY = 200
SDAMPING = 300
$
SUBCASE 1
DLOAD = 400
OUTPUT (XYPLOT)
```

```
$ POINT LOAD
$
RLOAD2, 500, 600, , -45., 310
$
FORCE, 600, 11, 1.0, , 1.0
$
$ COMBINE LOADS
$
DLOAD, 400, 1., 1., 600, 1.0, 500
$
$ SPECIFY FREQUENCY STEPS
$
FREQ1, 200, 20., 20., 49
$
FREQ4, 200, 20., 1000., .03, 5
$
ENDDATA
```

a

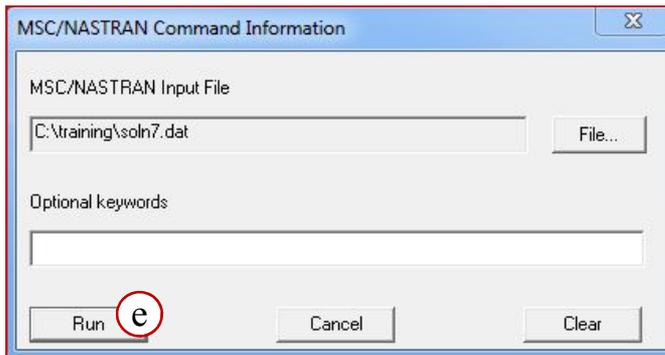
b

c

# Step 11. Save and Run the New Input File

Save and run the modified file in Nastran.

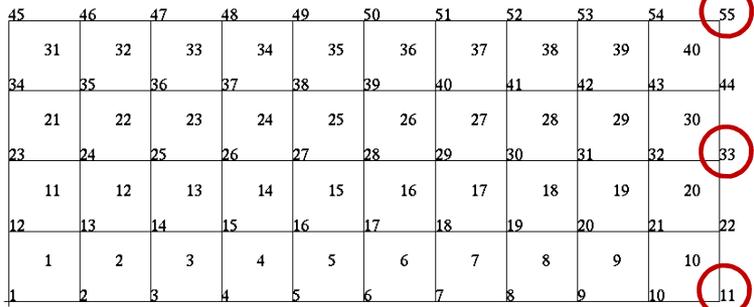
- a. Save the modified file as **soln7.dat**.
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln7.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 12. Review the Results in the Solution File

To see the results open the soln7.f06 file. The three grid points of interest lie along the tip of the plate, grid points 11, 33, 55.

Elements and Grid Coordinates



POINT-ID = 11

COMPLEX DISPLACEMENT VECTOR (MAGNITUDE/PHASE)

FREQUENCY	TYPE	T1	T2	T3	R1	R2	R3
2.000000E+01	G	1.647097E-12	2.530249E-12	1.122426E-02	6.413404E-04	3.278660E-03	2.135831E-12
4.000000E+01	G	1.770529E-12	2.719513E-12	1.199385E-02	6.408463E-04	3.493634E-03	2.295607E-12
6.000000E+01	G	2.022196E-12	3.105392E-12	1.356089E-02	6.394050E-04	3.931127E-03	2.621365E-12
8.000000E+01	G	2.520852E-12	3.869960E-12	1.666288E-02	6.353443E-04	4.797074E-03	3.266812E-12
1.000000E+02	G	3.674820E-12	5.639249E-12	2.383472E-02	6.228433E-04	6.799188E-03	4.760444E-12
1.200000E+02	G	8.109221E-12	1.243798E-11	5.136045E-02	5.649114E-04	1.448202E-02	1.049993E-11
1.296785E+02	G	1.976612E-11	3.030912E-11	1.235303E-01	4.691308E-04	3.460300E-02	2.558679E-11

POINT-ID = 33

COMPLEX DISPLACEMENT VECTOR (MAGNITUDE/PHASE)

FREQUENCY	TYPE	T1	T2	T3	R1	R2	R3
2.000000E+01	G	3.563233E-13	2.526298E-12	1.060259E-02	6.005725E-04	3.091645E-03	1.995002E-12
4.000000E+01	G	8.827738E-13	2.715289E-12	1.187102E-02	6.018661E-04	3.306011E-03	2.141321E-12
6.000000E+01	G	4.366947E-13	3.100613E-12	1.293688E-02	6.040240E-04	3.742584E-03	2.448646E-12
8.000000E+01	G	5.435219E-13	3.864083E-12	1.603816E-02	6.071010E-04	4.606856E-03	3.051621E-12
1.000000E+02	G	7.907077E-13	5.630832E-12	2.321236E-02	6.110976E-04	6.605485E-03	4.446970E-12
1.200000E+02	G	1.740441E-12	1.241982E-11	5.076776E-02	6.160660E-04	1.427831E-02	9.808802E-12
1.296785E+02	G	4.236551E-12	3.026598E-11	1.251536E-01	6.188346E-04	3.440506E-02	2.390300E-11

POINT-ID = 55

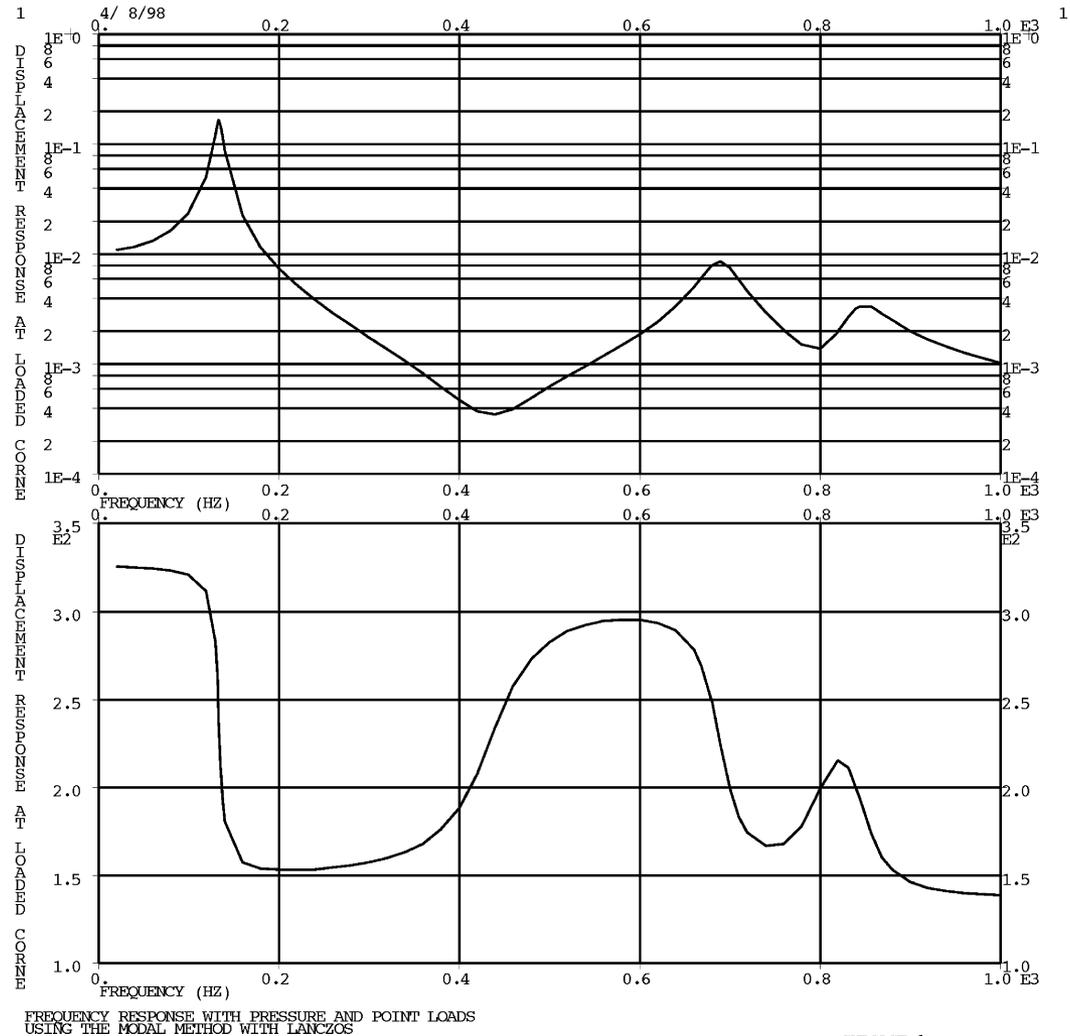
COMPLEX DISPLACEMENT VECTOR (MAGNITUDE/PHASE)

FREQUENCY	TYPE	T1	T2	T3	R1	R2	R3
2.000000E+01	G	2.299816E-12	2.628330E-12	1.003391E-02	5.635860E-04	3.021529E-03	2.074214E-12
4.000000E+01	G	2.471567E-12	2.824902E-12	1.079900E-02	5.666141E-04	3.235939E-03	2.229382E-12
6.000000E+01	G	2.822038E-12	3.225862E-12	1.235921E-02	5.723090E-04	3.672785E-03	2.545743E-12
8.000000E+01	G	3.516244E-12	4.020195E-12	1.545119E-02	5.823869E-04	4.537677E-03	3.172572E-12
1.000000E+02	G	5.122886E-12	5.858366E-12	2.260797E-02	6.027246E-04	6.538016E-03	4.623119E-12
1.200000E+02	G	1.129556E-11	1.292180E-11	5.011685E-02	6.704431E-04	1.421915E-02	1.019705E-11
1.296785E+02	G	2.752108E-11	3.148883E-11	1.224666E-01	8.095592E-04	3.437928E-02	2.484872E-11

# Step 13. Review the Graph Results

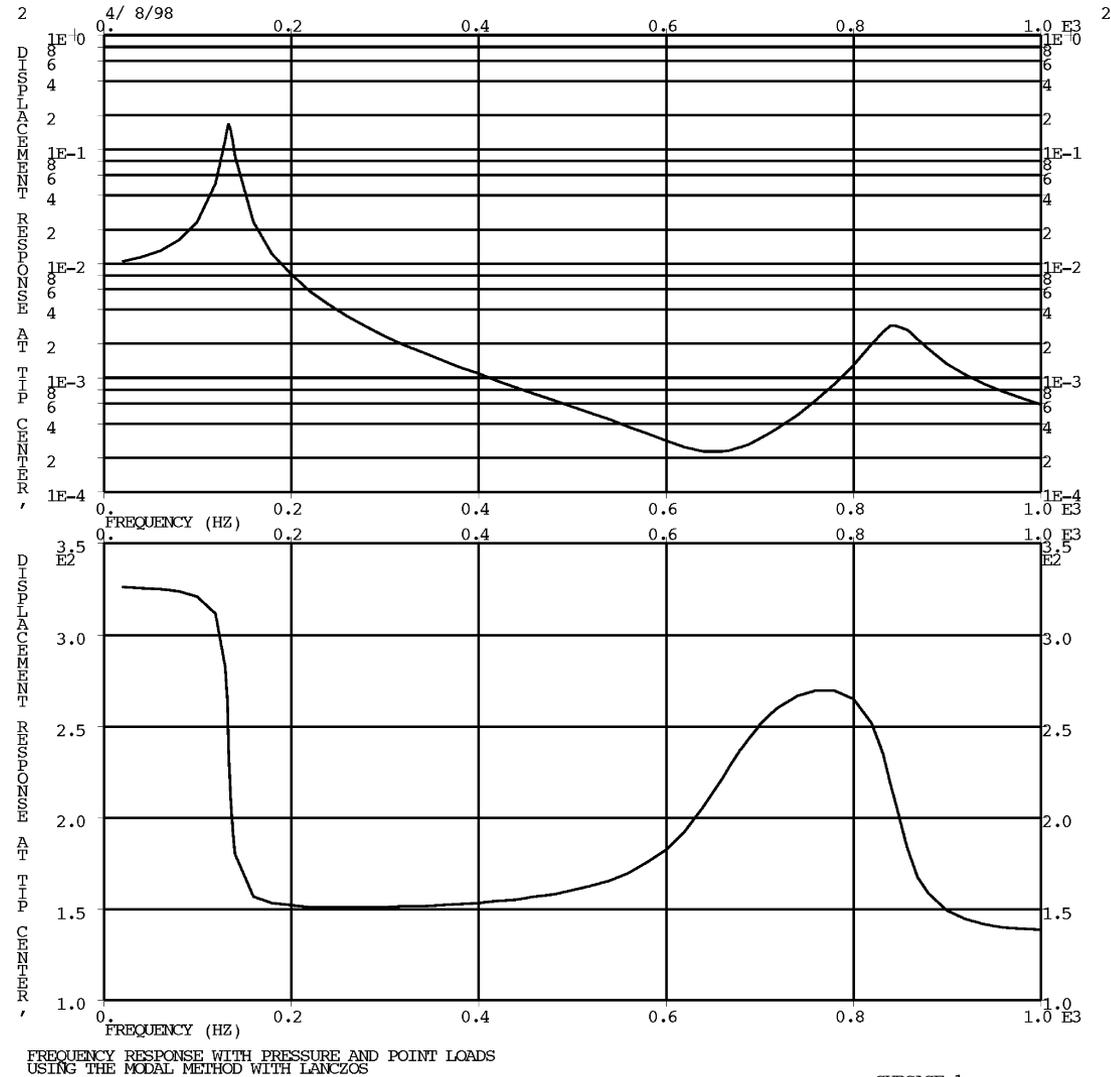
Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions given in workshop 4, step 9

Review the displacement response graph at the loaded corner. (grid point 11)



# Step 13. Review the Graph Results (Cont.)

Review the displacement response graph at the center of the tip of the plate. (grid 33)

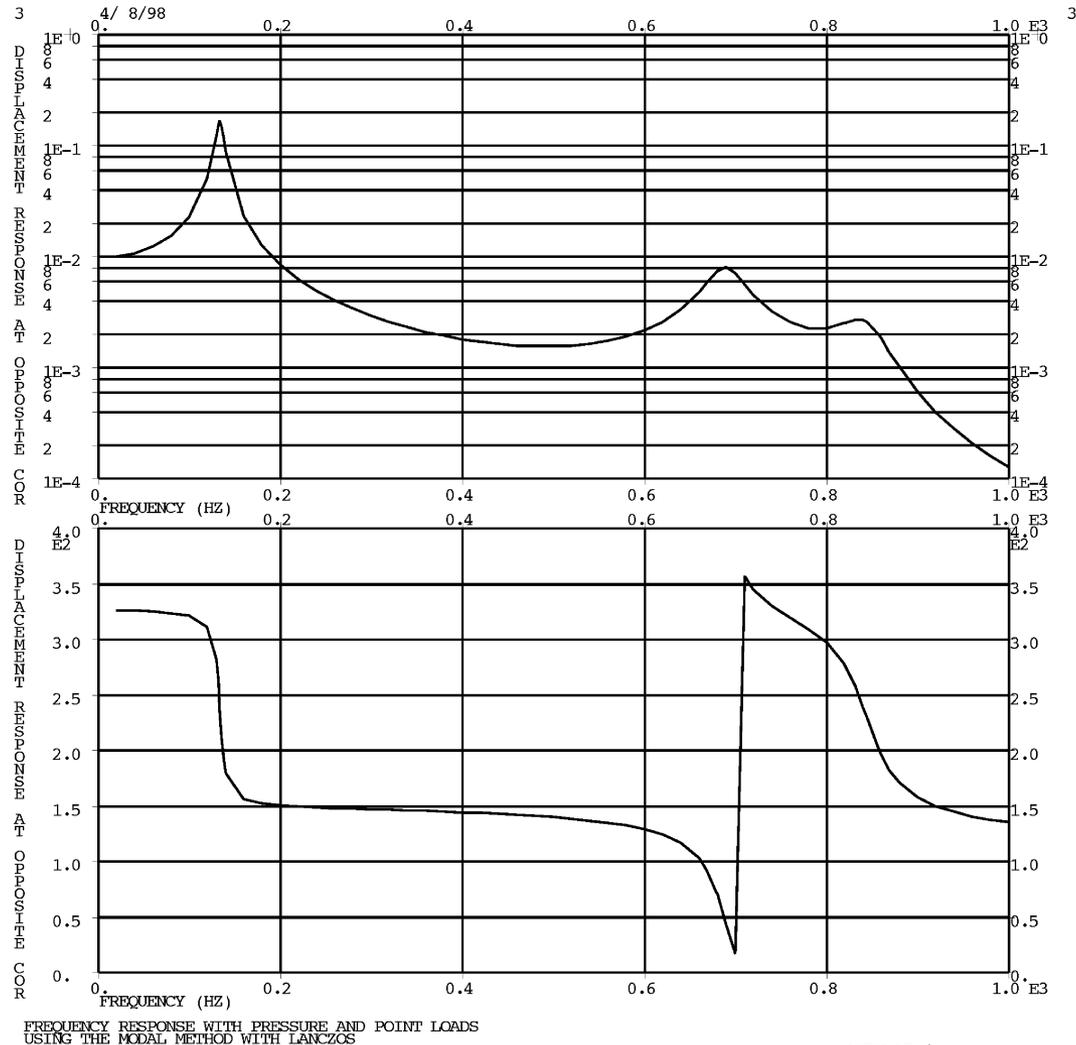


FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS  
USING THE MODAL METHOD WITH LANCZOS

SUBCASE 1

# Step 13. Review the Graph Results (Cont.)

Review the displacement response graph at the opposite corner of the point load. (grid point 55)



# **WORKSHOP 8A**

## **DIRECT TRANSIENT RESPONSE WITH ENFORCED ACCELERATION**



- **Workshop Objective**

- Using the direct method, determine the transient response of the flat plate (from workshop 1) due to the acceleration sine pulse described below.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

- Plate.bdf
- Wkshp8a.dat

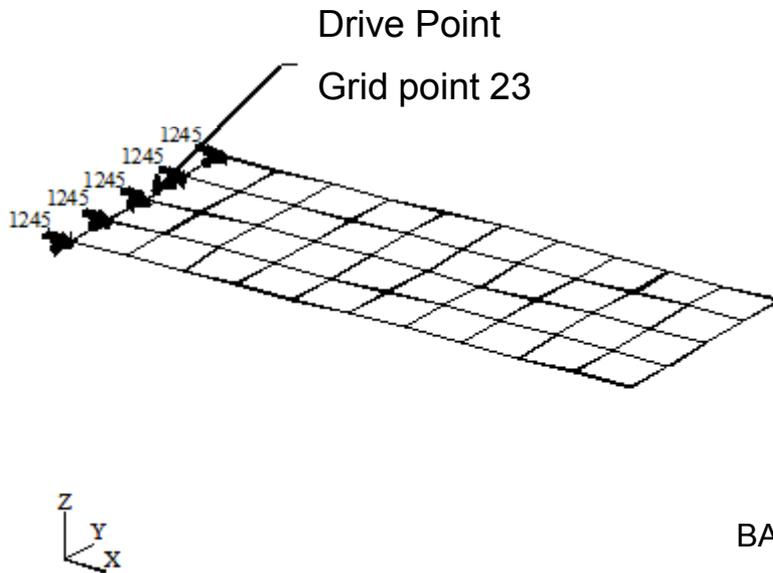
- **Problem Description**

- The unit acceleration sine pulse of 250 Hz is applied at the base in the z-direction for .004 seconds. Use a structural damping coefficient of  $g = 0.06$  and convert this damping to equivalent viscous damping at 250 Hz.

- **Problem Description Continued:**

- The figures below show the finite element representation of the flat plate and the loads and boundary condition

Load and Boundary Condition



Elements and Grid Coordinates

	45	46	47	48	49	50	51	52	53	54	55	
	31	32	33	34	35	36	37	38	39	40		
	34	35	36	37	38	39	40	41	42	43	44	
	21	22	23	24	25	26	27	28	29	30		
BASE	23	24	25	26	27	28	29	30	31	32	33	TIP
	11	12	13	14	15	16	17	18	19	20		
	12	13	14	15	16	17	18	19	20	21	22	
	1	2	3	4	5	6	7	8	9	10		
	1	2	3	4	5	6	7	8	9	10	11	

- **Suggested Steps**

1. Open and review the input file wkshp8A.dat
2. Add conversion to viscous damping.
3. Add boundary condition.
4. Add the sinusoidal acceleration.
5. Apply enforced motion to the base of plate.
6. Save and run the new input file in MSC Nastran.
7. Review the MSC Nastran result using the solution file soln8a.f06.
8. Review the graph results.

# Step 1. Open and Review Input File wkshp8A.dat

The file wkshp8A.dat is the starting input file to be modified.

The following information is already included in the input file.

- Output acceleration graph at grid point 23, and output displacement graphs at points 23 and 33.
- Parameters
  - ENFMETH – sets solution to REL
  - ENFMOTN – sets the output to ABS
- Structural damping
- Integration time step

```

$
$ wkshp8A.dat
$
$ add      :      conversion from structural to viscous damping
$          :      boundary conditions at left end
$          :      rbe2 for left edge in the vertical direction
$          :      loading and enforced motion
$
SOL 109
CEND
TITLE = TRANSIENT RESPONSE WITH ENFORCED MOTION
SUBTITLE = USING DIRECT TRANSIENT METHOD
ECHO = UNSORTED
SPC = 200
SET 111 = 23, 33
SET 1000 = 23
SPCF = 1000
DISPLACEMENT (SORT2) = 111
VELOCITY (SORT2) = 111
ACCELERATION (SORT2) = 111
SUBCASE 1
DLOAD = 500
TSTEP = 100
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= BASE ACCELERATION
XYPLOT ACCELERATION RESPONSE / 23 (T3)
YTITLE= BASE DISPLACEMENT
XYPLOT DISP RESPONSE / 23 (T3)
YTITLE= TIP CENTER DISPLACEMENT RESPONSE
XYPLOT DISP RESPONSE / 33 (T3)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM POST 0
PARAM ENFMETH REL
PARAM ENFMOTN ABS
PARAM COUPHASS 1
PARAM WTMASS 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM G 0.06
$
$ SPECIFY INTEGRATION TIME STEP
$
TSTEP 100, 200, 2.0E-4, 1
$
ENDDATA

```

# Step 2. Add damping Conversion

Add the appropriate parameter in the Bulk Data section for converting to viscous damping.

- a. First rename the input file as **soln8A.dat**.
- b. Use **PARAM W3**, for the value of this parameter, convert 250 Hz to radians/sec.

```
$
$ soln8A.dat a
$
SOL 109
CEND
TITLE = TRANSIENT RESPONSE WITH ENFORCED MOTION
SUBTITLE = USING DIRECT TRANSIENT METHOD
ECHO = UNSORTED
SPC = 200
SET 111 = 23, 33
SET 1000 = 23
SPCF = 1000
DISPLACEMENT (SORT2) = 111
VELOCITY (SORT2) = 111
ACCELERATION (SORT2) = 111
SUBCASE 1
DLOAD = 500
TSTEP = 100
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= BASE ACCELERATION
XYPLOT ACCELERATION RESPONSE / 23 (T3)
YTITLE= BASE DISPLACEMENT
XYPLOT DISP RESPONSE / 23 (T3)
YTITLE= TIP CENTER DISPLACEMENT RESPONSE
XYPLOT DISP RESPONSE / 33 (T3)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENFMETH, REF
PARAM, ENFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$ ADD CONVERSION TO VISCOUS DAMPING
$
b PARAM, W3, 1571.
$
ENDDATA
```

# Step 3. Add Boundary Condition

To apply the base constraint:

- a. Use **SPC1** to constrain the base of the plate in the X, Y directions and all rotations. Apply constraint at grid points **1, 12, 23, 34, 45**
- b. Use **SPC1** to constrain grid point **23** in the Z (3) direction.

```
$
$   soln8A.dat
$
SOL 109
CEND
TITLE = TRANSIENT RESPONSE WITH ENFORCED MOTION
SUBTITLE = USING DIRECT TRANSIENT METHOD
ECHO = UNSORTED
SPC = 200
SET 111 = 23, 33
SET 1000 = 23
SPCF = 1000
DISPLACEMENT (SORT2) = 111
VELOCITY (SORT2) = 111
ACCELERATION (SORT2) = 111
SUBCASE 1
DLOAD = 500
TSTEP = 100
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= BASE ACCELERATION
XYPLOT ACCELERATION RESPONSE / 23 (T3)
YTITLE= BASE DISPLACEMENT
XYPLOT DISP RESPONSE / 23 (T3)
YTITLE= TIP CENTER DISPLACEMENT RESPONSE
XYPLOT DISP RESPONSE / 33 (T3)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM,POST,0
PARAM,ENFMETH,REL
PARAM,ENFMOTN,ABS
PARAM,COUPMASS,1
PARAM,WTMASS,0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM,G,0.06
$
$ ADD CONVERSION TO VISCOUS DAMPING
$
PARAM,W3,1571.
$
$ APPLY EDGE CONSTRAINTS
a SPC1,200,12456,1,12,23,34,45
$
b SPC1,200,3,23
$
$ SPECIFY INTEGRATION TIME STEP
$
TSTEP,100,200,2.0E-4,1
$
ENDDATA
```

# Step 4. Add the Sinusoidal Acceleration

Apply the unit acceleration sine pulse of 250 Hz at the base (grid point 23) of the plate in the z-direction for .004 seconds.

- Use a **TLOAD2** entry in combination with a **SPCD** entry and the given information obtain:
  - Type = **A**, Enforced acceleration using a large mass.
  - Time = **0 to .004 secs**
  - Frequency = **250 HZ**
  - Phase angle = **-90**
- Make sure that the **DLOAD** Case Command identification number matches the SID for the **TLOAD2**
- For the **SPCD**, apply the unit acceleration pulse at grid point **23**, in the Z (**3**) direction.

```

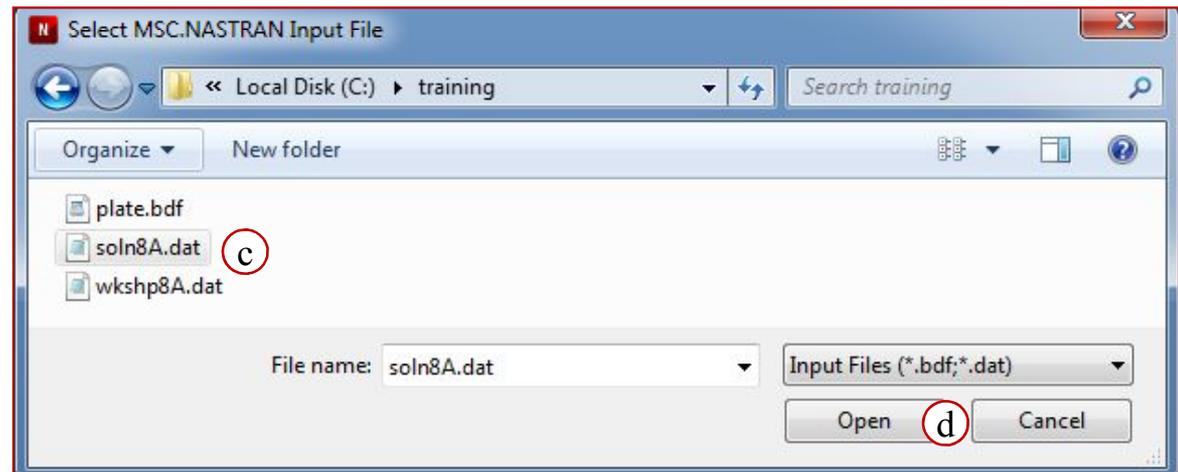
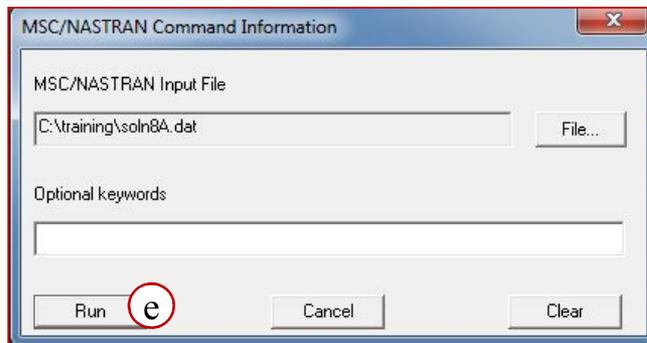
$
$   soln8A.dat
$
SOL 109
CEND
TITLE = TRANSIENT RESPONSE WITH ENFORCED MOTION
SUBTITLE = USING DIRECT TRANSIENT METHOD
ECHO = UNSORTED
SPC = 200
SET 111 = 23, 33
SET 1000 = 23
SPCF = 1000
DISPLACEMENT (SORT2) = 111
VELOCITY (SORT2) = 111
ACCELERATION (SORT2) = 111
SUBCASE 1
DLOAD = 500
TSTEP = 100
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= BASE ACCELERATION
XYPLOT ACCELERATION RESPONSE / 23 (T3)
VTITLE= BASE DISPLACEMENT
XYPLOT DISP RESPONSE / 23 (T3)
VTITLE= TIP CENTER DISPLACEMENT RESPONSE
XYPLOT DISP RESPONSE / 33 (T3)
$
BEGIN BULK
$
$   PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENPMETH, REL
PARAM, ENPMOTN, ABS
PARAM, COMPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$ ADD CONVERSION TO VISCOUS DAMPING
$
PARAM, W3, 1571.
$
$ APPLY EDGE CONSTRAINTS
$
SPC1, 200, 12456, 1, 12, 23, 34, 45
$
SPC1, 200, 3, 23
$
$ APPLY ACCELERATION TO THE BASE
$
TLOAD2, 500, 600, , A, 0.0, 0.004, 250., -90.
$
SPCD, 600, 23, 3, 1.0
$
$ SPECIFY INTEGRATION TIME STEPS
$
TSTEP, 100, 200, 2.0E-4, 1
$
ENDDATA

```

# Step 6. Save and Run the New Input File

Save and run the modified file in MSC Nastran.

- a. Save the modified file as **soln8A.dat**
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln8A.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 7. Review the Results in the Solution File

## Displacement

### Elements and Grid Coordinates

45	46	47	48	49	50	51	52	53	54	55
	31	32	33	34	35	36	37	38	39	40
34	35	36	37	38	39	40	41	42	43	44
	21	22	23	24	25	26	27	28	29	30
23	24	25	26	27	28	29	30	31	32	33
	11	12	13	14	15	16	17	18	19	20
12	13	14	15	16	17	18	19	20	21	22
	1	2	3	4	5	6	7	8	9	10
1	2	3	4	5	6	7	8	9	10	11

BASE

TIP

POINT-ID = 23

TIME	TYPE	T1	T2	T3	R1	R2	R3
0.000000E+00	G	0.0	0.0	0.0	0.0	0.0	0.0
2.000000E-04	G	0.0	0.0	2.060113E-09	0.0	0.0	0.0
4.000000E-04	G	0.0	0.0	1.627925E-08	0.0	0.0	0.0
6.000000E-04	G	0.0	0.0	5.362621E-08	0.0	0.0	0.0
8.000000E-04	G	0.0	0.0	1.228059E-07	0.0	0.0	0.0
9.999999E-04	G	0.0	0.0	2.294072E-07	0.0	0.0	0.0
1.200000E-03	G	0.0	0.0	3.753559E-07	0.0	0.0	0.0
1.400000E-03	G	0.0	0.0	5.587263E-07	0.0	0.0	0.0
1.600000E-03	G	0.0	0.0	7.739294E-07	0.0	0.0	0.0
1.800000E-03	G	0.0	0.0	1.012260E-06	0.0	0.0	0.0
2.000000E-03	G	0.0	0.0	1.262750E-06	0.0	0.0	0.0
2.200000E-03	G	0.0	0.0	1.513240E-06	0.0	0.0	0.0
2.400000E-03	G	0.0	0.0	1.751571E-06	0.0	0.0	0.0
2.600000E-03	G	0.0	0.0	1.966774E-06	0.0	0.0	0.0
2.800000E-03	G	0.0	0.0	2.150145E-06	0.0	0.0	0.0

POINT-ID = 33

TIME	TYPE	T1	T2	T3	R1	R2	R3
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0
2.000000E-04	G	0.0	0.0	-2.229395E-09	2.413720E-22	-5.655525E-11	0.0
4.000000E-04	G	0.0	0.0	-5.930439E-09	1.053352E-21	6.027918E-10	0.0
6.000000E-04	G	0.0	0.0	-1.557731E-08	3.079468E-21	5.724111E-09	0.0
8.000000E-04	G	0.0	0.0	-3.867503E-08	8.723578E-21	2.287048E-08	0.0
9.999999E-04	G	0.0	0.0	-8.154096E-08	2.808527E-20	5.995565E-08	0.0
1.200000E-03	G	0.0	0.0	-1.436685E-07	4.443902E-20	1.196107E-07	0.0
1.400000E-03	G	0.0	0.0	-2.157785E-07	3.702584E-20	1.970543E-07	0.0
1.600000E-03	G	0.0	0.0	-2.828655E-07	5.992170E-20	2.830783E-07	0.0
1.800000E-03	G	0.0	0.0	-3.288824E-07	7.642774E-20	3.683107E-07	0.0
2.000000E-03	G	0.0	0.0	-3.397712E-07	2.771064E-20	4.454396E-07	0.0
2.200000E-03	G	0.0	0.0	-3.040933E-07	9.048426E-20	5.092124E-07	0.0
2.400000E-03	G	0.0	0.0	-2.120215E-07	1.744754E-19	5.550235E-07	0.0
2.600000E-03	G	0.0	0.0	-5.429651E-08	2.250147E-19	5.773276E-07	0.0
2.800000E-03	G	0.0	0.0	1.770632E-07	2.875243E-19	5.697529E-07	0.0
3.000000E-03	G	0.0	0.0	4.861163E-07	3.340001E-19	5.273725E-07	0.0
3.200000E-03	G	0.0	0.0	8.702826E-07	2.800557E-19	4.492456E-07	0.0

# Step 7. Review the Results in the Solution File (Cont.)

## Velocity

POINT-ID = 23

VELOCITY VECTOR							
TIME	TYPE	T1	T2	T3	R1	R2	R3
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0
2.000000E-04	G	0.0	0.0	3.090170E-05	0.0	0.0	0.0
4.000000E-04	G	0.0	0.0	1.205819E-04	0.0	0.0	0.0
6.000000E-04	G	0.0	0.0	2.602621E-04	0.0	0.0	0.0
8.000000E-04	G	0.0	0.0	4.362695E-04	0.0	0.0	0.0
9.999999E-04	G	0.0	0.0	6.313751E-04	0.0	0.0	0.0
1.200000E-03	G	0.0	0.0	8.264808E-04	0.0	0.0	0.0
1.400000E-03	G	0.0	0.0	1.002488E-03	0.0	0.0	0.0
1.600000E-03	G	0.0	0.0	1.142168E-03	0.0	0.0	0.0
1.800000E-03	G	0.0	0.0	1.231849E-03	0.0	0.0	0.0
2.000000E-03	G	0.0	0.0	1.262750E-03	0.0	0.0	0.0
2.200000E-03	G	0.0	0.0	1.231849E-03	0.0	0.0	0.0
2.400000E-03	G	0.0	0.0	1.142168E-03	0.0	0.0	0.0
2.600000E-03	G	0.0	0.0	1.002488E-03	0.0	0.0	0.0
2.800000E-03	G	0.0	0.0	8.264808E-04	0.0	0.0	0.0
3.000000E-03	G	0.0	0.0	6.313752E-04	0.0	0.0	0.0
3.200000E-03	G	0.0	0.0	4.362696E-04	0.0	0.0	0.0
3.400000E-03	G	0.0	0.0	2.602622E-04	0.0	0.0	0.0
3.600000E-03	G	0.0	0.0	1.205820E-04	0.0	0.0	0.0
3.800000E-03	G	0.0	0.0	3.090173E-05	0.0	0.0	0.0
4.000000E-03	G	0.0	0.0	7.582639E-18	0.0	0.0	0.0
4.200000E-03	G	0.0	0.0	-1.587265E-11	0.0	0.0	0.0
4.400000E-03	G	0.0	0.0	-1.587265E-11	0.0	0.0	0.0
4.600000E-03	G	0.0	0.0	-1.587265E-11	0.0	0.0	0.0
4.800000E-03	G	0.0	0.0	-1.587265E-11	0.0	0.0	0.0
5.000000E-03	G	0.0	0.0	-1.587265E-11	0.0	0.0	0.0

## Acceleration

POINT-ID = 23

ACCELERATION VECTOR							
TIME	TYPE	T1	T2	T3	R1	R2	R3
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0
2.000000E-04	G	0.0	0.0	6.123234E-17	0.0	0.0	0.0
4.000000E-04	G	0.0	0.0	3.090170E-01	0.0	0.0	0.0
6.000000E-04	G	0.0	0.0	5.877852E-01	0.0	0.0	0.0
8.000000E-04	G	0.0	0.0	8.090170E-01	0.0	0.0	0.0
9.999999E-04	G	0.0	0.0	9.510565E-01	0.0	0.0	0.0
1.200000E-03	G	0.0	0.0	1.000000E+00	0.0	0.0	0.0
1.400000E-03	G	0.0	0.0	9.510565E-01	0.0	0.0	0.0
1.600000E-03	G	0.0	0.0	8.090170E-01	0.0	0.0	0.0
1.800000E-03	G	0.0	0.0	5.877853E-01	0.0	0.0	0.0
2.000000E-03	G	0.0	0.0	3.090171E-01	0.0	0.0	0.0
2.200000E-03	G	0.0	0.0	7.936330E-08	0.0	0.0	0.0
2.400000E-03	G	0.0	0.0	-3.090169E-01	0.0	0.0	0.0
2.600000E-03	G	0.0	0.0	-5.877852E-01	0.0	0.0	0.0
2.800000E-03	G	0.0	0.0	-8.090169E-01	0.0	0.0	0.0
3.000000E-03	G	0.0	0.0	-9.510565E-01	0.0	0.0	0.0
3.200000E-03	G	0.0	0.0	-1.000000E+00	0.0	0.0	0.0
3.400000E-03	G	0.0	0.0	-9.510565E-01	0.0	0.0	0.0
3.600000E-03	G	0.0	0.0	-8.090171E-01	0.0	0.0	0.0
3.800000E-03	G	0.0	0.0	-5.877854E-01	0.0	0.0	0.0
4.000000E-03	G	0.0	0.0	-3.090172E-01	0.0	0.0	0.0
4.200000E-03	G	0.0	0.0	-1.587266E-07	0.0	0.0	0.0
4.400000E-03	G	0.0	0.0	0.0	0.0	0.0	0.0
4.600000E-03	G	0.0	0.0	0.0	0.0	0.0	0.0
4.800000E-03	G	0.0	0.0	0.0	0.0	0.0	0.0
5.000000E-03	G	0.0	0.0	0.0	0.0	0.0	0.0

POINT-ID = 33

VELOCITY VECTOR							
TIME	TYPE	T1	T2	T3	R1	R2	R3
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0
2.000000E-04	G	0.0	0.0	-2.462252E-05	3.638675E-18	1.506980E-06	0.0
4.000000E-04	G	0.0	0.0	-4.170311E-05	7.950396E-18	1.445167E-05	0.0
6.000000E-04	G	0.0	0.0	-8.791599E-05	1.979687E-17	5.566922E-05	0.0
8.000000E-04	G	0.0	0.0	-1.680922E-04	6.284114E-17	1.355789E-04	0.0
9.999999E-04	G	0.0	0.0	-2.624938E-04	8.928861E-17	2.418505E-04	0.0
1.200000E-03	G	0.0	0.0	-3.324108E-04	2.202479E-17	3.427466E-04	0.0
1.400000E-03	G	0.0	0.0	-3.419379E-04	3.808539E-17	4.086690E-04	0.0
1.600000E-03	G	0.0	0.0	-2.744263E-04	9.764959E-17	4.281412E-04	0.0
1.800000E-03	G	0.0	0.0	-1.324679E-04	-8.153294E-17	4.059033E-04	0.0
2.000000E-03	G	0.0	0.0	7.227329E-05	3.408427E-17	3.52542E-04	0.0
2.200000E-03	G	0.0	0.0	3.291708E-04	3.659066E-16	2.739599E-04	0.0
2.400000E-03	G	0.0	0.0	6.328252E-04	3.354710E-16	1.702878E-04	0.0
2.600000E-03	G	0.0	0.0	9.787661E-04	2.820008E-16	3.682334E-05	0.0
2.800000E-03	G	0.0	0.0	1.354215E-03	2.721368E-16	-1.248876E-04	0.0
3.000000E-03	G	0.0	0.0	1.733049E-03	-1.867139E-17	-3.012681E-04	0.0
3.200000E-03	G	0.0	0.0	2.080214E-03	-6.001737E-16	-4.702475E-04	0.0
3.400000E-03	G	0.0	0.0	2.361821E-03	-1.379293E-15	-6.102431E-04	0.0
3.600000E-03	G	0.0	0.0	2.553679E-03	-1.367178E-15	-7.072667E-04	0.0
3.800000E-03	G	0.0	0.0	2.644025E-03	-5.990513E-16	-7.566559E-04	0.0
4.000000E-03	G	0.0	0.0	2.641382E-03	-1.532903E-16	-7.596798E-04	0.0
4.200000E-03	G	0.0	0.0	2.540666E-03	6.165753E-17	-7.206953E-04	0.0
4.400000E-03	G	0.0	0.0	2.346593E-03	5.695914E-17	-6.501650E-04	0.0
4.600000E-03	G	0.0	0.0	2.093832E-03	-2.511450E-16	-5.665186E-04	0.0
4.800000E-03	G	0.0	0.0	1.822495E-03	-6.824969E-16	-4.861337E-04	0.0
5.000000E-03	G	0.0	0.0	1.551111E-03	-1.822495E-03	-4.861337E-04	0.0

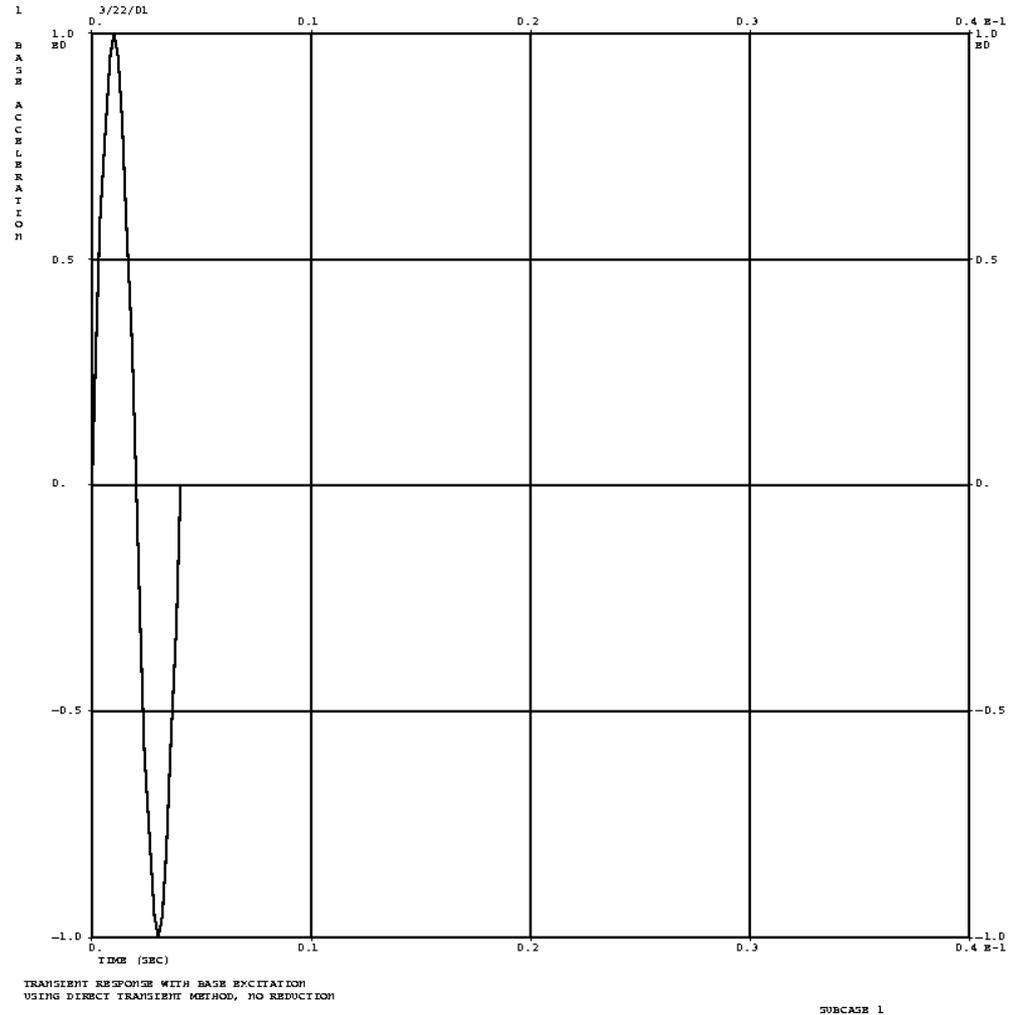
POINT-ID = 33

ACCELERATION VECTOR							
TIME	TYPE	T1	T2	T3	R1	R2	R3
0.0	G	0.0	0.0	0.0	0.0	0.0	0.0
2.000000E-04	G	0.0	0.0	-1.072377E-01	1.131945E-14	-1.413881E-03	0.0
4.000000E-04	G	0.0	0.0	-3.174978E-02	1.374785E-14	1.789756E-02	0.0
6.000000E-04	G	0.0	0.0	-1.390561E-01	2.936936E-14	1.115493E-01	0.0
8.000000E-04	G	0.0	0.0	-3.230727E-01	8.909541E-14	3.006262E-01	0.0
9.999999E-04	G	0.0	0.0	-4.786894E-01	3.413473E-13	4.984702E-01	0.0
1.200000E-03	G	0.0	0.0	-4.652266E-01	-7.687262E-14	5.642461E-01	0.0
1.400000E-03	G	0.0	0.0	-2.340436E-01	-5.957656E-13	4.447148E-01	0.0
1.600000E-03	G	0.0	0.0	1.387729E-01	7.563717E-13	2.145095E-01	0.0
1.800000E-03	G	0.0	0.0	5.363429E-01	-1.607297E-13	-1.978769E-02	0.0
2.000000E-03	G	0.0	0.0	8.832412E-01	-1.631096E-12	-2.025912E-01	0.0
2.200000E-03	G	0.0	0.0	1.164171E+00	-2.787268E-12	-3.358997E-01	0.0
2.400000E-03	G	0.0	0.0	1.404804E+00	5.309538E-13	-4.490427E-01	0.0
2.600000E-03	G	0.0	0.0	1.631741E+00	-8.353122E-13	-5.87684E-01	0.0
2.800000E-03	G	0.0	0.0	1.827669E+00	3.006101E-13	-7.469665E-01	0.0
3.000000E-03	G	0.0	0.0	1.926822E+00	-3.992500E-13	-8.701430E-01	0.0
3.200000E-03	G	0.0	0.0	1.861511E+00	-2.508832E-12	-8.93624E-01	0.0
3.400000E-03	G	0.0	0.0	1.610138E+00	-3.306211E-12	-7.961314E-01	0.0
3.600000E-03	G	0.0	0.0	1.205940E+00	-4.484961E-12	-6.038246E-01	0.0
3.800000E-03	G	0.0	0.0	7.126371E-01	4.606110E-12	-3.664117E-01	0.0
4.000000E-03	G	0.0	0.0	1.908275E-01	3.075157E-12	-1.274805E-01	0.0
4.200000E-03	G	0.0	0.0	-2.172589E-01	1.382454E-12	9.724218E-02	0.0
4.400000E-03	G	0.0	0.0	-7.899043E-01	7.670239E-12	3.926024E-01	0.0
4.600000E-03	G	0.0	0.0	-1.159825E+00	-8.140078E-13	4.125903E-01	0.0
4.800000E-03	G	0.0	0.0	-1.376788E+00	-2.267033E-12	4.257840E-01	0.0
5.000000E-03	G	0.0	0.0	-1.526666E+00	2.946486E-13	3.800555E-01	0.0

# Step 8. Review the Graph Results

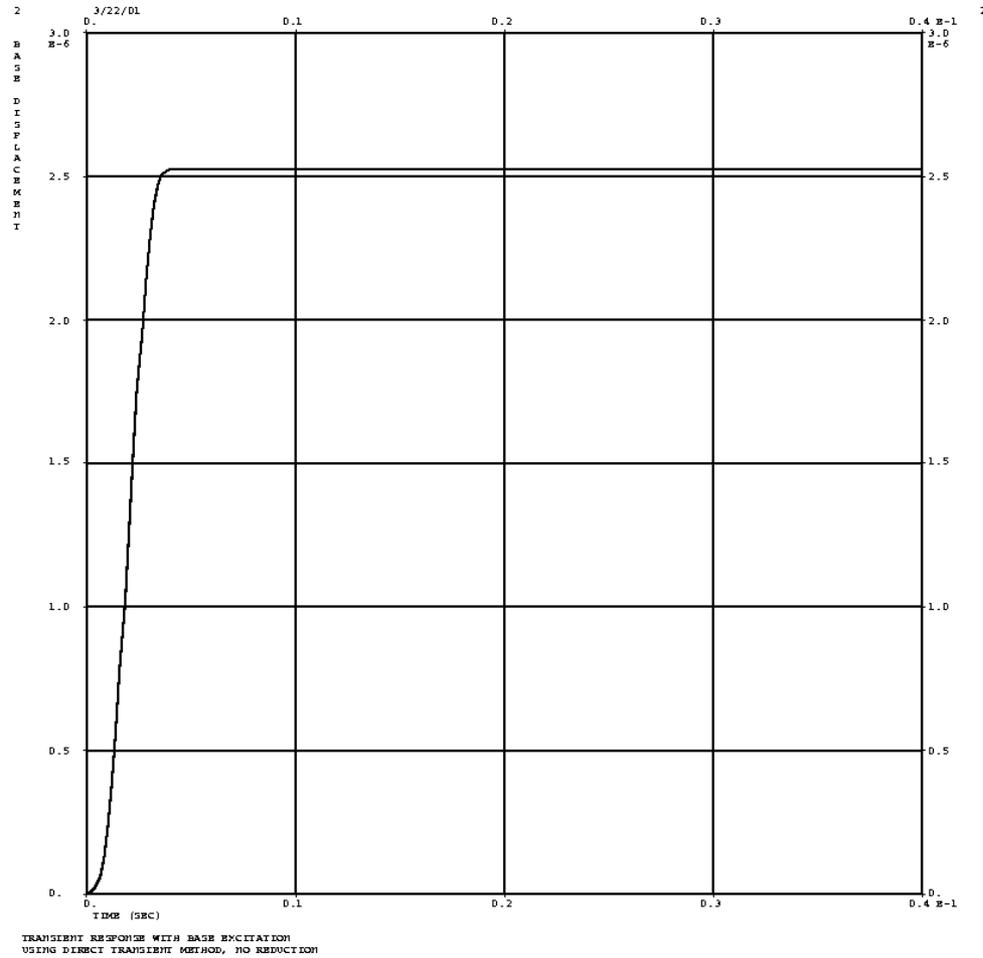
Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions in workshop 4, step 9.

Base acceleration at Grid Point 23



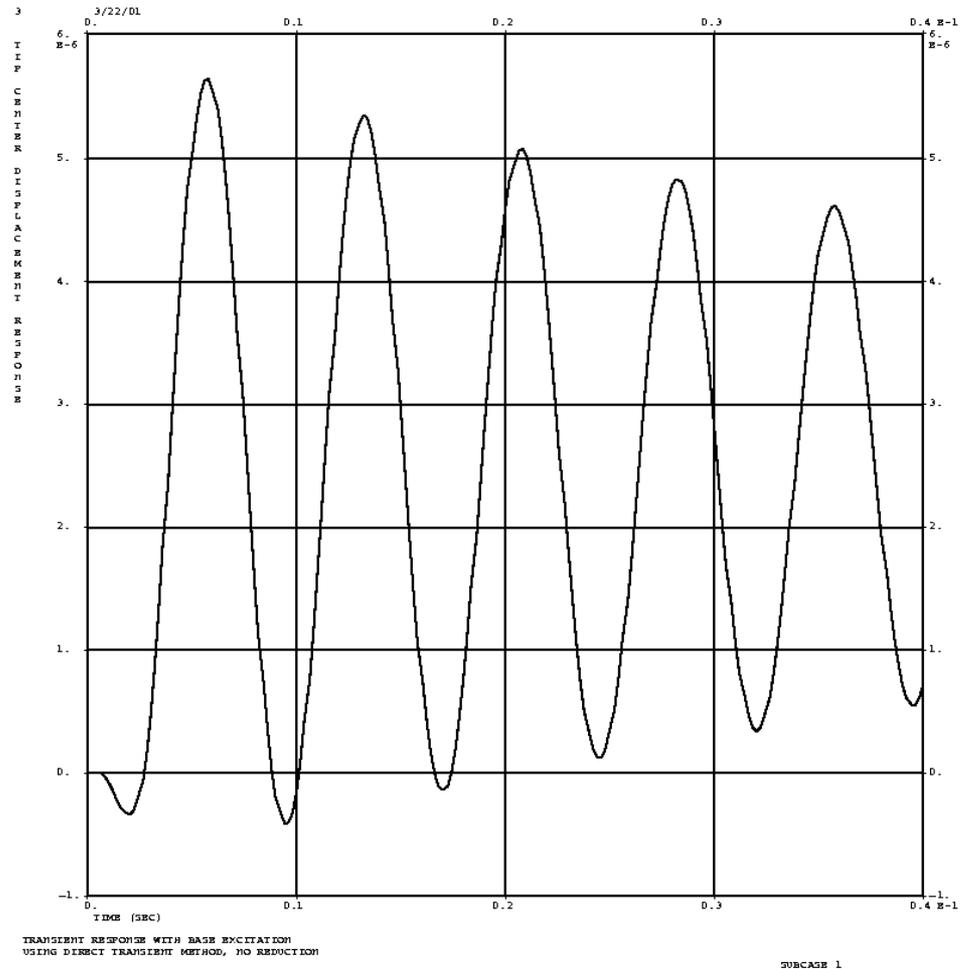
# Step 8. Review the Graph Results (Cont.)

Base displacement at Grid Point 23



# Step 8. Review the Graph Results (Cont.)

Tip displacement at Grid Point 33





# **WORKSHOP 8B**

## **MODAL TRANSIENT RESPONSE WITH ENFORCED ACCELERATION**



- **Workshop Objective**

- Using the modal method, determine the transient response of the flat plate (from workshop 1) due to the acceleration sine pulse described below.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

- Plate.bdf
- Wkshp8b.dat

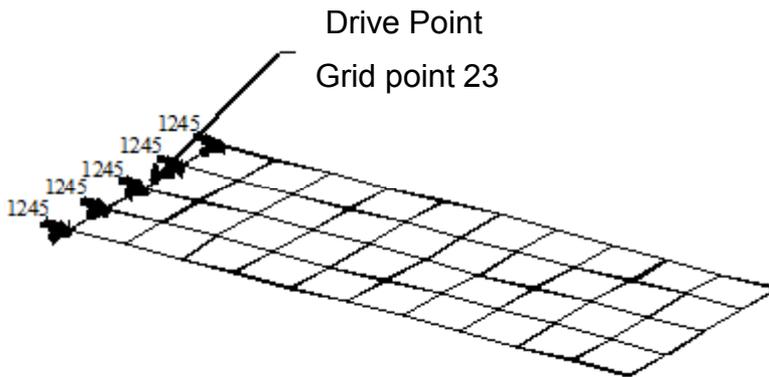
- **Problem Description**

- The unit acceleration sine pulse of 250 Hz is applied at the base in the z-direction for .004 seconds. Use a structural damping coefficient of  $g = 0.06$  and convert this damping to equivalent viscous damping at 250 Hz. Be sure to include residual vectors.

- **Problem Description Continued:**

- The figures below show the finite element representation of the flat plate and the loads and boundary condition.

### Load and Boundary Condition



### Elements and Grid Coordinates

	45	46	47	48	49	50	51	52	53	54	55	
	31	32	33	34	35	36	37	38	39	40		
	34	35	36	37	38	39	40	41	42	43	44	
	21	22	23	24	25	26	27	28	29	30		
BASE	23	24	25	26	27	28	29	30	31	32	33	TIP
	11	12	13	14	15	16	17	18	19	20		
	12	13	14	15	16	17	18	19	20	21	22	
	1	2	3	4	5	6	7	8	9	10		
	1	2	3	4	5	6	7	8	9	10	11	

- **Suggested Steps**

1. Open and review the input file wkshp8B.dat
2. Change the solution to modal transient response, SOL 112.
3. Add option to include residual vectors.
4. Add eigenvalue method.
5. Save and run the new input file in MSC Nastran.
6. Review the MSC Nastran result using the solution file soln8b.f06.
7. Review the graph results.

# Step 1. Open and Review Input File wkshp8B.dat

The file wkshp8b.dat is the starting input file. This is the final input file from workshop 8a. All that is necessary is to change from a direct method to a modal one and to add a case control command for the residual vector option.

```
$
$ wkshp8B.dat
$
$ add: change solution request to SOL112
$ residual vectos
$ eigenvalue method
$
SOL 109
CEND
TITLE = TRANSIENT RESPONSE WITH BASE EXCITATION
SUBTITLE = USING MODAL TRANSIENT METHOD, WITH RESIDUAL VECTORS
ECHO = UNSORTED
SPC = 200
SET 111 = 23, 33
DISPLACEMENT (SORT2) = 111
VELOCITY (SORT2) = 111
ACCELERATION (SORT2) = 111
SUBCASE 1
METHOD = 1000
DLOAD = 500
TSTEP = 100
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= BASE ACCELERATION
XYPLOT ACCELERATION RESPONSE / 23 (T3)
YTITLE= BASE DISPLACEMENT
XYPLOT DISP RESPONSE / 23 (T3)
YTITLE= TIP CENTER DISPLACEMENT RESPONSE
XYPLOT DISP RESPONSE / 33 (T3)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.0
$
$ ADD CONVERSION TO VISCOUS DAMPING
$
PARAM, W3, 1571.
$
$ APPLY EDGE CONSTRAINTS
$
SPC1, 200, 12456, 1, 12, 23, 34, 45
$
SPC1, 200, 3, 23
$
$ APPLY ACCELERATION TO THE BASE
$
TLOAD2, 500, 600, , A, 0.0, 0.004, 250., -90.
$
SPCD, 600, 23, 3, 1.0
$
$ SPECIFY INTEGRATION TIME STEPS
$
TSTEP, 100, 200, 2.0E-4, 1
$
ENDDATA
```

# Step 2. Change Solution Request

First change the file name to **soln8B.dat**. The solution request for a modal transient response is SOL 112, so change the SOL 109 to **SOL112**.

```
soln8B.dat
SOL 112
END
TITLE = TRANSIENT RESPONSE WITH BASE EXCITATION
SUBTITLE = USING MODAL TRANSIENT METHOD, WITH RESIDUAL VECTORS
ECHO = UNSORTED
SPC = 200
SET 111 = 23, 33
DISPLACEMENT (SORT2) = 111
VELOCITY (SORT2) = 111
ACCELERATION (SORT2) = 111
$
RESVEC = YES
$
SUBCASE 1
METHOD = 1000
DLOAD = 500
TSTEP = 100
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= BASE ACCELERATION
XYPLOT ACCELERATION RESPONSE / 23 (T3)
YTITLE= BASE DISPLACEMENT
XYPLOT DISP RESPONSE / 23 (T3)
YTITLE= TIP CENTER DISPLACEMENT RESPONSE
XYPLOT DISP RESPONSE / 33 (T3)
$
BEGIN BULK
*****
***** PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
*****
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
*****
ADD EIGENVALUE METHOD
*****
TIGRL,1000,,10
*****
SPECIFY STRUCTURAL DAMPING
PARAM, G, 0.06
*****
ADD CONVERSION TO VISCOUS DAMPING
PARAM, W3, 1571.
*****
APPLY EDGE CONSTRAINTS]
SPC1, 200, 12456, 1, 12, 23, 34, 45
$
SPC1, 200, 3, 23
*****
APPLY ACCELERATION TO THE BASE
TLOAD2, 500, 600, , A, 0.0, 0.004, 250, , -90.
$
SPCD, 600, 23, 3, 1.0
*****
SPECIFY INTEGRATION TIME STEPS
TSTEP, 100, 200, 2.0E-4, 1
$
ENDDATA
```

# Step 3. Add Option for Residual Vectors

Use the Case Control command **RESVEC** to specify the option for residual vectors.

```
$ soln8B.dat
$
SOL 112
CEND
TITLE = TRANSIENT RESPONSE WITH BASE EXCITATION
SUBTITLE = USING MODAL TRANSIENT METHOD, WITH RESIDUAL VECTORS
ECHO = UNSORTED
SPC = 200
SET 111 = 23, 33
DISPLACEMENT (SORT2) = 111
VELOCITY (SORT2) = 111
ACCELERATION (SORT2) = 111
$
RESVEC = YES
$
SUBCASE 1
METHOD = 1000
DLOAD = 500
TSTEP = 100
$
OUTPUT (XVPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= BASE ACCELERATION
XVPLOT ACCELERATION RESPONSE / 23 (T3)
YTITLE= BASE DISPLACEMENT
XVPLOT DISP RESPONSE / 23 (T3)
YTITLE= TIP CENTER DISPLACEMENT RESPONSE
XVPLOT DISP RESPONSE / 33 (T3)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COUPHASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$ ADD CONVERSION TO VISCOUS DAMPING
$
PARAM, W3, 1571.
$
$ APPLY EDGE CONSTRAINTS
$
SPC1, 200, 12456, 1, 12, 23, 34, 45
$
SPC1, 200, 3, 23
$
$ APPLY ACCELERATION TO THE BASE
$
TLOAD2, 500, 600, , A, 0.0, 0.004, 250., -90.
$
SPCD, 600, 23, 3, 1.0
$
$ CONCENTRATED MASS AT GRID POINT 23
$
CONM2, 700, 23, ,1000.0
$
$ DEFINE BASE AS RIGID BODY
$
RBE2, 101, 23, 3, 1, 12, 34, 45
$
$ SPECIFY INTEGRATION TIME STEPS
$
TSTEP, 100, 200, 2.0E-4, 1
$
ENDDATA
```

# Step 4. Add the Eigenvalue Method

To add the eigenvalue Method:

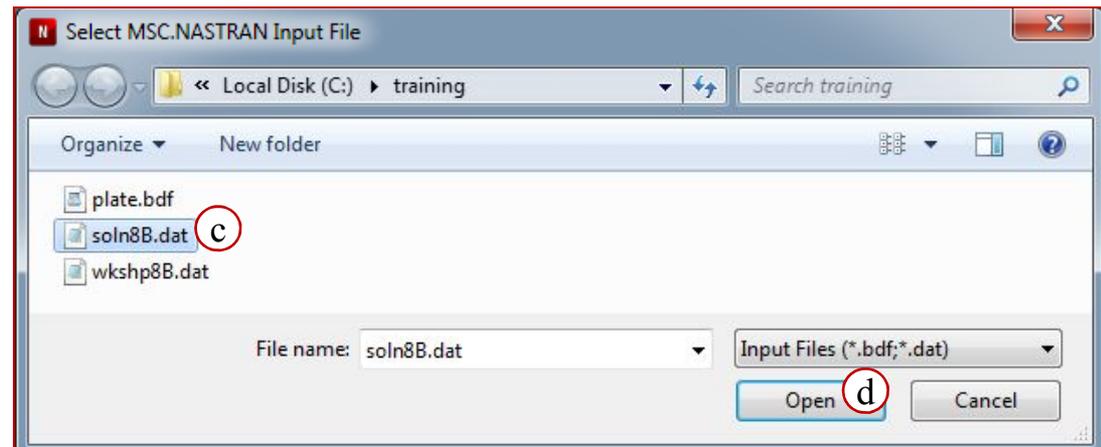
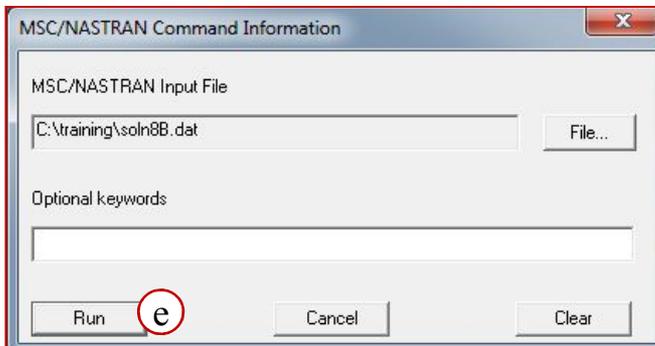
- a. Use the **EIGRL** entry specifying **10** roots.
- b. Make sure that the **METHOD** Case Control command identification number matches the **EIGRL** SID.

```
$
$   so1n8B.dat
$
SOL 112
CEND
TITLE = TRANSIENT RESPONSE WITH BASE EXCITATION
SUBTITLE = USING MODAL TRANSIENT METHOD, WITH RESIDUAL VECTORS
ECHO = UNSORTED
SPC = 200
SET 111 = 23, 33
DISPLACEMENT (SORT2) = 111
VELOCITY (SORT2) = 111
ACCELERATION (SORT2) = 111
$
RESVEC = YES
$
SUBCASE 1
METHOD = 1000
DLOAD = 500
TSTEP = 100
$
OUTPUT (XYPLOT)
XGRID=YES
YGRID=YES
XTITLE= TIME (SEC)
YTITLE= BASE ACCELERATION
XYPLOT ACCELERATION RESPONSE / 23 (T3)
YTITLE= BASE DISPLACEMENT
XYPLOT DISP RESPONSE / 23 (T3)
YTITLE= TIF CENTER DISPLACEMENT RESPONSE
XYPLOT DISP RESPONSE / 33 (T3)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COMPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
ADD EIGENVALUE METHOD
EIGRL ,1000, ,10
$
SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
ADD CONVERSION TO VISCOUS DAMPING
$
PARAM, W3, 1571.
$
APPLY EDGE CONSTRAINTS
$
SPC1, 200, 12456, 1, 12, 23, 34, 45
$
SPC1, 200, 3, 23
$
APPLY ACCELERATION TO THE BASE
TLOAD2, 500, 600, , A, 0.0, 0.004, 250, , -90.
$
SPCD, 600, 23, 3, 1.0
$
SPECIFY INTEGRATION TIME STEPS
TSTEP, 100, 200, 2.0E-4, 1
$
ENDDATA
```

# Step 5. Save and Run the New Input File

Save and run the modified file in MSC Nastran.

- a. Save the modified file as **soln8B.dat**
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln8B.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 6. Review the Results in the Solution File

REAL EIGENVALUES (BEFORE AUGMENTATION OF RESIDUAL VECTORS)						
MODE NO.	EXTRACTION ORDER	EIGENVALUE	RADIANS	CYCLES	GENERALIZED MASS	GENERALIZED STIFFNESS
1	1	7.050426E+05	8.396682E+02	1.336373E+02	1.000000E+00	7.050426E+05
2	2	1.832175E+07	4.280392E+03	6.812455E+02	1.000000E+00	1.832175E+07
3	3	2.776317E+07	5.269076E+03	8.385995E+02	1.000000E+00	2.776317E+07
4	4	1.856838E+08	1.362658E+04	2.168738E+03	1.000000E+00	1.856838E+08
5	5	2.221668E+08	1.490526E+04	2.372246E+03	1.000000E+00	2.221668E+08
6	6	2.233164E+08	1.494377E+04	2.378375E+03	1.000000E+00	2.233164E+08
7	7	6.335290E+08	2.517000E+04	4.005930E+03	1.000000E+00	6.335290E+08
8	8	8.685228E+08	2.947071E+04	4.690409E+03	1.000000E+00	8.685228E+08
9	9	1.360507E+09	3.688505E+04	5.870438E+03	1.000000E+00	1.360507E+09
10	10	1.583123E+09	3.978848E+04	6.332533E+03	1.000000E+00	1.583123E+09

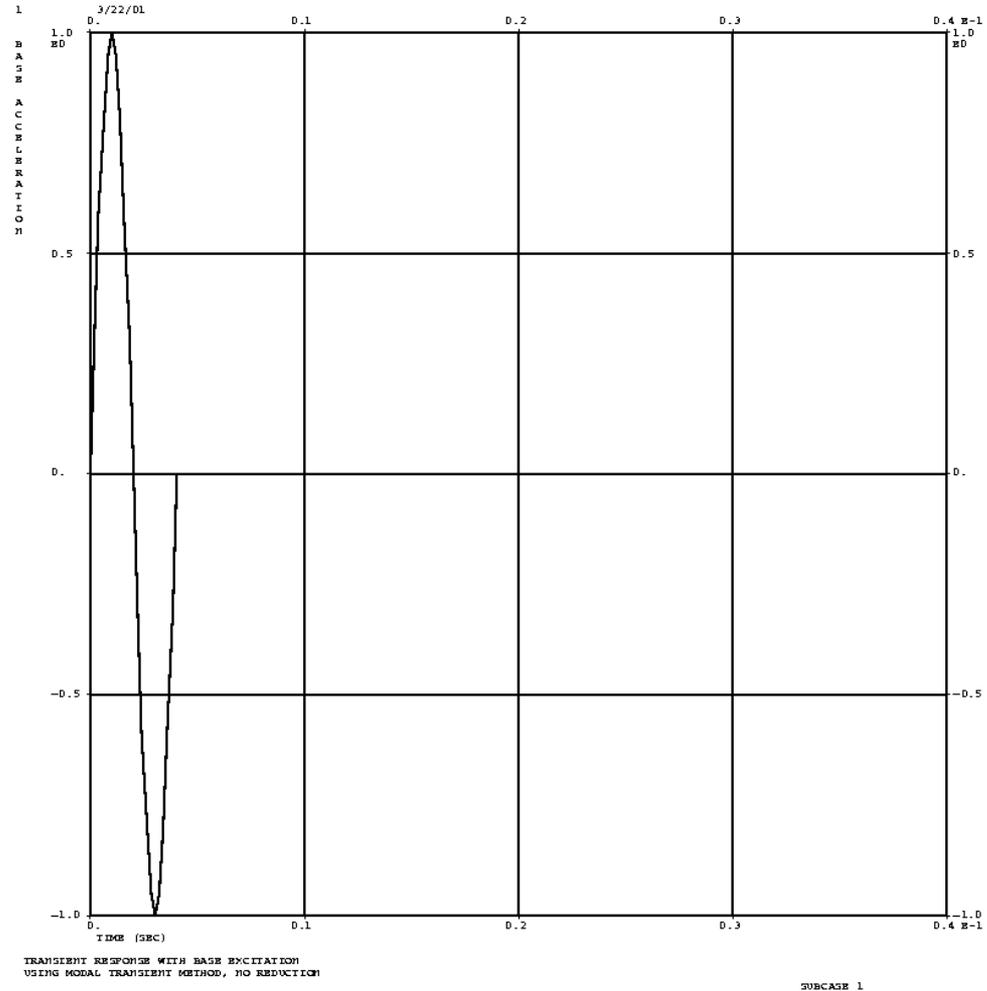
  

REAL EIGENVALUES (AFTER AUGMENTATION OF RESIDUAL VECTORS)						
MODE NO.	EXTRACTION ORDER	EIGENVALUE	RADIANS	CYCLES	GENERALIZED MASS	GENERALIZED STIFFNESS
1	1	7.050426E+05	8.396682E+02	1.336373E+02	1.000000E+00	7.050426E+05
2	2	1.832176E+07	4.280392E+03	6.812455E+02	1.000000E+00	1.832176E+07
3	3	2.776316E+07	5.269076E+03	8.385995E+02	1.000000E+00	2.776316E+07
4	4	1.856838E+08	1.362658E+04	2.168738E+03	1.000000E+00	1.856838E+08
5	5	2.221668E+08	1.490526E+04	2.372246E+03	1.000000E+00	2.221668E+08
6	6	2.233164E+08	1.494377E+04	2.378375E+03	1.000000E+00	2.233164E+08
7	7	6.335290E+08	2.517000E+04	4.005930E+03	1.000000E+00	6.335290E+08
8	8	8.685228E+08	2.947071E+04	4.690409E+03	1.000000E+00	8.685228E+08
9	9	1.360507E+09	3.688505E+04	5.870438E+03	1.000000E+00	1.360507E+09
10	10	1.583123E+09	3.978848E+04	6.332533E+03	1.000000E+00	1.583123E+09
11	11	2.517908E+09	5.017876E+04	7.986197E+03	1.000000E+00	2.517908E+09
12	12	3.681851E+09	6.067826E+04	9.657244E+03	1.000000E+00	3.681851E+09
13	13	4.154735E+09	6.445723E+04	1.025869E+04	1.000000E+00	4.154735E+09
14	14	4.205938E+09	6.485321E+04	1.032171E+04	1.000000E+00	4.205938E+09
15	15	6.573208E+09	8.107532E+04	1.290354E+04	1.000000E+00	6.573208E+09
16	16	3.216851E+10	1.793558E+05	2.854536E+04	1.000000E+00	3.216851E+10

# Step 7. Review the Graph Results

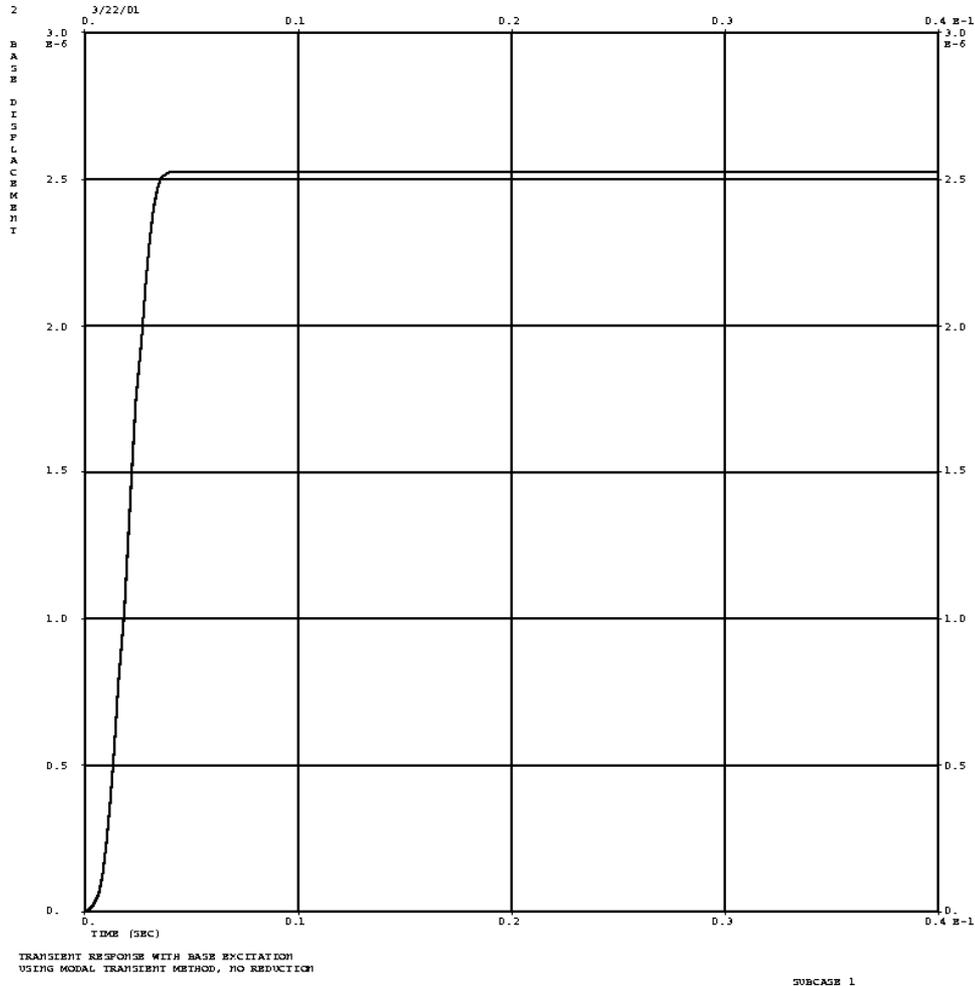
Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions given in workshop 4, step 9.

Base acceleration at Grid Point 23



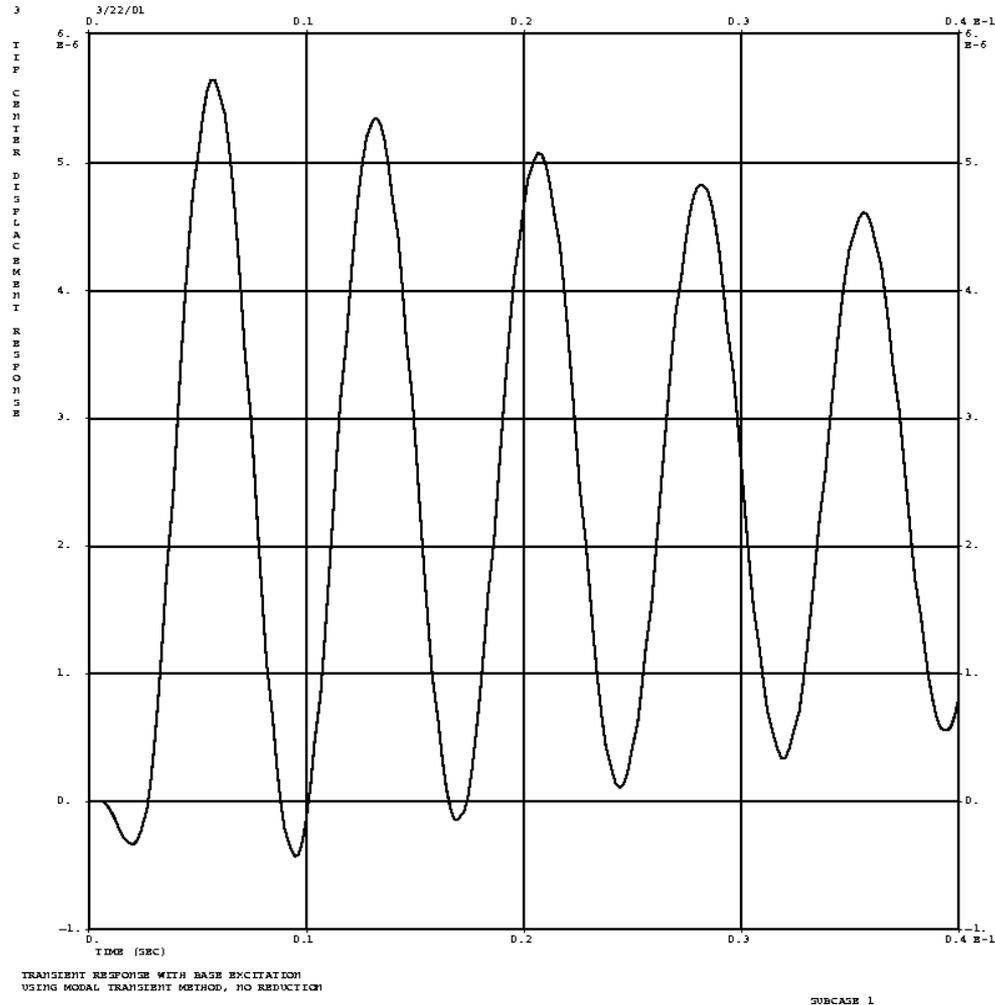
# Step 7. Review the Graph Results (Cont.)

Base displacement at Grid Point 23



# Step 7. Review the Graph Results (Cont.)

Tip displacement at Grid Point 33



# **WORKSHOP 9A**

## **DIRECT FREQUENCY RESPONSE WITH ENFORCED DISPLACEMENT**



- **Workshop Objective**

- Using the direct method, determine the frequency response of the flat rectangular plate (from workshop1) subject to an enforced displacement as described below.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

- plate.bdf
- wkshp9A.dat

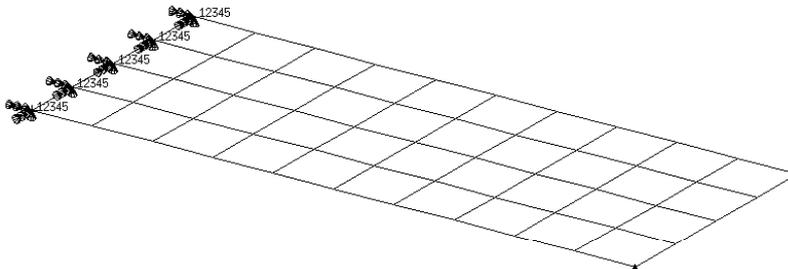
- **Problem Description**

- The structure is subject to a 0.1 inch enforced displacement at the corner of the tip. Use a frequency step of 20 Hz in the range of 20 to 1000 Hz. Use a structural damping of  $g = 0.06$ .

- **Problem Description Continued:**

- The figures below show the finite element representation of the flat plate and the loads and boundary condition.

### Load and Boundary Condition



Displacement applied in Z direction at grid point 11



### Elements and Grid Coordinates

45	46	47	48	49	50	51	52	53	54	55
31	32	33	34	35	36	37	38	39	40	
34	35	36	37	38	39	40	41	42	43	44
21	22	23	24	25	26	27	28	29	30	33
23	24	25	26	27	28	29	30	31	32	
11	12	13	14	15	16	17	18	19	20	
12	13	14	15	16	17	18	19	20	21	22
1	2	3	4	5	6	7	8	9	10	
1	2	3	4	5	6	7	8	9	10	11

TIP  
↓

- **Suggested Step**

1. Open and review the input file wkshp9A.dat.
2. Add structural damping.
3. Add enforced motion input.
4. Add frequency steps.
5. Save and run the new input file in MSC Nastran
6. Review the MSC Nastran results using the soln9A.f06 file.
7. Review the graph results

# Step 1. Open and Review Input File wkshp9A.dat

The file wkshp9A is the starting input file to be modified.

```
$
$ wkshp9A.dat
$
$   add      :   enforced motion input
$             frequencies of loading
$
SOL 108
CEND
TITLE= FREQUENCY RESPONSE DUE TO .1 DISPLACEMENT AT TIP
SUBTITLE= DIRECT METHOD
ECHO= UNSORTED
SPC= 1
SET 111= 11, 33, 55
DISPLACEMENT(PHASE, SORT2)= 111
SET 222 = 11
OLOAD= 222
SUBCASE 1
DLOAD= 500
FREQUENCY= 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
ENDDATA
```

# Step 2. Add structural Damping

Add the appropriate parameters in the Bulk Data section for damping.

- a. First rename the input file as **soln9A.dat**.
- b. Use **PARAM G** with a value of **.06**.

```
soln9A.dat
*
SOL 108
CEND
TITLE= FREQUENCY RESPONSE DUE TO .1 DISPLACEMENT AT TIP
SUBTITLE= DIRECT METHOD
ECHO= UNSORTED
SPC= 1
SET 111= 11, 33, 55
DISPLACEMENT(PHASE, SORT2)= 111
$SDISP(PHASE, SORT2)= ALL
SET 222 = 11
OLOAD= 222
SUBCASE 1
DLOAD= 500
FREQUENCY= 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
ENDDATA
```

# Step 3. Add Enforced Motion Input

Add 0.1 displacement at the corner of the tip (grid point 11) of the plate, with a frequency step of 20 Hz in the range of 20 to 1000 Hz. Use the following entries:

- a. **SPC1** – grid point **11**, Z (**3**) direction
- b. **SPCD** - apply the **.1** displacement in the Z (**3**) direction at grid point **11**.
- c. **RLOAD2** - define the excitation as displacement and point to the **SPCD** and **TABLED1**. Make sure the SID for the **RLOAD2** entry matches the identification number for the **DLOAD** in the Case Control section.
- d. **TABLED1** – add frequencies for loading.

```
$
$   soln9A.dat
$
SOL 108
CEND
TITLE= FREQUENCY RESPONSE DUE TO .1 DISPLACEMENT AT TIP
SUBTITLE= DIRECT METHOD
ECHO= UNSORTED
SPC= 1
SET 111= 11, 33, 55
DISPLACEMENT(PHASE, SORT2)= 111
SET 222 = 11
OLOAD= 222
SUBCASE 1
DLOAD= 500
FREQUENCY= 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTITITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTITITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTITITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENEMETH, REL
PARAM, ENEMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$ APPLY DISPLACEMENT AT FREE EDGE
$
a SPC1, 11, 3, 11
b SPCD, 600, 11, 3, 0.1
c RLOAD2, 500, 600, ., .310, ., DISP
d TABLED1, 310,
, 0., 1., 10000., 1., ENDT
$
ENDDATA
```

# Step 4. Add the frequency steps

To add the frequency steps use of the **FREQ1** entry.

- a. For **FREQ1** entry, from the given information you can obtain:
  - First freq. = **20**
  - Frequency incr = **20**
  - Number of freq. increments = **49**
- b. Make sure that the **SID** for the **FREQ1** entry matches the identification number for the **FREQUENCY** in the Case Control section.

```

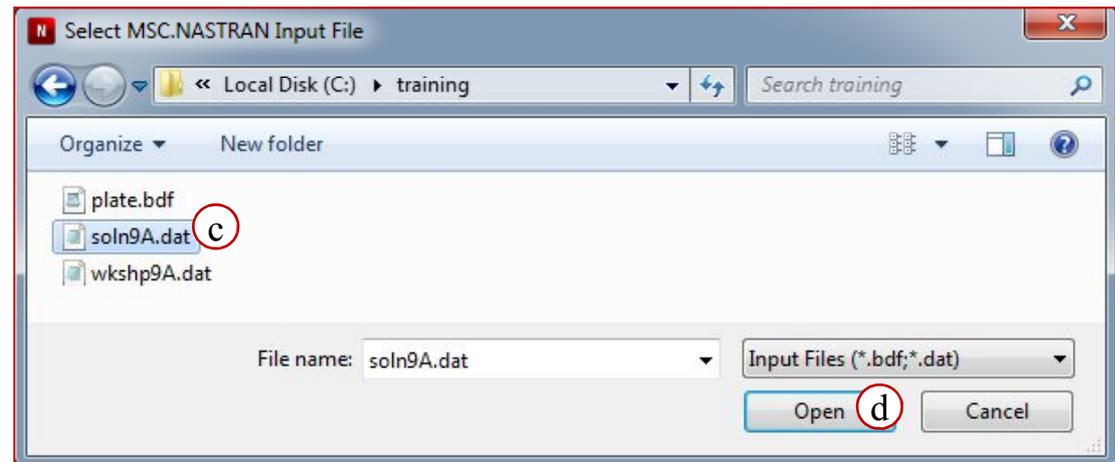
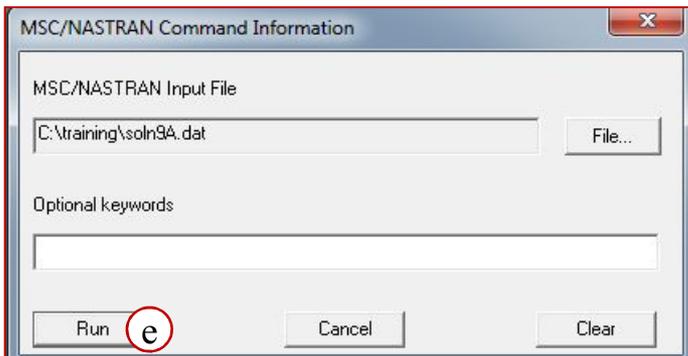
$
$   soln9A.dat
$
SOL 108
CEND
TITLE= FREQUENCY RESPONSE DUE TO .1 DISPLACEMENT AT TIP
SUBTITLE= DIRECT METHOD
ECHO= UNSORTED
SPC= 1
SET 111= 11, 33, 55
DISPLACEMENT(PHASE, SORT2)= 111
SET 222 = 11
OLOAD= 222
SUBCASE 1
DLOAD= 500
FREQUENCY= 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
VTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YHLOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
$
$   PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
$   SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$   APPLY DISPLACEMENT AT TIP
$
SPC1, 1, 3, 11
$
SPCD, 600, 11, 3, 0.1
$
RLOAD2, 500, 600, ., .310, ., DISP
$
TABLED1, 310,
, 0., 1., 10000., 1., ENDT
$
$   SPECIFY FREQUENCY STEPS
$
FREQ1, 100, 20., 20., 49
$
ENDDATA

```

# Step 5. Save and Run the New Input File

Save and run the modified file in MSC Nastran.

- a. Save the modified file as **soln9A.dat**
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln9A.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 6. Review the Results in the Solution File

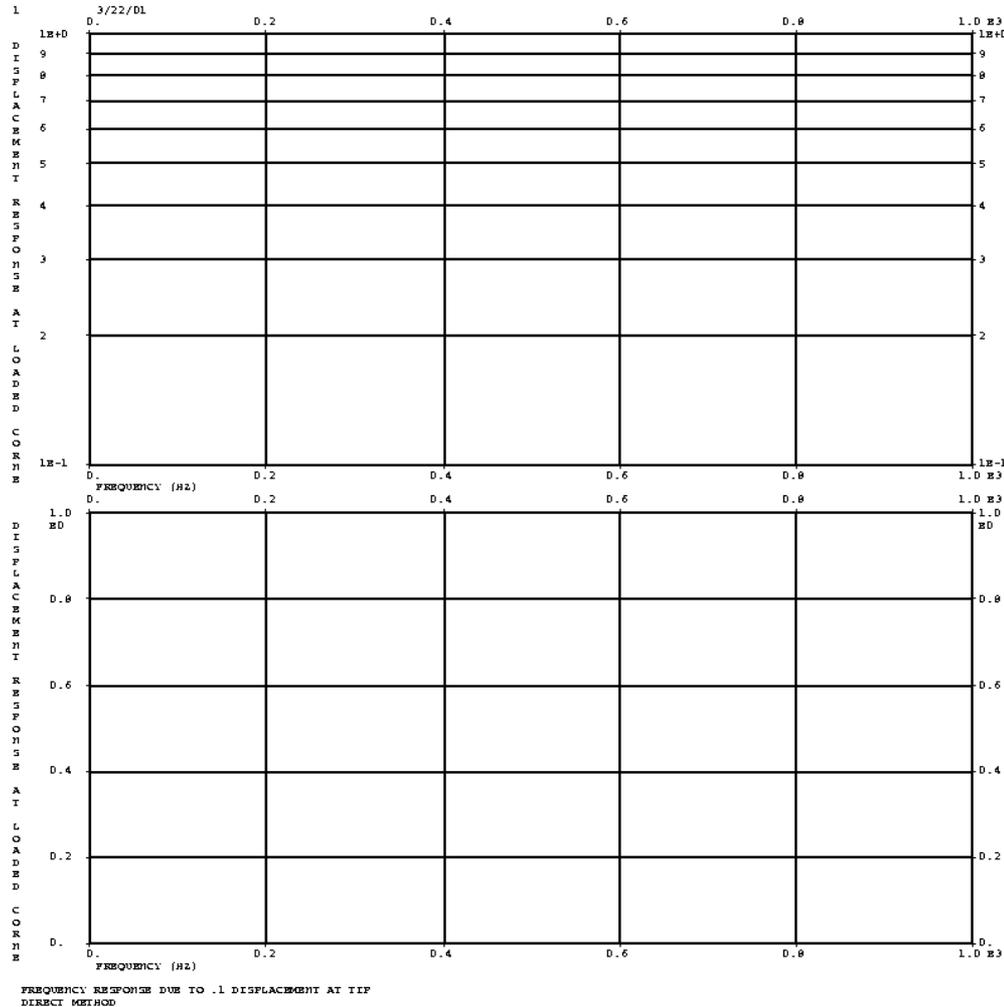
To view the results open the soln9a.f06 file.

SUBCASE 1										
X Y - O U T P U T S U M M A R Y ( R E S P O N S E )										
SUBCASE	CURVE	FRAME	CURVE ID. /	XMIN-FRAME/	XMAX-FRAME/	YMIN-FRAME/	X FOR	YMAX-FRAME/	X FOR	
ID	TYPE	NO.	PANEL : GRID ID	ALL DATA	ALL DATA	ALL DATA	YMIN	ALL DATA	YMAX	
1	DISP	1	11( 5,--)	2.000000E+01	1.000000E+03	1.000000E-01	2.000000E+01	1.000000E-01	2.000000E+01	2.000000E+01
1	DISP	1	11(--, 11)	2.000000E+01	1.000000E+03	0.000000E+00	2.000000E+01	0.000000E+00	2.000000E+01	2.000000E+01
1	DISP	2	33( 5,--)	2.000000E+01	1.000000E+03	0.000000E+00	2.000000E+01	0.000000E+00	2.000000E+01	2.000000E+01
1	DISP	2	33(--, 11)	2.000000E+01	1.000000E+03	2.310269E-03	6.000000E+02	8.439929E-01	3.800000E+02	3.800000E+02
1	DISP	3	55( 5,--)	2.000000E+01	1.000000E+03	2.443192E-02	1.000000E+03	1.623458E+00	3.800000E+02	3.800000E+02
1	DISP	3	55(--, 11)	2.000000E+01	1.000000E+03	2.443192E-02	1.000000E+03	1.623458E+00	3.800000E+02	3.800000E+02
				2.000000E+01	1.000000E+03	3.672138E+00	1.000000E+03	3.599891E+02	2.000000E+01	2.000000E+01
				2.000000E+01	1.000000E+03	3.672138E+00	1.000000E+03	3.599891E+02	2.000000E+01	2.000000E+01

# Step 7. Review the Graph Results

Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions given in workshop 4, step 9.

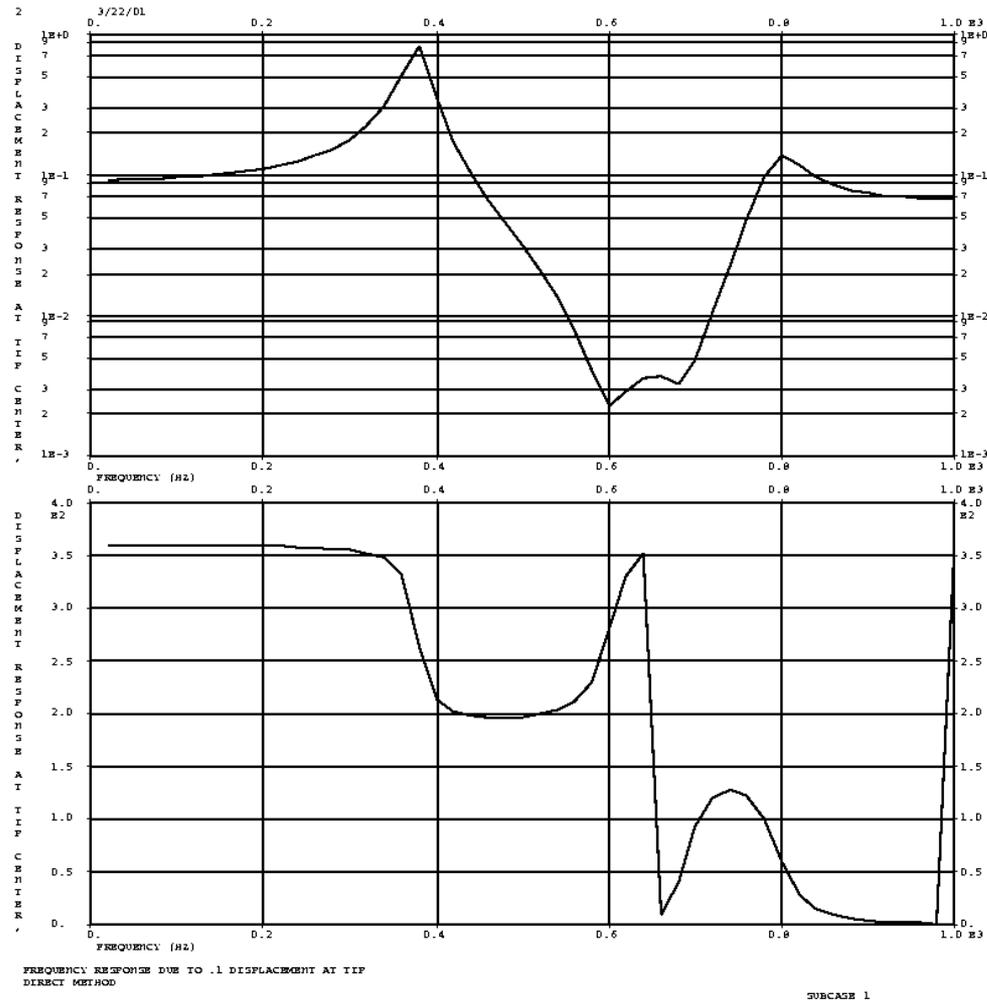
Displacement at loaded corner at Grid Point 11



SUBCASE 1

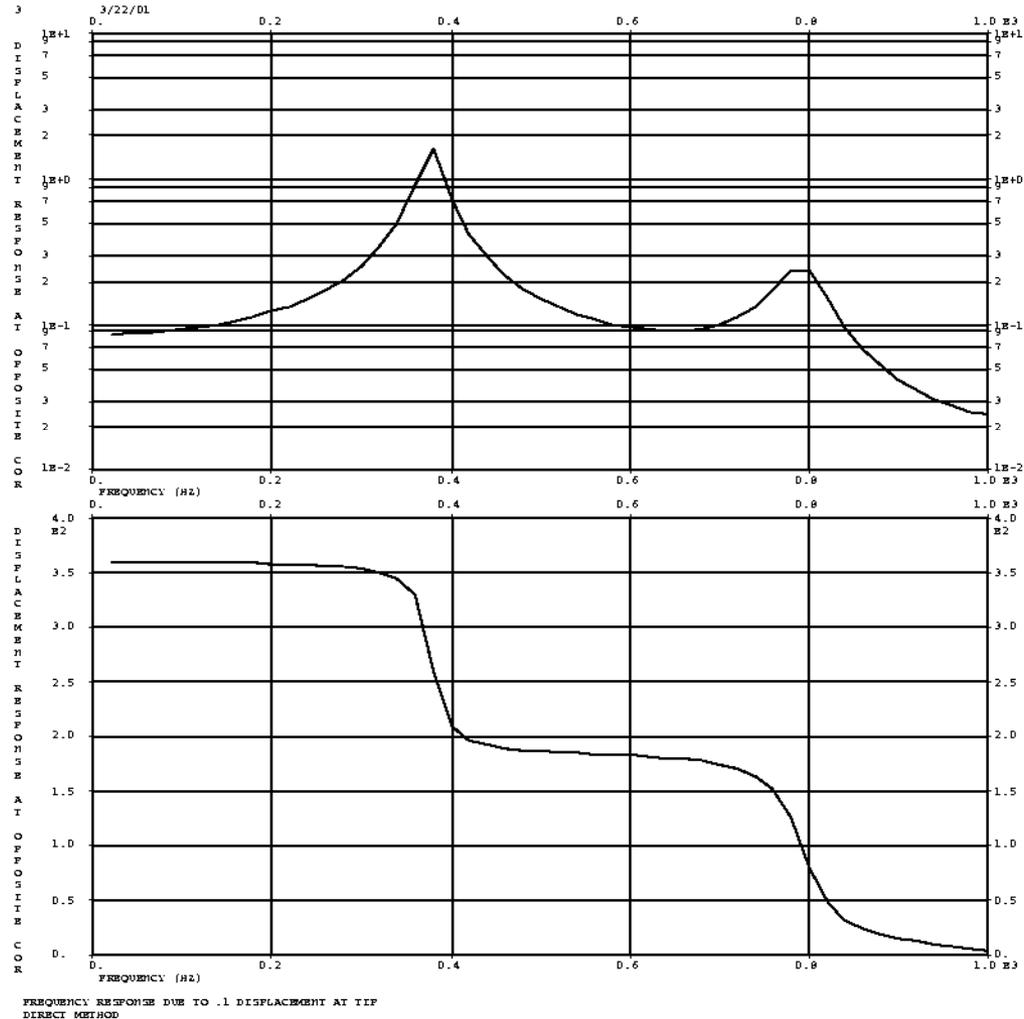
# Step 7. Review the Graph Results (Cont.)

Displacement at center of the tip at Grid Point 33



# Step 7. Review the Graph Results (Cont.)

Displacement at opposite corner from the load at Grid Point 55



SUBCASE 1

# **WORKSHOP 9B**

## **MODAL FREQUENCY RESPONSE WITH ENFORCED DISPLACEMENT**



- **Workshop Objective**

- Using the modal method, determine the frequency response of the flat rectangular plate, (from Workshop 1) subject to an enforced displacement described below.

- **Software Version**

- MSC Nastran

- **Files Required**

- plate.bdf
- wkshp9B.dat

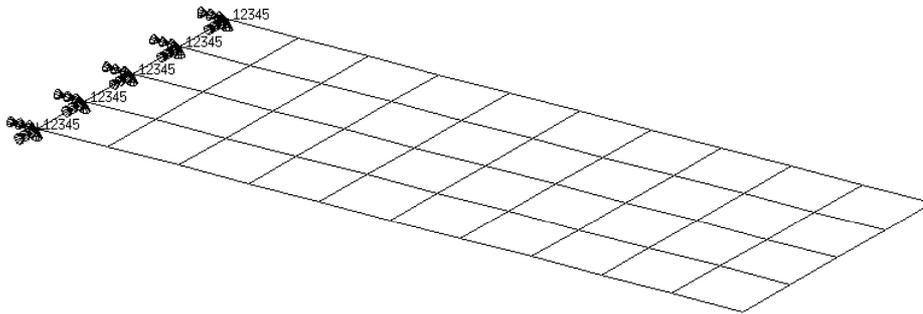
- **Problem Description**

- The structure is subject to an 0.1 enforced displacement at the corner of the tip. Use a frequency step of 20 Hz in the range of 20 to 1000 Hz. Use a structural damping of  $g = 0.06$ . Be sure to include residual vectors.

- **Problem Description Continued:**

- The figures below show the finite element representation of the flat plate and the loads and boundary condition.

### Load and Boundary Condition



Displacement applied in Z direction at grid point 11



### Elements and Grid Coordinates

45	46	47	48	49	50	51	52	53	54	55
31	32	33	34	35	36	37	38	39	40	44
34	35	36	37	38	39	40	41	42	43	44
21	22	23	24	25	26	27	28	29	30	33
23	24	25	26	27	28	29	30	31	32	33
11	12	13	14	15	16	17	18	19	20	22
12	13	14	15	16	17	18	19	20	21	22
1	2	3	4	5	6	7	8	9	10	11
1	2	3	4	5	6	7	8	9	10	11

TIP



- **Suggested Steps**

1. Open and review the input file wkshp9B.dat.
2. Change the solution request to SOL111.
3. Add option to include residual vectors.
4. Add eigenvalue method.
5. Save and run the new input file in MSC Nastran.
6. Review the MSC Nastran result using the soln9b.f06 file.
7. Review the graph results.

# Step 1. Open and Review Input File wkshp9B.dat

The file wkshp9B.dat is the starting input file. This is the final input file from workshop9A. All that is necessary is to change from a direct method to a modal one and to add a case control command for the residual vector option.

```
$
$ wkshp9B.dat
$
$ add: change solution request SOL111
$ add residual vectors
$ add engenvalue method
$
SOL 108
CEND
TITLE= FREQUENCY RESPONSE DUE TO .1 DISPLACEMENT AT TIP
SUBTITLE= MODAL METHOD WITH RESIDUAL VECTORS
ECHO= UNSORTED
SPC= 1
SET 111= 11, 33, 55
DISPLACEMENT(PHASE, SORT2)= 111
SET 222 = 11
OLOAD = 222
SUBCASE 1
METHOD = 1000
DLOAD = 500
FREQUENCY = 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
YTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T31F)
YTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T31F)
YTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T31F)
$
BEGIN BULK
$
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$ APPLY DISPLACEMENT AT TIP POINT
$
SPC1, 1, 3, 11
$
SPCD, 600, 11, 3, 0.1
$
RLOAD2, 500, 600, ., ., 310, ., D
$
TABLED1, 310,
.0, ., 1, ., 10000.0, 1.0, ENDT
$
$ SPECIFY FREQUENCY STEPS
$
FREQ1, 100, 20, ., 20, ., 49
$
ENDDATA
```



# Step 3. Add Option for Residual Vectors

Use the Case Control command **RESVEC** to specify the option for residual vectors.

```

$
$   soln9B.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE DUE TO .1 DISPLACEMENT AT TIP
SUBTITLE = MODAL METHOD WITH RESIDUAL VECTORS
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE, SORT2)= 111
SET 222 = 11
OLOAD = 222
$
RESVEC = YES
$
SUBCASE 1
METHOD = 1000
DLOAD = 500
FREQUENCY= 100
$
OUTPUT (XYPLOT)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
YBLOG= NO
XTITLE= FREQUENCY (HZ)
VTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
VBITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IF)
VTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
VBITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IF)
VTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
VBITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IF)
$
BEGIN BULK
$
PARAM, POST, 0
PARAM, ENFMETH, REL
PARAM, ENFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$ APPLY DISPLACEMENT AT TIP POINT
$
SPC1, 1, 3, 11
$
SPCD, 600, 11, 3, 0.1
$
RLOAD2, 500, 600, , , 310, , D
$
TABLED1, 310,
, 0, , 1, , 10000.0, 1.0, ENDT
$
$ SPECIFY FREQUENCY STEPS
$
FREQ1, 100, 20, , 20, , 49
$
ENDDATA
```

# Step 4. Add the Eigenvalue Method

Add the eigenvalue Method:

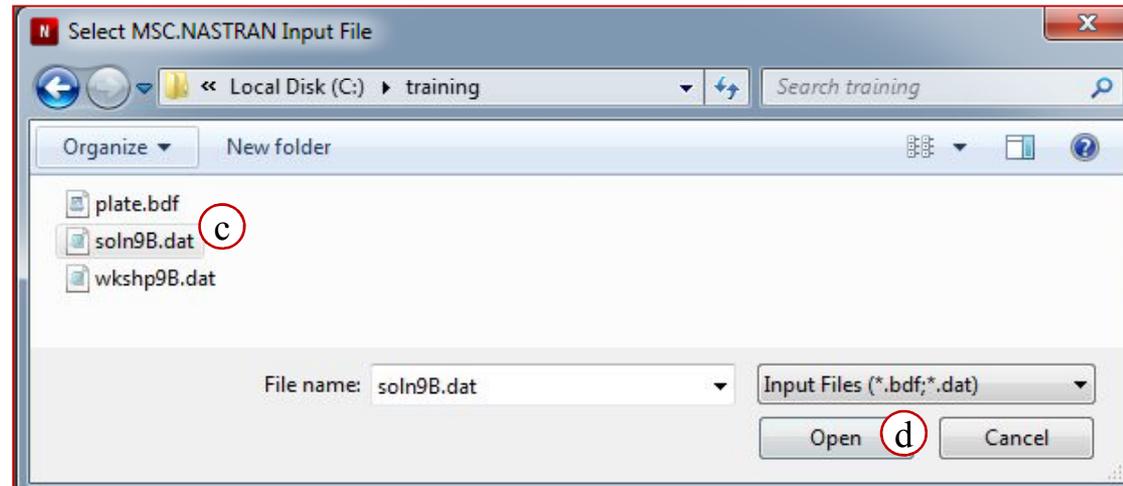
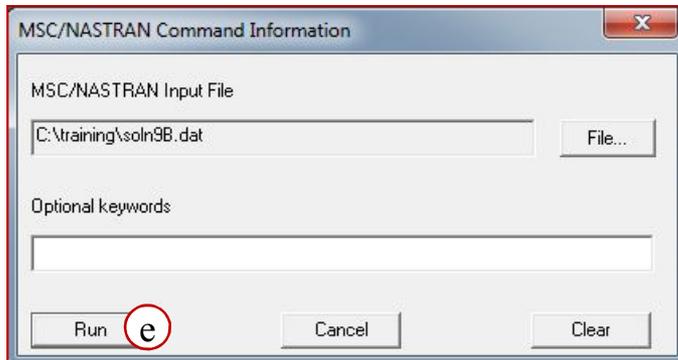
- a. Use the **EIGRL** entry specifying **10** roots.
- b. Make sure that the **METHOD** Case Control command identification number matches the **EIGRL** SID.

```
$
$   soln9B.dat
$
SOL 111
CEND
TITLE = FREQUENCY RESPONSE DUE TO .1 DISPLACEMENT AT TIP
SUBTITLE = MODAL METHOD WITH RESIDUAL VECTORS
ECHO = UNSORTED
SPC = 1
SET 111 = 11, 33, 55
DISPLACEMENT(PHASE, SORT2)= 111
SET 222 = 11
OLOAD = 222
$
RESVEC = YES
$
SUBCASE 1
METHOD = 1000
DLOAD = 50
FREQUENCY = 10
$
OUTPUT (XYPL01)
$
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTILOG= YES
YELOG= NO
XTITLE= FREQUENCY (HZ)
YTTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT LOADED CORNER, PHASE
XYPLOT DISP RESPONSE / 11 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT TIP CENTER, PHASE
XYPLOT DISP RESPONSE / 33 (T3RM, T3IP)
YTTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= DISPLACEMENT RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT DISP RESPONSE / 55 (T3RM, T3IP)
$
BEGIN BULK
$
PARAM, POST, 0
PARAM, ERFMETH, REL
PARAM, ERFMOTN, ABS
PARAM, COUPMASS, 1
PARAM, WMASS, 0.00259
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
INCLUDE 'plate.bdf'
$
$ ADD EIGENVALUE METHOD
$ EIGRL, 1000, ., 10
$
$ SPECIFY STRUCTURAL DAMPING
$
PARAM, G, 0.06
$
$ APPLY DISPLACEMENT AT TIP POINT
$
SPC1, 1, 3, 11
$
$
SPCD, 600, 11, 3, 0.1
$
RLOAD2, 500, 600, ., .310, .D
$
TABLED1, 310,
.0, .1, 10000.0, 1.0, ENDT
$
$ SPECIFY FREQUENCY STEPS
$
FREQ1, 100, 20, ., 20, ., 49
$
ENDDATA
```

# Step 5. Save and Run the New Input File

Save and run the modified file in MSC Nastran.

- a. Save the modified file as **soln9B.dat**
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln9B.dat**.
- d. Click **Open**.
- e. Click **Run**.



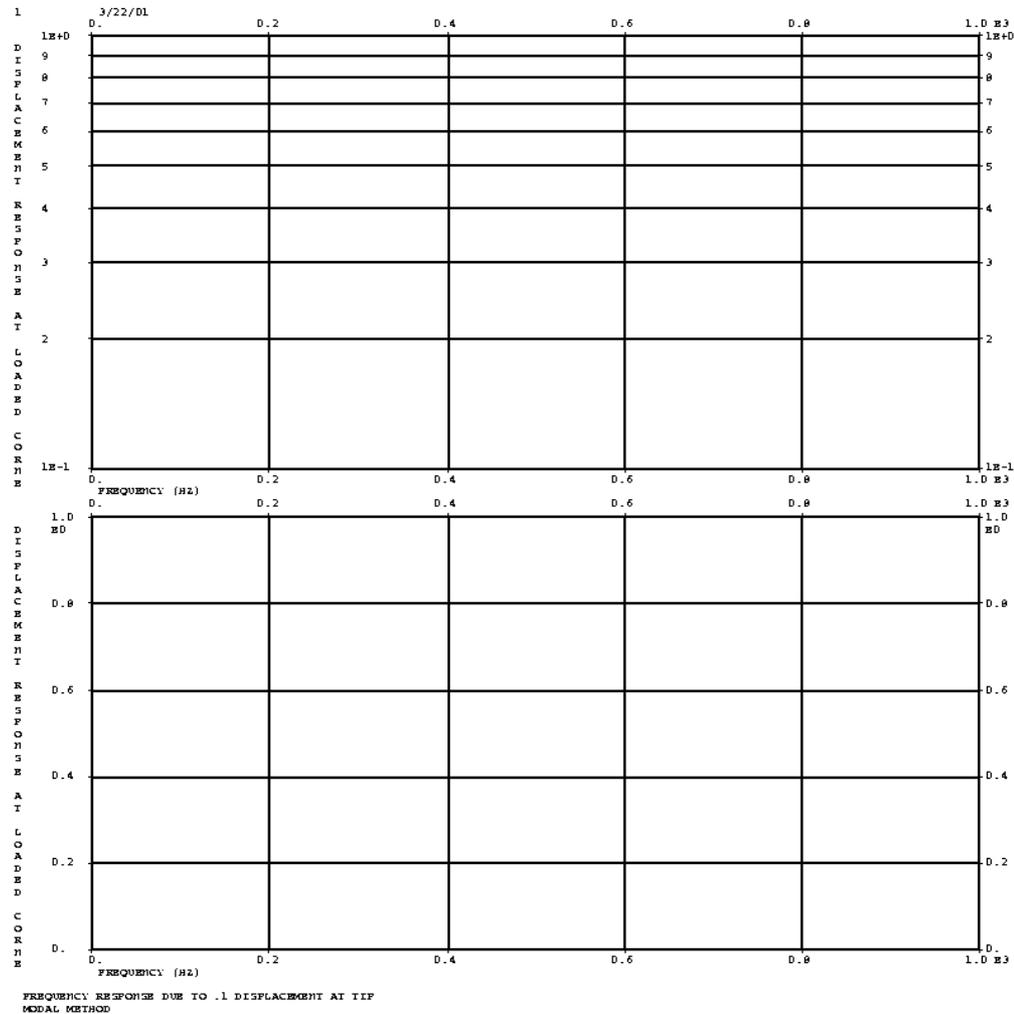
# Step 6. Review the Results in the Solution File

SUBCASE 1									
X Y - O U T P U T S U M M A R Y ( R E S P O N S E )									
SUBCASE	CURVE	FRAME	CURVE ID./	XMIN-FRAME/	XMAX-FRAME/	YMIN-FRAME/	X FOR	YMAX-FRAME/	X FOR
ID	TYPE	NO.	PANEL : GRID ID	ALL DATA	ALL DATA	ALL DATA	YMIN	ALL DATA	YMAX
1	DISP	1	11( 5,--)	2.000000E+01	1.000000E+03	1.000000E-01	2.000000E+01	1.000000E-01	2.000000E+01
				2.000000E+01	1.000000E+03	1.000000E-01	2.000000E+01	1.000000E-01	2.000000E+01
1	DISP	1	11(--, 11)	2.000000E+01	1.000000E+03	0.000000E+00	2.000000E+01	0.000000E+00	2.000000E+01
				2.000000E+01	1.000000E+03	0.000000E+00	2.000000E+01	0.000000E+00	2.000000E+01
1	DISP	2	33( 5,--)	2.000000E+01	1.000000E+03	2.310252E-03	6.000000E+02	8.439928E-01	3.800000E+02
				2.000000E+01	1.000000E+03	2.310252E-03	6.000000E+02	8.439928E-01	3.800000E+02
1	DISP	2	33(--, 11)	2.000000E+01	1.000000E+03	3.307163E-01	9.799999E+02	3.599946E+02	2.000000E+01
				2.000000E+01	1.000000E+03	3.307163E-01	9.799999E+02	3.599946E+02	2.000000E+01
1	DISP	3	55( 5,--)	2.000000E+01	1.000000E+03	2.443258E-02	1.000000E+03	1.623458E+00	3.800000E+02
				2.000000E+01	1.000000E+03	2.443258E-02	1.000000E+03	1.623458E+00	3.800000E+02
1	DISP	3	55(--, 11)	2.000000E+01	1.000000E+03	3.671850E+00	1.000000E+03	3.599891E+02	2.000000E+01
				2.000000E+01	1.000000E+03	3.671850E+00	1.000000E+03	3.599891E+02	2.000000E+01

# Step 7. Review the Graph Results

Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions given in workshop 4, step 9.

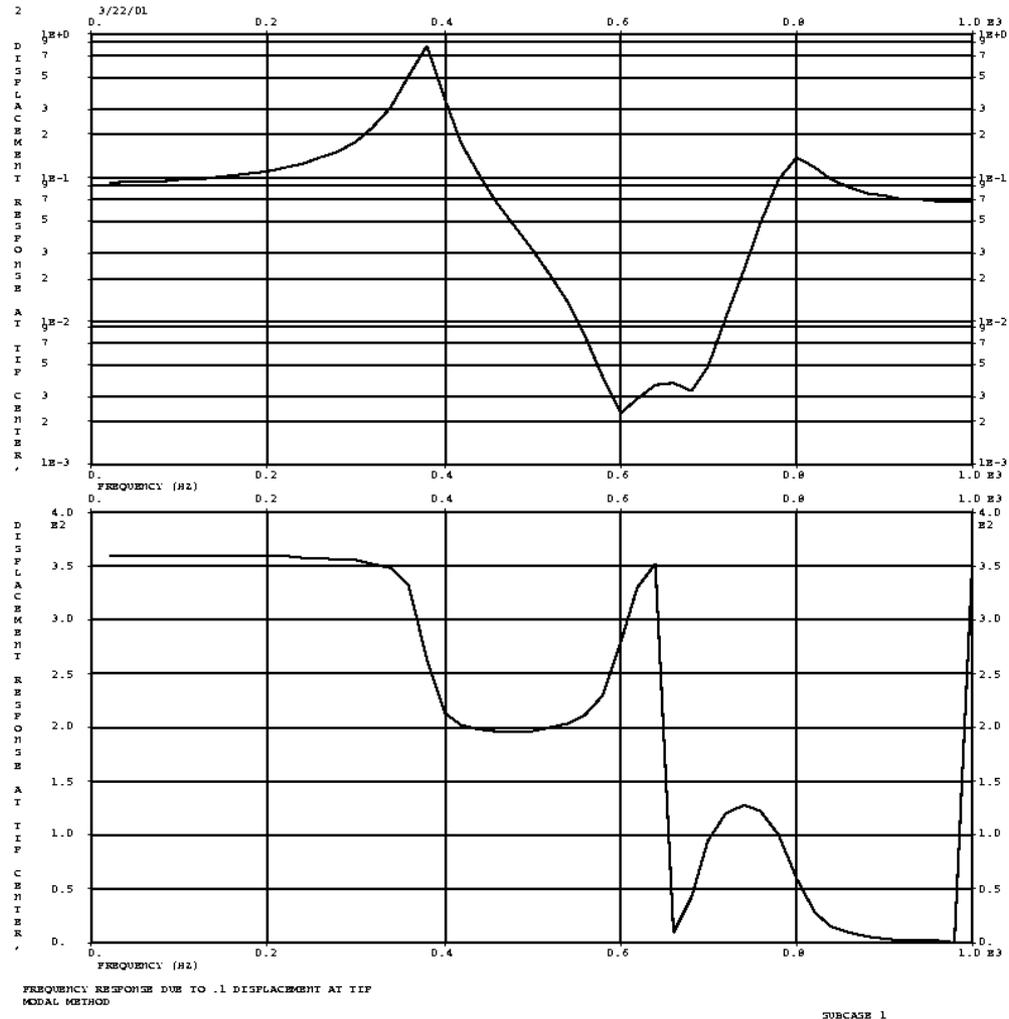
Displacement at loaded corner at Grid Point 11



SUBCASE 1

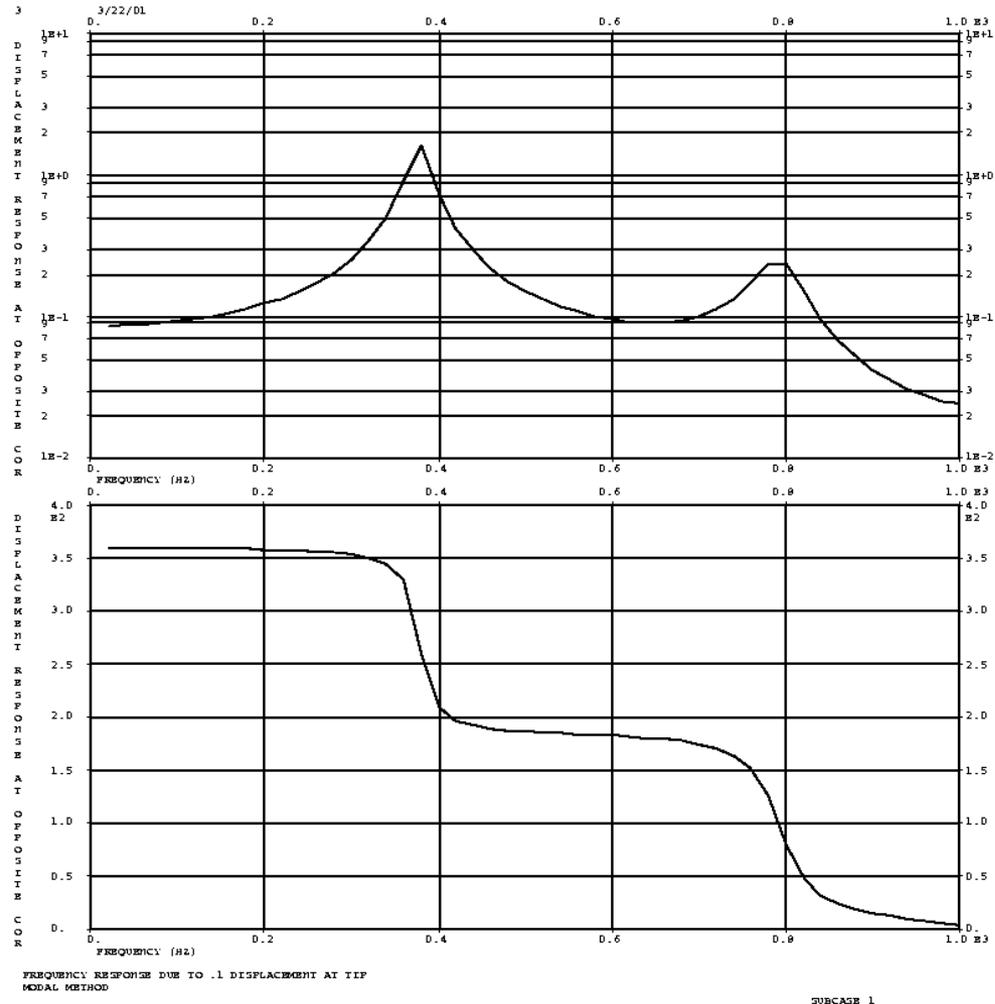
# Step 7. Review the Graph Results (Cont.)

Displacement at center of the tip at Grid Point 33



# Step 6. Review the Graph Results (Cont.)

Displacement at opposite corner from the load at Grid Point 55



# **WORKSHOP 10A**

## **GENERATE A SHOCK SPECTRUM INPUT**



- **Workshop Objectives:**

- Generate a shock spectrum for the plate (from workshop 1) due to a 2.0 in/sec<sup>2</sup> sine pulse applied at the fixed edge. Compute spectra for 0, 2, and 4 percent damping.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

- wkshp10A.dat

- **Problem Description**

- This is the first part of a two part problem. This workshop is to generate the shock spectrum. In the next workshop, 10b we need to apply generated shock input.

- **Suggested Steps**

1. Open and review the input file wkshp10A.dat
2. Add the XYplot/XYpunch commands to generate a response spectrum at grid point 3000.
3. Add the time dependent load.
4. Add the request for calculation of spectra.
5. Add entries to specify damping and natural frequencies for oscillator
6. Add entry to correlate frequency and damping requests.
7. Save and run the new input file in MSC Nastran.
8. Review the tabular results of the acceleration spectra data using the file soln10a.pch.
9. Review the graphical results.

# Step 1. Open and Review Input File wkshp10A.dat

This is the starting input file, to be modified to add the shock spectrum.

```

$
$ wkshp10A.dat
$
$ case control, add : generate response spectrum curve at grid point 3000
$ using xyplot/ypunch commands
$ bulk data, add : Add the loading
$ Add appropriate parameters to create response spectrum
$ curves for appropriate damping and frequencies at grid
$ point 3000
$
$
ID SEMINAR, PROB10A
SOL 109
TIME 30
CEND
TITLE= TRANSIENT RESPONSE
SUBTITLE= USING DIRECT TRANSIENT METHOD
LABEL= SHOCK SPECTRUM CALCULATION
ECHO= UNSORTED
SFC= 100
SET 111= 3000
DISPLACEMENT (SORT2)= 111 $ AT LEAST DISP AND VEL MUST APPEAR
VELOCITY (SORT2)= 111
ACCELERATION ()= 111
DLOAD= 500
TSTEP= 100
$
OUTPUT (XYPLOT)
$
$ SHOCK RESPONSE IS ONLY AVAILABLE IN PLOT OR PUNCH OUTPUT. THEREFORE,
$ THE 'OUTPUT(XYPLOT)' SECTION OF THE CASE CONTROL MUST BE USED.
$
XGRID=YES
YGRID=YES
XYPLOT ACCE / 3000(T1)
XLOG= YES
YLOG= YES
$
$ RELATIVE SHOCK RESPONSES ARE CONTAINED IN THE IMAGINARY/PHASE
$ COMPONENTS OF THE OUTPUT
$ ABSOLUTE SHOCK RESPONSES ARE CONTAINED IN THE REAL/MAGNITUDE
$ COMPONENTS OF THE OUTPUT
$
$
BEGIN BULK
$ DEFINE GRID POINT
$ GRID, 3000, .0..0..0., .23456
$
$ DEFINE MASS
$ CMASS2, 100, 1.0, 3000, 1
$
$ SPECIFY INTEGRATION TIME STEPS
$ TSTEP, 100, 100, 4.0E-4, 1
$ ENDDATA

```

The following information is already included in the input file.

- Grid point 3000 at location (0,0,0) and fixed in every direction and rotation except the X direction.
- Mass as a unit mass at grid point 3000
- Integration time step

# Step 2. Add the XYplot/XYpunch Commands

Change file name to **soln10A.dat** and add the **XYPLOT/XPUNCH** commands to graph and save in tabular form the response spectrum (in a pch file) at grid point **3000**, as shown to the right.

```
$
$ soln10A.dat
$
SOL 109
TIME 30
CEND
TITLE= TRANSIENT RESPONSE
SUBTITLE= USING DIRECT TRANSIENT METHOD
LABEL= SHOCK SPECTRUM CALCULATION
ECHO= UNSORTED
SPC= 100
SET 111= 3000
DISPLACEMENT (SORT2)= 111 $ AT LEAST DISP AND VEL MUST APPEAR
VELOCITY (SORT2)= 111
ACCELERATION (sort2)= 111
DLOAD= 500
TSTEP= 100
$
OUTPUT (XYPLOT)
$
$ SHOCK RESPONSE IS ONLY AVAILABLE IN PLOT OR PUNCH OUTPUT. THEREFORE,
$ THE 'OUTPUT(XYPLOT)' SECTION OF THE CASE CONTROL MUST BE USED.
$
XGRID=YES
YGRID=YES
XYPLOT ACCE / 3000(T1)
XLOG= YES
YLOG= YES
$
$ RELATIVE SHOCK RESPONSES ARE CONTAINED IN THE IMAGINARY/PHASE
$ COMPONENTS OF THE OUTPUT
$ ABSOLUTE SHOCK RESPONSES ARE CONTAINED IN THE REAL/MAGNITUDE
$ COMPONENTS OF THE OUTPUT
$
XTITLE= FREQUENCY (CYCLES/SEC)
YTITLE= RELATIVE DISPLACEMENT
XYPLOT DISP SPECTRAL 1 / 3000 (T1IP)
YTITLE= RELATIVE VELOCITY
XYPLOT VELOCITY SPECTRAL 1 / 3000 (T1IP)
YTITLE= ABSOLUTE ACCELERATION
XYPLOT ACCELERATION SPECTRAL 1 / 3000 (T1RM)
$
$ PUNCH SHOCK SPECTRUM FOR LATER USE
$
XPUNCH ACCELERATION SPECTRAL 1 / 3000(T1RM)
$
BEGIN BULK
$
$ DEFINE GRID POINT
$
GRID, 3000, .0.,.0.,.0., .23456
$
$ DEFINE MASS
$
CMASS2, 100, 1.0, 3000, 1
$
$ SPECIFY INTEGRATION TIME STEPS
$
TSTEP, 100, 100, 4.0E-4, 1
$
ENDDATA
```

# Step 3. Add the Time Dependent Load

Add the 2 in/sec<sup>2</sup> sine pulse load at the fixed edge (grid point 3000).

a. Use a **TLOAD2** entry in combination with a **DAREA** and the given information on page WS10A-3:

- Time = **0 to .004 sec**
- Frequency = **250 HZ**
- Phase angle = **-90°**

```
$
$   soln10A.dat
$
SOL 109
TIME 30
CEND
TITLE= TRANSIENT RESPONSE
SUBTITLE= USING DIRECT TRANSIENT METHOD
LABEL= SHOCK SPECTRUM CALCULATION
ECHO= UNSORTED
SPC= 100
SET 111= 3000
DISPLACEMENT (SORT2)= 111 $ AT LEAST DISP AND VEL MUST APPEAR
VELOCITY (SORT2)= 111
ACCELERATION (sort2)= 111
DLOAD= 500
TSTEP= 100
$
OUTPUT (XYPLOT)
$
$ SHOCK RESPONSE IS ONLY AVAILABLE IN PLOT OR PUNCH OUTPUT. THEREFORE,
$ THE 'OUTPUT(XYPLOT)' SECTION OF THE CASE CONTROL MUST BE USED.
$
XGRID=YES
YGRID=YES
XYPAPLOT ACCE / 3000(T1)
XLOG= YES
YLOG= YES
$
$ RELATIVE SHOCK RESPONSES ARE CONTAINED IN THE IMAGINARY/PHASE
$ COMPONENTS OF THE OUTPUT
$ ABSOLUTE SHOCK RESPONSES ARE CONTAINED IN THE REAL/MAGNITUDE
$ COMPONENTS OF THE OUTPUT
$
XTITLE= FREQUENCY (CYCLES/SEC)
YTITLE= RELATIVE DISPLACEMENT
XYPLOT DISP SPECTRAL 1 / 3000 (T1IP)
YTITLE= RELATIVE VELOCITY
XYPLOT VELOCITY SPECTRAL 1 / 3000 (T1IP)
YTITLE= ABSOLUTE ACCELERATION
XYPLOT ACCELERATION SPECTRAL 1 / 3000 (T1RM)
$
$ PUNCH SHOCK SPECTRUM FOR LATER USE
$
XYPUNCH ACCELERATION SPECTRAL 1 / 3000(T1RM)
$
BEGIN BULK
$
$ DEFINE GRID POINT
$
GRID, 3000, .0.,.0.,.0., .23456
$
$ DEFINE MASS
$
CMASS2, 100, 1.0, 3000, 1
$
$ APPLY LOADING TO MASS
$
TLOAD2, 500, 600, 0, 0., 0.004, 250., -90.
$
DAREA, 600, 3000, 1, 1.
$
$ SPECIFY INTEGRATION TIME STEPS
$
TSTEP, 100, 100, 4.0E-4, 1
$
ENDDATA
```

# Step 4. Add the Request for Calculation of Spectra

To request calculation of spectra, use **PARAM, RSPECTRA** with a value of **0** for a transient analysis.

```
$
$      soln10A.dat
$
SOL 109
TIME 30
CEND
TITLE= TRANSIENT RESPONSE
SUBTITLE= USING DIRECT TRANSIENT METHOD
LABEL= SHOCK SPECTRUM CALCULATION
ECHO= UNSORTED
SPC= 100
SET 111= 3000
DISPLACEMENT (SORT2)= 111 $ AT LEAST DISP AND VEL MUST APPEAR
VELOCITY (SORT2)= 111
ACCELERATION (sort2)= 111
DLOAD= 500
TSTEP= 100
$
$      OUTPUT (XYPLOT)
$
$      SHOCK RESPONSE IS ONLY AVAILABLE IN PLOT OR PUNCH OUTPUT. THEREFORE,
$      THE 'OUTPUT(XYPLOT)' SECTION OF THE CASE CONTROL MUST BE USED.
$
XGRID=YES
YGRID=YES
XYFAPLOT ACCE / 3000(T1)
XLOG= YES
YLOG= YES
$
$      RELATIVE SHOCK RESPONSES ARE CONTAINED IN THE IMAGINARY/PHASE
$      COMPONENTS OF THE OUTPUT
$      ABSOLUTE SHOCK RESPONSES ARE CONTAINED IN THE REAL/MAGNITUDE
$      COMPONENTS OF THE OUTPUT
$
XTITLE= FREQUENCY (CYCLES/SEC)
YTITLE= RELATIVE DISPLACEMENT
XYPLOT DISP SPECTRAL 1 / 3000 (T1IP)
YTITLE= RELATIVE VELOCITY
XYPLOT VELOCITY SPECTRAL 1 / 3000 (T1IP)
YTITLE= ABSOLUTE ACCELERATION
XYPLOT ACCELERATION SPECTRAL 1 / 3000 (T1RM)
$
$      PUNCH SHOCK SPECTRUM FOR LATER USE
$
XYPUNCH ACCELERATION SPECTRAL 1 / 3000(T1RM)
$
BEGIN BULK
$
$      DEFINE GRID POINT
$
GRID, 3000, .0.,.0.,.0., .,23456
$
$      DEFINE MASS
$
CMASS2, 100, 1.0, 3000, 1
$
$      APPLY LOADING TO MASS
$
TLOAD2, 500, 600, ., 0, 0., 0.004, 250., -90.
$
DAREA, 600, 3000, 1, 1.
$
$      SPECIFY INTEGRATION TIME STEPS
$
TSTEP, 100, 100, 4.0E-4, 1
$
$      PARAMETER TO CALCULATE SHOCK SPECTRUM
$
PARAM, RSPECTRA, 0
$
ENDDATA
```

# Step 5. Add Damping and Natural Frequencies

- a. Use the entry **FREQ** to specify damping of **0**, **2**, and **4** percent .
- b. Use the **FREQ1** entry to specify the natural frequencies of oscillator.

```
YGRID=YES
XYPAPLOT ACCE / 3000(T1)
XLOG= YES
YLOG= YES
$
$ RELATIVE SHOCK RESPONSES ARE CONTAINED IN THE IMAGINARY/PHASE
$ COMPONENTS OF THE OUTPUT
$ ABSOLUTE SHOCK RESPONSES ARE CONTAINED IN THE REAL/MAGNITUDE
$ COMPONENTS OF THE OUTPUT
$
XTITLE= FREQUENCY (CYCLES/SEC)
YTITLE= RELATIVE DISPLACEMENT
XYPLOT DISP SPECTRAL 1 / 3000 (T1IP)
YTITLE= RELATIVE VELOCITY
XYPLOT VELOCITY SPECTRAL 1 / 3000 (T1IP)
YTITLE= ABSOLUTE ACCELERATION
XYPLOT ACCELERATION SPECTRAL 1 / 3000 (T1RM)
$
$ PUNCH SHOCK SPECTRUM FOR LATER USE
$
XYPUNCH ACCELERATION SPECTRAL 1 / 3000(T1RM)
$
BEGIN BULK
$
$ DEFINE GRID POINT
$
GRID, 3000, ,0.,0.,0., ,23456
$
$ DEFINE MASS
$
CMASS2, 100, 1.0, 3000, 1
$
$ APPLY LOADING TO MASS
$
TLOAD2, 500, 600, , 0, 0., 0.004, 250., -90.
$
DAREA, 600, 3000, 1, 1.
$
$ SPECIFY INTEGRATION TIME STEPS
$
TSTEP, 100, 100, 4.0E-4, 1
$
$ PARAMETER TO CALCULATE SHOCK SPECTRUM
$
PARAM, RSPECTRA, 0
$
$ DAMPING INFORMATION FOR OSCILLATORS
$
a FREQ, 111, 0., 0.02, 0.04
$
$ NATURAL FREQUENCIES OF OSCILLATORS
$
b FREQ1, 222, 20., 20., 49
$
ENDDATA
```

# Step 6. Add Entry to correlate Frequency and Damping Requests

To correlate the frequency and damping request, use **DTI**, **SPSEL** entry to specify frequency and damping values for the oscillator at GRID point **3000**.

```

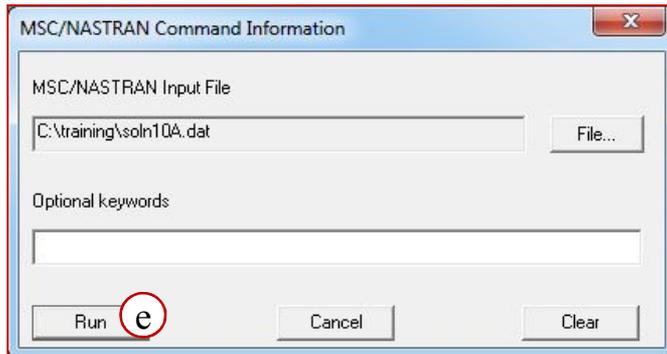
* COMPONENTS OF THE SDOF
$
XTITLE= FREQUENCY (CYCLES/SEC)
YTITLE= RELATIVE DISPLACEMENT
XYPLOT DISP SPECTRAL 1 / 3000 (T1IP)
VTITLE= RELATIVE VELOCITY
XYPLOT VELOCITY SPECTRAL 1 / 3000 (T1IP)
YTITLE= ABSOLUTE ACCELERATION
XYPLOT ACCELERATION SPECTRAL 1 / 3000 (T1RM)
$
$ PUNCH SHOCK SPECTRUM FOR LATER USE
$
XYPUNCH ACCELERATION SPECTRAL 1 / 3000(T1RM)
$
BEGIN BULK
$
$ DEFINE GRID POINT
$
GRID, 3000, .0..0..0., .23456
$
$ DEFINE MASS
$
CMASS2, 100, 1.0, 3000, 1
$
$ APPLY LOADING TO MASS
$
TLOAD2, 500, 600, ., 0, 0., 0.004, 250., -90.
$
DAREA, 600, 3000, 1, 1.
$
$ SPECIFY INTEGRATION TIME STEPS
$
TSTEP, 100, 100, 4.0E-4, 1
$
$ PARAMETER TO CALCULATE SHOCK SPECTRUM
$
PARAM, RSPECTRA, 0
$
$ DAMPING INFORMATION FOR OSCILLATORS
$
FREQ, 111, 0., 0.02, 0.04
$
$ NATURAL FREQUENCIES OF OSCILLATORS
$
FREQ1, 222, 20., 20., 49
$
$ SPECIFY FREQUENCY AND DAMPING VALUES FOR
$ THE SDOF OSCILLATORS AT GRID 3000
$
DTI, SPSEL, 0
DTI, SPSEL, 1, 111, 222, 3000
$
$ 1= SUBCASE... 111= DAMPING... 222= FREQUENCIES... 3000= GRID NUMBER
$
ENDDATA

```

# Step 7. Save and Run the New Input File

Save and run the modified file in MSC Nastran.

- a. Save the modified file as **soln10A.dat**
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln10A.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 8. Review the tabular Results

Open the **soln10A.pch** file to see the tabular results of the acceleration spectra data. This tabular data will be used in the next workshop.

```

$SUBCASE      1
$ACCE        4      3000      3      1
$          0.000000E+00
TABLED1      2
  20.      .038684  40.      .15254  60.      .33511  80.      .576058
  100.     .862048  120.     1.17619  140.     1.50169  160.     1.82017
  180.     2.11405  200.     2.36801  220.     2.56617  240.     2.70027
  260.     2.76274  280.     2.75072  300.     2.74632  320.     2.61887
  340.     2.4218  360.     2.39068  380.     2.24931  400.     2.02296
  420.     1.78538  440.     1.70355  460.     1.57056  480.     1.40493
  500.     1.22608  520.     1.20483  540.     1.17613  560.     1.14097
  580.     1.10048  600.     1.05582  620.     1.00818  640.     .958762
  660.     .908726  680.     .859158  700.     .827673  720.     .782131
  740.     .729006  760.     .694086  780.     .668597  800.     .63504
  820.     .598493  840.     .571834  860.     .563066  880.     .550503
  900.     .528848  920.     .509283  940.     .500533  960.     .498019
  980.     .488734  1000.    .468324ENDT

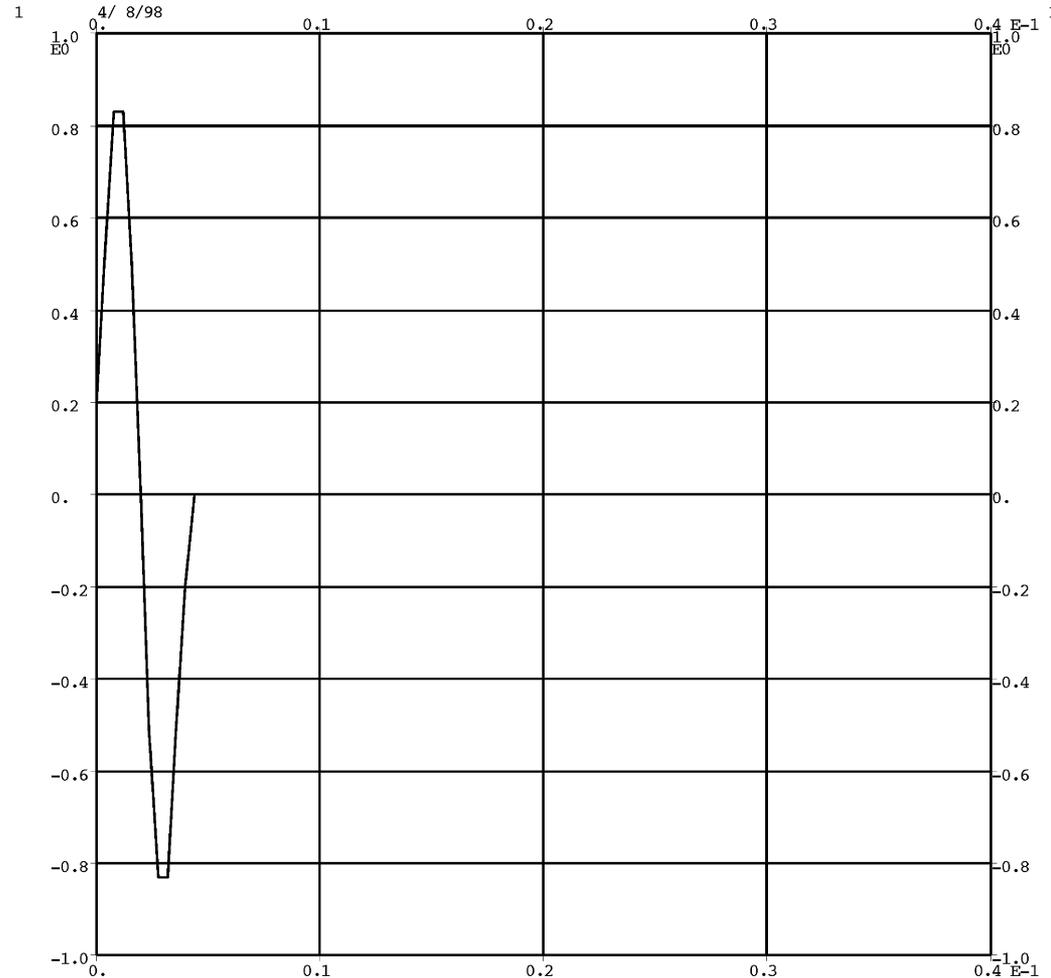
$SUBCASE      1
$ACCE        4      3000      3      1
$          2.000000E-02
TABLED1      3
  20.      .037712  40.      .143379  60.      .314988  80.      .541456
  100.     .809969  120.     1.10538  140.     1.40713  160.     1.69615
  180.     1.98219  200.     2.22274  220.     2.35265  240.     2.53081
  260.     2.56191  280.     2.55563  300.     2.58573  320.     2.45747
  340.     2.2928  360.     2.25739  380.     2.12621  400.     1.92303
  420.     1.68344  440.     1.60986  460.     1.49297  480.     1.34918
  500.     1.19515  520.     1.17318  540.     1.1448  560.     1.11071
  580.     1.072  600.     1.02975  620.     .985074  640.     .939072
  660.     .892781  680.     .847162  700.     .803073  720.     .761247
  740.     .722277  760.     .686602  780.     .654499  800.     .626083
  820.     .601307  840.     .583144  860.     .567999  880.     .548813
  900.     .532571  920.     .520415  940.     .508938  960.     .49739
  980.     .485013  1000.    .47107  ENDT

$SUBCASE      1
$ACCE        4      3000      3      1
$          4.000000E-02
TABLED1      4
  20.      .039345  40.      .137732  60.      .297482  80.      .511465
  100.     .765278  120.     1.04465  140.     1.31663  160.     1.58562
  180.     1.85768  200.     2.10273  220.     2.19188  240.     2.39249
  260.     2.3985  280.     2.42747  300.     2.44087  320.     2.31392
  340.     2.17684  360.     2.13899  380.     2.01787  400.     1.83559
  420.     1.61829  440.     1.52782  460.     1.42521  480.     1.30025
  500.     1.16724  520.     1.14423  540.     1.11633  560.     1.08339
  580.     1.04644  600.     1.0065  620.     .964608  640.     .921751
  660.     .878861  680.     .83678  700.     .796249  720.     .757883
  740.     .722165  760.     .689432  780.     .659873  800.     .633532
  820.     .610311  840.     .589978  860.     .57218  880.     .556463
  900.     .542287  920.     .529047  940.     .516098  960.     .502777
  980.     .488426  1000.    .472416ENDT
    
```

# Step 9. Review the Graphical Results

Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions given in workshop 4, step 9.

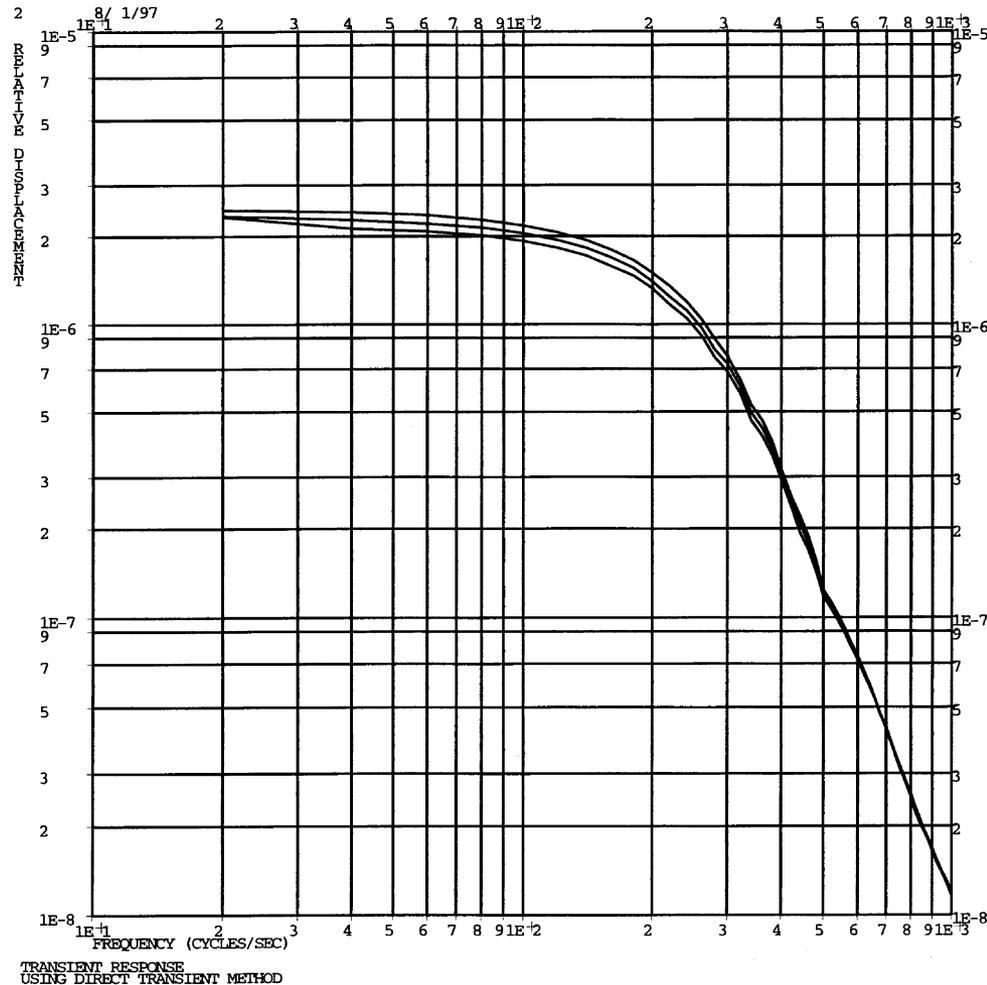
Acceleration shock spectrum  
with damping = 0



TRANSIENT RESPONSE  
USING DIRECT TRANSIENT METHOD  
SHOCK SPECTRUM CALCULATION

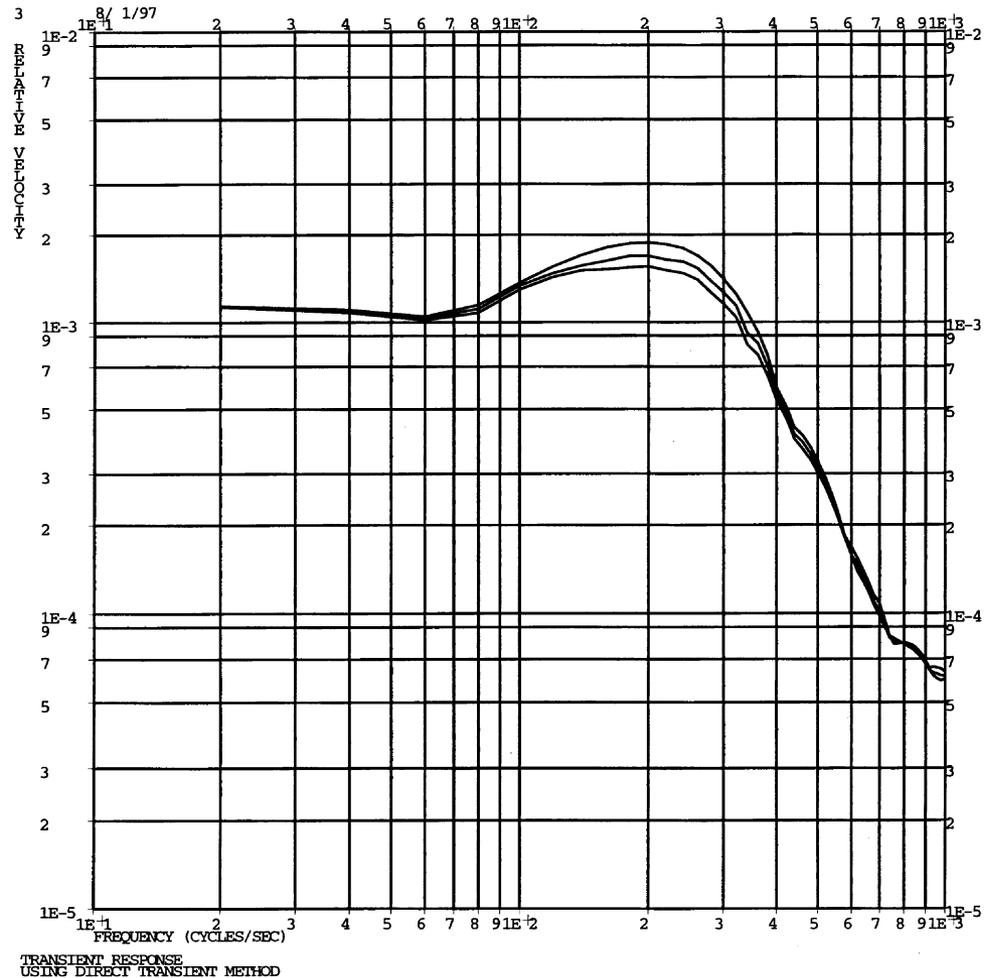
# Step 9. Review the Graphical Results (Cont.)

Relative displacement spectral graph



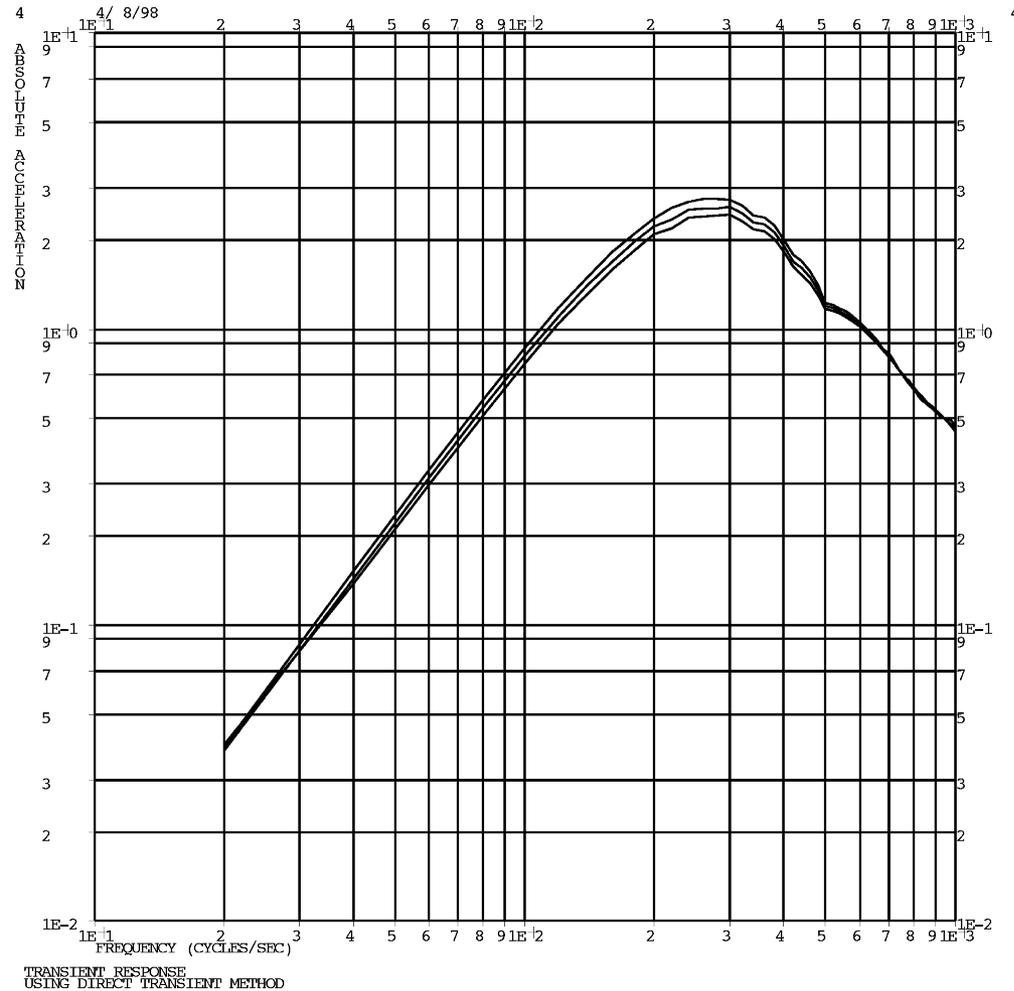
# Step 9. Review the Graphical Results (Cont.)

Relative velocity spectral graph



# Step 9. Review the Graphical Results (Cont.)

Absolute acceleration spectral graph



# **WORKSHOP 10B**

## **APPLY THE SHOCK SPECTRUM**



- **Workshop Objective**

- Apply the shock spectrum generated in workshop 10A and sum the response using the SRSS option.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

- plate.bdf
- wkshp10B.dat

- **Problem Description**

- This is the second part to a two part workshop. In the first part you should have added to the wkshp10A.dat input file the necessary entries to create the shock spectrum. In this workshop you will use the input file wkshp10B.dat and add the necessary entries to apply the shock spectrum. The data for the tables will come from the soln10a.pch file. Be sure to include modes up to 1000 Hz using 3% critical damping. The model is the plate described in workshop 1.

- **Suggested Steps**

1. Open and review the input file wkshp10B.dat
2. Add the specification for shock spectrum.
3. Add Shock tables.
4. Save and run the new input file in MSC Nastran.
5. Review the MSC Nastran results using the solution file soln10B.f06.

# Step 1. Open and Review Input File wkshp10B.dat

The file wkshp10B.dat is the starting input file to be modified.

The following information is already included in the input file.

- Model information, same as workshop 1.
- Boundary condition for clamped modes
- Foundation 1000 lbs mass at base (grid point 23 ) to stimulate clamped modes
- RBE mass at remaining points at the base of plate.
- SUPORT entry at Grid point 23, Z-direction
- Lanczos method of Eigenvalue extraction. Frequency range from 0 to 1000.
- 3% critical Modal damping
- Modal frequency range

```
$
$ wkshp10B.dat
$
$ case control, add: appropriate solution sequence
$
$ bulk data, add: add the specification for shock spectrum,
$ use the srss summing method.
$ apply the response spectrum curves generated
$ in workshop 10a.
$
TIME 30
CEND
TITLE= RESPONSE SPECTRUM ANALYSIS
SUBTITLE= USING CALCULATED SHOCK RESPONSE
LABEL= SHOCK WILL BE INPUT IN Z DIRECTION
ECHO= UNSORTED
SET 111= ALL
DISPLACEMENT= 111
SPC= 200
SUBCASE 1
METHOD= 100
SDAMP= 200
DLOAD= 500
$
$ BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARAM, POST, -1
INCLUDE 'plate.bdf'
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
$ BOUNDRY CONDITIONS FOR 'CLAMPED' MODES
$
SPC1, 200, 1245, 1, 12, 23, 34, 45
$
$ PLACE BIG FOUNDATION MASS (BFM) AT BASE
$ TO STIMULATE 'CLAMPED' MODES
$
CMASS2, 110, 1000., 23, 3
$
$ RBE MASS TO REMAINING BASE POINTS
$
RBE2, 101, 23, 3, 1, 12, 34, 45
$
$ SUPORT CARD TO IDENTIFY EXCITATION DOFS
$
SUPORT, 23, 3
$
$ EIGENVALUE EXTRACTION
$ MUST BE MASS NORMALIZED (DEFAULT)
$
EIGRL, 100, 0., 1000.
$
$ TABLE TO SPECIFY DAMPING FOR USE IN THE ANALYSIS
$
TABDMP1, 200, CRIT,
, 0., 0.03, 1000., 0.03, ENDT
$
$ MODAL FREQUENCY RANGE CAN BE SELECTED USING
$
PARAM, LFREQ, 0.1
$
PARAM, HFREQ, 1000.
$
ENDDATA
```

# Step 2. Add the specification for Shock Spectrum

- a. To add specification of shock spectrum use a **DLOAD**. Make sure that the **DLOAD SID** matches the identification number of the **DLOAD** in the Case Control Section.
- b. To select shock response calculation. Set the **PARAM SCRSPEC** to a value of 0.
- c. Use **PARAM, OPTION, SRSS** to select the SRSS method to combined the modes.

```
$ soln10B.dat
$
SOL 103
TIME 30
CEND
TITLE= RESPONSE SPECTRUM ANALYSIS
SUBTITLE= USING CALCULATED SHOCK RESPONSE
LABEL= SHOCK WILL BE INPUT IN Z DIRECTION
ECHO= UNSORTED
SET 111= ALL
DISPLACEMENT= 111
SPC= 200
SUBCASE 1
METHOD= 100
SDAMP= 200
DLOAD= 500
$
BEGIN BULK
$
$ PLATE MODEL DESCRIBED IN NORMAL MODES EXAMPLE
$
PARM, POST, -1
INCLUDE 'plate.bdf'
PARAM, COUFMASS, 1
PARAM, WTMASS, 0.00259
$
$ BOUNDRY CONDITIONS FOR 'CLAMPED' MODES
$
SPC1, 200, 1245, 1, 12, 23, 34, 45
$
$ PLACE BIG FOUNDATION MASS (BFM) AT BASE
$ TO STIMULATE 'CLAMPED' MODES
$
CHASS2, 110, 1000., 23, 3
$
$ RBE MASS TO REMAINING BASE POINTS
$
RBE2, 101, 23, 3, 1, 12, 34, 45
$
$ SUPORT CARD TO IDENTIFY EXCITATION DOFS
$
SUPORT, 23, 3
$
$ EIGENVALUE EXTRACTION
$ MUST BE MASS NORMALIZED (DEFAULT)
$
EIGRL, 100, 0., 1000.
$
$ TABLE TO SPECIFY DAMPING FOR USE IN THE ANALYSIS
$
TABDMP1, 200, CRIT,
, 0., 0.03, 1000., 0.03, ENDT
$
$ SPECIFICATION OF SHOCK SPECTRUM TO BE USED
$
a DLOAD, 500, 1.0, 2.0, 1
$
$ DLOAD, ID, OVERALL SCALE, SCALE FOR R-SET DOF# 1, SHOCK TABLE FOR DOF# 1,
$ SCALE FOR R-SET DOF# 2, SHOCK TABLE FOR DOF# 2, ETC.
$
$ SELECT SHOCK RESPONSE CALCULATION
$
b PARAM, SCRSPEC, 0
$
$ SELECT SUMMATION OPTION
$
c PARAM, OPTION, SRSS
$
$ MODAL FREQUENCY RANGE CAN BE SELECTED USING
$
PARAM, LFREQ, 0.1
$
PARAM, HFREQ, 1000.
$
ENDDATA
```

# Step 3. Add Shock Tables

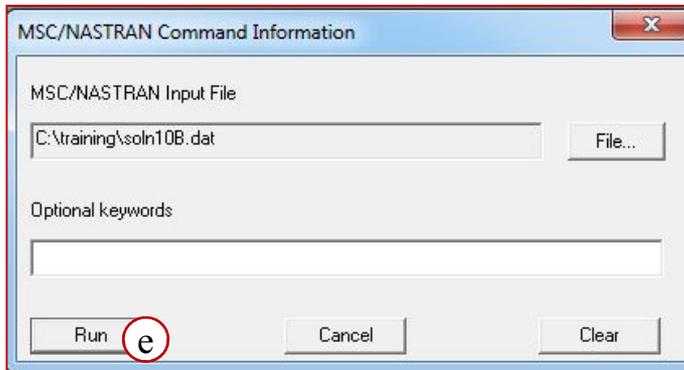
- a. First add the specification for the shock tables using the **DTI SPECSEL** entry.
- b. To add the shock tables, open the file from the previous workshop **soln10a.pch** and copy the tables to this input file for **TABLED1** TID numbers **2, 3, 4**

```
*****
$
$ SPECIFICATION FOR SHOCK TABLES
$
$ DTI, SPECSEL, 0
$ DTI, SPECSEL, 1, , A, 2, 0., 3, 0.02,
$ 4, 0.04, ENDREC
$
$ DTI, SPECSEL, SHOCK TABLE NUMBER, [(A)CCELERATION, (V)ELOCITY, OR (D)ISP],
$ TABLED1 POINTER, DAMPING FOR TABLE, ETC.
$
$ PUNCH OUTPUT FOR SHOCK SPECTRUM CALCULATION
$
$ ACCE 4 3000 3 1
$ 0.000000E+00
$
$
b) TABLED1 2
20. .038683 40. .152539 60. .33511 80. .576059
100. .862049 120. 1.17619 140. 1.50169 160. 1.82018
180. 2.11404 200. 2.36801 220. 2.56617 240. 2.70027
260. 2.76275 280. 2.75073 300. 2.74632 320. 2.61887
340. 2.4218 360. 2.39068 380. 2.24931 400. 2.02296
420. 1.78538 440. 1.70355 460. 1.57056 480. 1.40493
500. 1.22608 520. 1.20483 540. 1.17631 560. 1.14097
580. 1.10048 600. 1.05582 620. 1.00818 640. .958761
660. .908725 680. .859158 700. .827667 720. .782127
740. .728996 760. .694088 780. .668602 800. .635044
820. .598496 840. .571831 860. .563072 880. .550499
900. .528854 920. .509281 940. .500534 960. .498016
980. .488793 1000. .468321 ENDT
$ACCE 4 3000 3 52
$ 2.000000E-02
TABLED1 3
20. .037708 40. .143365 60. .314936 80. .541342
100. .80976 120. 1.10506 140. 1.40671 160. 1.69567
180. 1.98167 200. 2.22217 220. 2.35249 240. 2.53055
260. 2.56231 280. 2.55577 300. 2.58668 320. 2.45921
340. 2.29411 360. 2.25956 380. 2.12901 400. 1.92605
420. 1.68656 440. 1.61355 460. 1.4968 480. 1.35263
500. 1.19796 520. 1.17707 540. 1.14947 560. 1.11613
580. 1.07807 600. 1.03637 620. .992124 640. .946383
660. .900171 680. .854434 700. .810016 720. .767647
740. .727923 760. .691288 780. .658039 800. .628311
820. .602091 840. .579207 860. .559362 880. .542128
900. .526973 920. .51329 940. .500403 960. .487602
980. .474171 1000. .459408 ENDT
$ACCE 4 3000 3 103
$ 4.000000E-02
TABLED1 4
20. .039336 40. .137673 60. .297382 80. .511244
100. .764891 120. 1.04406 140. 1.31588 160. 1.58461
180. 1.85678 200. 2.10175 220. 2.19165 240. 2.3921
260. 2.39929 280. 2.42782 300. 2.44263 320. 2.317
340. 2.17923 360. 2.14283 380. 2.0227 400. 1.8407
420. 1.62279 440. 1.53417 460. 1.43168 480. 1.30597
500. 1.17212 520. 1.15165 540. 1.12513 560. 1.09349
580. 1.05768 600. 1.01868 620. .977462 640. .934986
660. .892143 680. .849752 700. .808538 720. .769114
740. .731968 760. .69746 780. .665814 800. .637115
820. .611319 840. .588261 860. .567655 880. .549125
900. .532205 920. .516369 940. .501047 960. .485644
980. .469568 1000. .452243 ENDT
$
ENDDATA
```

# Step 4. Save and Run the New Input File

Save and run the modified file in MSC Nastran.

- a. Save the modified file as **soln10B.dat**
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln10B.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 5. Review the Results in the Solution File

To review the results open the soln10b.f06 file.

```

      REAL EIGENVALUES
MODE  EXTRACTION  EIGENVALUE  RADIANS  CYCLES  GENERALIZED  GENERALIZED
NO.   ORDER       EIGENVALUE  RADIANS  CYCLES  MASS         STIFFNESS
  1     1         0.0         0.0      0.0      1.000000E+00  0.0
  2     2       7.057114E+05  8.400663E+02  1.337007E+02  1.000000E+00  7.057114E+05
  3     3       1.877186E+07  4.332651E+03  6.895628E+02  1.000000E+00  1.877186E+07
  4     4       2.811329E+07  5.302197E+03  8.438708E+02  1.000000E+00  2.811329E+07
^^^
*** USER INFORMATION MESSAGE 9047 (SUBDMAP POSTREIG)
    SCALED RESPONSE SPECTRA FOR RESIDUAL STRUCTURE ONLY
^^^
*** USER INFORMATION MESSAGE 7588 (GKAM)
    BASED ON THE USER PARAMETERS LMODES, LFREQ OR HFREQ, ONLY      3 OF THE      4 COMPUTED STRUCTURE MODES
    (MODES      2 THROUGH      4) WILL BE USED IN THIS MODAL TRANSIENT RESPONSE ANALYSIS
    (DETAILS OF THE EIGENVALUE DATA FOR THE MODES USED ARE GIVEN BELOW)
1  RESPONSE SPECTRUM ANALYSIS                                     JUNE 17, 2013  MSC Nastran  3/22/13  PAGE  14
0  USING CALCULATED SHOCK RESPONSE
    SHOCK WILL BE INPUT IN Z DIRECTION                                     SUBCASE 1

      REAL EIGENVALUES
      (ACTUAL MODES USED IN THE DYNAMIC ANALYSIS)
MODE  EXTRACTION  EIGENVALUE  RADIANS  CYCLES  GENERALIZED  GENERALIZED
NO.   ORDER       EIGENVALUE  RADIANS  CYCLES  MASS         STIFFNESS
  2     2       7.057114E+05  8.400663E+02  1.337007E+02  1.000000E+00  7.057114E+05
  3     3       1.877186E+07  4.332651E+03  6.895628E+02  1.000000E+00  1.877186E+07
  4     4       2.811329E+07  5.302197E+03  8.438708E+02  1.000000E+00  2.811329E+07

```

# Step 5. Review the Results in the Solution File (Cont.)

RESPONSE SPECTRUM ANALYSIS										PAGE	19
USING CALCULATED SHOCK RESPONSE											
SHOCK WILL BE INPUT IN Z DIRECTION										SUBCASE 1	
SCALED SPECTRAL RESPONSE, SRSS OPTION											
D I S P L A C E M E N T										V E C T O R	
POINT ID.	TYPE	T1	T2	T3	R1	R2	R3				
1	G	0.0	0.0	6.222940E-10	0.0	0.0	7.935691E-19				
2	G	1.656957E-18	7.935692E-19	7.362169E-08	8.380406E-08	3.053683E-07	1.051390E-18				
3	G	3.038116E-18	1.358444E-18	3.172597E-07	1.218669E-07	6.622535E-07	1.255203E-18				
4	G	4.072766E-18	2.361845E-18	7.194942E-07	1.166965E-07	9.376346E-07	1.666441E-18				
5	G	4.328389E-18	3.551950E-18	1.246647E-06	1.041301E-07	1.160351E-06	1.080336E-18				
6	G	3.627728E-18	4.017596E-18	1.870941E-06	8.255398E-08	1.326449E-06	9.151231E-19				
7	G	2.420518E-18	3.036923E-18	2.566087E-06	6.151257E-08	1.444593E-06	3.255618E-18				
8	G	1.341661E-18	8.730071E-19	3.309156E-06	4.199305E-08	1.519643E-06	4.678898E-18				
9	G	6.757277E-19	1.706825E-18	4.080598E-06	2.667464E-08	1.560018E-06	5.025599E-18				
10	G	3.296047E-19	4.233287E-18	4.865306E-06	1.686023E-08	1.575035E-06	5.004866E-18				
11	G	2.095948E-19	6.747358E-18	5.653790E-06	1.297877E-08	1.577920E-06	5.028553E-18				
12	G	0.0	0.0	6.222940E-10	0.0	0.0	3.374295E-19				
13	G	1.284789E-18	3.374295E-19	9.575232E-08	1.422466E-08	3.706305E-07	7.431859E-19				
14	G	2.567051E-18	1.025792E-18	3.578117E-07	4.377303E-08	6.681862E-07	1.214033E-18				
15	G	3.503078E-18	2.147589E-18	7.614714E-07	5.341377E-08	9.365016E-07	1.493373E-18				
16	G	4.075929E-18	3.476097E-18	1.284625E-06	4.872339E-08	1.147595E-06	8.960050E-19				
17	G	4.285337E-18	4.111313E-18	1.901705E-06	4.106761E-08	1.312830E-06	9.204374E-19				
18	G	4.103842E-18	3.290782E-18	2.589259E-06	3.140395E-08	1.430604E-06	3.124885E-18				
19	G	3.648684E-18	1.175248E-18	3.325306E-06	2.262744E-08	1.507978E-06	4.599421E-18				
20	G	3.148179E-18	1.474161E-18	4.091200E-06	1.553729E-08	1.551421E-06	5.119173E-18				
21	G	2.814204E-18	4.149320E-18	4.872369E-06	1.099402E-08	1.570711E-06	5.200536E-18				
22	G	2.724076E-18	6.779860E-18	5.659360E-06	8.939463E-09	1.576600E-06	5.228438E-18				
23	G	0.0	0.0	6.222940E-10	0.0	0.0	0.0				
24	G	1.196377E-18	0.0	9.885985E-08	1.796845E-17	3.798827E-07	5.093010E-19				
25	G	2.420211E-18	6.742267E-19	3.681180E-07	9.822498E-18	6.838622E-07	1.159155E-18				
26	G	3.536324E-18	1.878780E-18	7.747086E-07	9.786365E-19	9.332841E-07	1.342422E-18				
27	G	4.500103E-18	3.185220E-18	1.296676E-06	2.041427E-17	1.145849E-06	7.381549E-19				
28	G	5.283288E-18	3.918342E-18	1.911939E-06	3.836081E-17	1.307837E-06	7.453452E-19				
29	G	5.734223E-18	3.395828E-18	2.597088E-06	5.211755E-17	1.426339E-06	2.702517E-18				
30	G	5.775559E-18	1.523178E-18	3.330967E-06	3.282461E-17	1.503985E-06	4.362045E-18				
31	G	5.589506E-18	1.155372E-18	4.095104E-06	2.811199E-18	1.548690E-06	5.300022E-18				
32	G	5.424978E-18	4.061999E-18	4.875149E-06	1.780149E-17	1.569137E-06	5.633833E-18				
33	G	5.405391E-18	6.940042E-18	5.661615E-06	7.842894E-18	1.576083E-06	5.696025E-18				
34	G	0.0	0.0	6.222940E-10	0.0	0.0	3.185051E-19				
35	G	9.404143E-19	3.185051E-19	9.575232E-08	1.422466E-08	3.706305E-07	3.298516E-19				
36	G	2.113821E-18	2.647971E-19	3.578117E-07	4.377303E-08	6.681862E-07	1.390967E-18				
37	G	3.329228E-18	1.502156E-18	7.614714E-07	5.341377E-08	9.365016E-07	1.758861E-18				
38	G	4.639182E-18	2.779863E-18	1.284625E-06	4.872339E-08	1.147595E-06	1.256388E-18				
39	G	5.986635E-18	3.597597E-18	1.901705E-06	4.106761E-08	1.312830E-06	0.0				
40	G	7.113710E-18	3.370403E-18	2.589259E-06	3.140395E-08	1.430604E-06	2.098707E-18				
41	G	7.821573E-18	1.755290E-18	3.325306E-06	2.262744E-08	1.507978E-06	4.184268E-18				
42	G	8.163046E-18	9.312579E-19	4.091200E-06	1.553729E-08	1.551421E-06	5.564552E-18				
43	G	8.297201E-18	4.019585E-18	4.872369E-06	1.099402E-08	1.570711E-06	6.097018E-18				
44	G	8.360041E-18	7.134714E-18	5.659360E-06	8.939463E-09	1.576600E-06	6.178330E-18				
45	G	0.0	0.0	6.222940E-10	0.0	0.0	6.170719E-19				
46	G	8.014713E-19	6.170719E-19	7.362169E-08	8.380406E-08	3.053683E-07	0.0				

# **WORKSHOP 11**

## **RANDOM RESPONSE WITH SINGLE INPUT**



- **Workshop Objective**

- For the plate (from workshop 1) with a base motion in the z-direction (described on the next page), determine the acceleration PSD response at the drive point (grid point 9999) and at the corner and center of the tip of the plate (grid points 33 and 55).

- **Software Version**

- MSC Nastran 2013

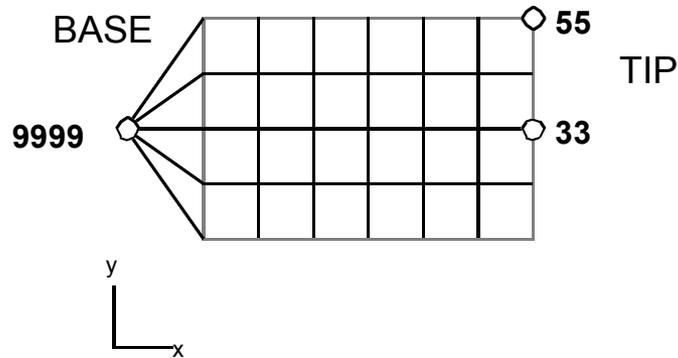
- **Files Required**

- plate.bdf
- wkshp11.dat

- **Problem Description Continued:**

- Apply the base a motion in the z-direction to the plate using the power spectral density, (PSD) described on the next page.

## Problem Description Continued



Autospectra of the Base Excitation	
Frequency (Hz)	G2/Hz
20	0.1
30	1
100	1
500	0.1
1000	0.1

- Connect the base of the plate with an RBE2 to grid point 9999 and apply the enforced motion at grid point 9999
- Use a modal solution.
- Assume a constant critical damping ratio of 3% across the whole frequency range.
- Use a log-log input for the PSD.
- Determine the acceleration PSD response at the drive point (grid point 9999) and at the corner and center of the tip (grid points 33 and 55)
- Request output in both print and xyplot format

- **Suggested Steps**

1. Open and review the input file wkshp11.dat.
2. Add output plots for PSD data.
3. Add Eigenvalue method.
4. Add Modal damping.
5. Add enforced motion at Grid point 9999.
6. Add the frequency steps.
7. Add the spectral density.
8. Save and run the new input file in MSC Nastran.
9. Review the MSC Nastran results using the solution file soln11.f06.
10. Review the graph results.

# Step 1. Open and Review Input File wkshp11.dat

This is the starting input file to be modified.

Plot a logarithmic y-axis

Grid point 9999 is already defined

```
$
$ wkshp11.dat
$
$ case control, add : plot command for psd output
$
$ bulk data, add : enforced motion at grid point 9999
$ modal damping
$ forcing frequencies
$ random input
$ eigenvalue method
$
SOL 111
CEND
TITLE= RANDOM ANALYSIS - BASE EXCITATION
SUBTITLE= USING THE MODAL METHOD WITH LANCZOS
ECHO= UNSORTED
SPC= 101
SET 111= 33, 55, 9999
ACCELERATION(SORT2,PHASE)= 111
METHOD= 100
FREQUENCY= 200
SDAMPING= 300
RANDOM= 400
DLOAD= 500
$
OUTPUT(XY PLOT)
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
XTITLE= FREQUENCY
YTTITLE= ACCEL RESPONSE BASE, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT BASE, PHASE
XY PLOT ACCEL RESPONSE / 9999 (T3RM, T3IP)
YTTITLE= ACCEL RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT TIP CENTER, PHASE
XY PLOT ACCEL RESPONSE / 33 (T3RM, T3IP)
YTTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, PHASE
XY PLOT ACCEL RESPONSE / 55 (T3RM, T3IP)
$
$ PLOT OUTPUT IS ONLY MEANS OF VIEWING PSD DATA
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
GRID, 9999, , 0., 1., 0.
$
RBE2, 101, 9999, 12345, 1, 12, 23, 34, 45
$
SPC1, 101, 12456, 9999
$
ENDDATA
```

# Step 2. Add Output Plots for PSD Data

Add the XY Plot commands to print plots of the PSD data at the loaded base point (grid 9999), at tip center (grid 33) and at tip corner (grid 55) as shown to the right.

```
$
$   so1n11.dat
$
SOL 111
CEND
TITLE= RANDOM ANALYSIS - BASE EXCITATION
SUBTITLE= USING THE MODAL METHOD WITH LANCZOS
ECHO= UNSORTED
SPC= 101
SET 111= 33, 55, 9999
ACCELERATION(real,PHASE)= 111
METHOD= 100
FREQUENCY= 200
SDAMPING= 300
RANDOM= 400
DLOAD= 500
$
OUTPUT(XY PLOT)
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
XTITLE= FREQUENCY
YTITLE= ACCEL RESPONSE BASE, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT BASE, PHASE
XY PLOT ACCEL RESPONSE / 9999 (T3RM, T3IP)
YTITLE= ACCEL RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT TIP CENTER, PHASE
XY PLOT ACCEL RESPONSE / 33 (T3RM, T3IP)
YTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, PHASE
XY PLOT ACCEL RESPONSE / 55 (T3RM, T3IP)
$
$ PLOT OUTPUT IS ONLY MEANS OF VIEWING PSD DATA
$
XGRID= YES
YGRID= YES
XLOG= YES
YLOG= YES
YTITLE= ACCEL P S D AT LOADED CORNER
XY PLOT ACCEL PSDF / 9999(T3)
YTITLE= ACCEL P S D AT TIP CENTER
XY PLOT ACCEL PSDF / 33(T3)
YTITLE= ACCEL P S D AT OPPOSITE CORNER
XY PLOT ACCEL PSDF / 55(T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
GRID, 9999, , 0., 1., 0.
$
RBE2, 101, 9999, 12345, 1, 12, 23, 34, 45
$
SPC1, 101, 12456, 9999
$
ENDDATA
```

# Step 3. Add the Eigenvalue Method

To add the eigenvalue Method:

- a. Use the **EIGRL** entry with a frequency range of interest from **0 to 2000**. (see note below)
- b. Make sure that the **METHOD** Case Control command identification number matches the **EIGRL** SID.

```
$
$ soln11.dat
$
$ SOL 111
$ CEND
$ TITLE= RANDOM ANALYSIS - BASE EXCITATION
$ SUBTITLE= USING THE MODAL METHOD WITH LANZCOS
$ ECHO= UNSORTED
$ SPC= 101
$ SET 111= 33, 55, 9999
$ ACCELERATION(real_PHASE)= 111
$ METHOD= 100
$ FREQUENCY= 200
$ SDAMPING= 1300
$ RANDOM= 400
$ DLOAD= 500
$
$ OUTPUT(XY PLOT)
$ XTGRID= YES
$ YTGRID= YES
$ XBGRID= YES
$ YBGRID= YES
$ YTLOG= YES
$ XTITLE= FREQUENCY
$ YTTITLE= ACCEL RESPONSE BASE, MAGNITUDE
$ YBTITLE= ACCEL RESPONSE AT BASE, PHASE
$ XY PLOT ACCEL RESPONSE / 9999 (T3RM, T3IP)
$ YTTITLE= ACCEL RESPONSE AT TIP CENTER, MAGNITUDE
$ YBTITLE= ACCEL RESPONSE AT TIP CENTER, PHASE
$ XY PLOT ACCEL RESPONSE / 33 (T3RM, T3IP)
$ YTTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, MAGNITUDE
$ YBTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, PHASE
$ XY PLOT ACCEL RESPONSE / 55 (T3RM, T3IP)
$
$ PLOT OUTPUT IS ONLY MEANS OF VIEWING PSD DATA
$
$ XGRID= YES
$ YGRID= YES
$ XLOG= YES
$ YLOG= YES
$ YTTITLE= ACCEL P S D AT LOADED CORNER
$ XY PLOT ACCEL PSDF / 9999(T3)
$ YTTITLE= ACCEL P S D AT TIP CENTER
$ XY PLOT ACCEL PSDF / 33(T3)
$ YTTITLE= ACCEL P S D AT OPPOSITE CORNER
$ XY PLOT ACCEL PSDF / 55(T3)
$
$ BEGIN BULK
$ PARAM, POST, 0
$ PARAM, COUPMASS, 1
$ PARAM, WTMASS, 0.00259
$
$ INCLUDE 'plate.bdf'
$
$ GRID, 9999, , 0., 1., 0.
$
$ RBE2, 101, 9999, 12345, 1, 12, 23, 34, 45
$
$ SPC1, 101, 12456, 9999
$
$ EIGENVALUE EXTRACTION PARAMETERS
$ EIGRL, 100, 2000.
$ ENDDATA
```

The frequency range here just needs to be larger than the frequency range of the base excitation.

# Step 4. Add Modal Damping

To add a constant critical damping ratio of 3% across the whole frequency range

a. Use the **TABDMP1** entry

- TID = **300** (note must match identification number from SDAMPING in Case Control)
- Type = **CRIT**
- First Natural Freq. = **0.0**
- Damping Value = **.03**
- Last Natural Freq. = **10.0** (see note below)
- Damping Value = **.03**

Tables in MSC Nastran are extrapolated. Since in this case, the table represents a straight line, then any two points on that line will work.

```
soln11.dat
*****
SOL 111
CEND
TITLE= RANDOM ANALYSIS - BASE EXCITATION
SUBTITLE= USING THE MODAL METHOD WITH LANCZOS
ECHO= UNSORTED
SPC= 101
SET 111= 33, 55, 9999
ACCELERATION(real,PHASE)= 111
METHOD= 100
FREQUENCY= 200
SDAMPING= 300
RANDOM= 400
DLOAD= 500
$
OUTPUT(XY PLOT)
XTGRID= YES
YTGRID= YES
XBGRID= YES
YBGRID= YES
YTLOG= YES
XTITLE= FREQUENCY
YTITLE= ACCEL RESPONSE BASE, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT BASE, PHASE
XY PLOT ACCEL RESPONSE / 9999 (T3RM, T3IP)
YTITLE= ACCEL RESPONSE AT TIP CENTER, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT TIP CENTER, PHASE
XY PLOT ACCEL RESPONSE / 33 (T3RM, T3IP)
YTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YBTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, PHASE
XY PLOT ACCEL RESPONSE / 55 (T3RM, T3IP)
$
$ PLOT OUTPUT IS ONLY MEANS OF VIEWING PSD DATA
$
XGRID= YES
YGRID= YES
XLOG= YES
YLOG= YES
YTITLE= ACCEL P S D AT LOADED CORNER
XY PLOT ACCEL PSDF / 9999(T3)
YTITLE= ACCEL P S D AT TIP CENTER
XY PLOT ACCEL PSDF / 33(T3)
YTITLE= ACCEL P S D AT OPPOSITE CORNER
XY PLOT ACCEL PSDF / 55(T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COUPMASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
GRID, 9999, , 0., 1., 0.
$
RBE2, 101, 9999, 12345, 1, 12, 23, 34, 45
$
SPC1, 101, 12456, 9999
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
SIGRL, 100, , 2000.
$
$ SPECIFY MODAL DAMPING
TABDMP1, 300, CRIT,
, 0., .03, 10., .03, ENDT
$
ENDDATA
```

a

# Step 5. Add Enforced Motion at Base of Plate

Apply at the base a motion in the z-direction using the given power spectral density, (PSD).

- a. **SPC1** – grid point 9999, z direction.
- b. **SPCD** – Apply enforced motion to point 9999 in z direction.
- c. **RLOAD 2** – define excitation as enforced acceleration and point to **SPCD** and **TABLED1**. Make sure the SID for the **RLOAD2** entry matches the identification number for the **DLOAD** in the Case Control section.
- d. **TABLED1** – add frequencies for loading.

```
!FREQUENCY= 200
!SDAMPING= 300
!RANDOM= 400
!DLOAD= 500
$
!OUTPUT(XY PLOT)
!XTGRID= YES
!YTGRID= YES
!XDGRID= YES
!YBGRID= YES
!YTLOG= YES
!XTITLE= FREQUENCY
!YTTITLE= ACCEL RESPONSE BASE, MAGNITUDE
!YBTITLE= ACCEL RESPONSE AT BASE, PHASE
!XY PLOT ACCEL RESPONSE / 9999 (T3RM, T3IP)
!YTTITLE= ACCEL RESPONSE AT TIP CENTER, MAGNITUDE
!YBTITLE= ACCEL RESPONSE AT TIP CENTER, PHASE
!XY PLOT ACCEL RESPONSE / 33 (T3RM, T3IP)
!YTTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, MAGNITUDE
!YBTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, PHASE
!XY PLOT ACCEL RESPONSE / 55 (T3RM, T3IP)
$
! PLDT OUTPUT IS ONLY MEANS OF VIEWING PSD DATA
$
!XGRID= YES
!YGRID= YES
!XLOG= YES
!YLOG= YES
!YTITLE= ACCEL P S D AT LOADED CORNER
!XY PLOT ACCEL PSDF / 9999(T3)
!YTITLE= ACCEL P S D AT TIP CENTER
!XY PLOT ACCEL PSDF / 33(T3)
!YTITLE= ACCEL P S D AT OPPOSITE CORNER
!XY PLOT ACCEL PSDF / 55(T3)
$
!BEGIN BULK
!PARAM, POST, 0
!PARAM, COMPMASS, 1
!PARAM, WTMASS, 0.00259
$
!INCLUDE 'plate.bdf'
$
!GRID, 9999, , 0., 1., 0.
$
!RBE2, 101, 9999, 12345, 1, 12, 23, 34, 45
$
!SPC1, 101, 12456, 9999
$
! EIGENVALUE EXTRACTION PARAMETERS
$
!EIGRL, 100, , 2000.
$
! SPECIFY MODAL DAMPING
$
!TABDMP1, 300, CRIT,
!, 0., .03, 10., .03, ENDT
$
! LOADING AT BASE
$
!RLOAD2, 500, 600, , , 310.,A
$
!SPCD, 600, 9999, 3, 1.0
$
!SPC1, 101, 3, 9999
$
!TABLED1, 310,
!, 10., 1., 1000., 1., ENDT
$
!ENDDATA
```

c  
b  
a  
d

# Step 6. Add Frequency Steps

Make sure the SIDs for the **FREQ**, **FREQ1**, **FREQ4** steps matches the **FREQUENCY** identification number in the Case Control section.

```
METHOD= 100
FREQUENCY= 100
SDAMPING= 300
RANDOM= 400
D_LOAD= 500
$
OUTPUT (XYPLO)
XTRID= YES
YTRID= YES
XGRID= YES
YGRID= YES
YLOG= YES
XTITLE= FREQUENCY
YTITLE= ACCEL RESPONSE BASE, MAGNITUDE
YSTITLE= ACCEL RESPONSE AT BASE, PHASE
XYPLOT ACCEL RESPONSE / 9999 (T3R, T3IP)
YTITLE= ACCEL RESPONSE AT TIP CENTER, MAGNITUDE
YSTITLE= ACCEL RESPONSE AT TIP CENTER, PHASE
XYPLOT ACCEL RESPONSE / 33 (T3R, T3IP)
YTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, MAGNITUDE
YSTITLE= ACCEL RESPONSE AT OPPOSITE CORNER, PHASE
XYPLOT ACCEL RESPONSE / 55 (T3R, T3IP)
$
$ PLOT OUTPUT IS ONLY MEANS OF VIEWING PSD DATA
$
XGRID= YES
YGRID= YES
XLOG= YES
YLOG= YES
YTITLE= ACCEL P S D AT LOADED CORNER
XYPLOT ACCEL PSD / 9999 (T3)
YTITLE= ACCEL P S D AT TIP CENTER
XYPLOT ACCEL PSD / 33 (T3)
YTITLE= ACCEL P S D AT OPPOSITE CORNER
XYPLOT ACCEL PSD / 55 (T3)
$
BEGIN BULK
PARAM, POST, 0
PARAM, COMPASS, 1
PARAM, WTMASS, 0.00259
$
INCLUDE 'plate.bdf'
$
GRID, 9999, , 0, 1, 0,
$
RBE2, 100, 9999, 1, 12, 23, 34, 45
$
SPC1, 100, 12456, 9999
$
$ EIGENVALUE EXTRACTION PARAMETERS
$
EIGRL, 100, , 2000.
$
$ SPECIFY MODAL DAMPING
$
TABDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$
$ LOADING AT BASE
$
RLOAD2, 500, 600, , , 310, , A
$
SPCD, 600, 9999, 3, 1, 0
$
SPC1, 100, 3, 9999
$
TABLED1, 310,
+, 10., 1., 1000., 1., ENDT
$
$ SPECIFY FREQUENCY STEPS
$
FREQ, 200, 20.
$
FREQ1, 200, 20., 20., 50
$
FREQ4, 200, 20., 1000., .03, 5
$
ENDDATA
```

# Step 7. Add Spectral Density

- a. To define a power spectral density for a random analysis, use **RANDPS** entry.
- Subcase of excited load set = 1
  - Subcase of applied load set = 1
  - Component X = 1.0
  - Component Y = 0
  - Reference **TABRDN1**
  - Make sure that the SID matches the identification number for **RANDOM** in the Case Control section.
- b. The **TABRND1** table defines the power spectral density as a tabular function of frequency for a random analysis. Here the input for the PSD is defined as **log-log**.

```
soln11.dat
*****
SOI 111
CFND
TITLE= RANDOM ANALYSIS - BASE EXCITATION
SUBTITLE= USING THE MODAL METHOD WITH LANCZOS
ECHO= UNSORTED
SPC= 101
SET 111= 33, 55, 9999
ACCELERATION(real,PHASE)= 111
METHOD= 100
FREQUENCY= 200
SDAMPING= 300
RANDOM= 400
ULOAD= 500
$
OUTPUT(XYFLOT)
XTGRID= YES
YTGRID= YES
*****
$ EIGENVALUE EXTRACTION PARAMETERS
EIGRL, 100, , 2000.
$ SPECIFY MODAL DAMPING
TABDMP1, 300, CRIT,
+, 0., .03, 10., .03, ENDT
$ LOADING AT BASE
RLOAD2, 500, 600, , , 310.,A
SPCD, 600, 9999, 3, 1.0
$ SPC1, 101, 3, 9999
$ TABLED1, 310,
+, 10., 1., 1000., 1., ENDT
$ SPECIFY FREQUENCY STEPS
FREQ, 200, 80.
FREQ1, 200, 20., 20., 50
$
FREQ4, 200, 20., 1000., .03, 5
$ SPECIFY SPECTRAL DENSITY
RANDPS, 400, 1, 1, 1., 0., 111
$
TABRND1, 111, LOG, LOG
+, 20., 0.1, 30., 1., 100., 1., 500., .1,
+, 1000., .1, ENDT
$
ENDDATA
```

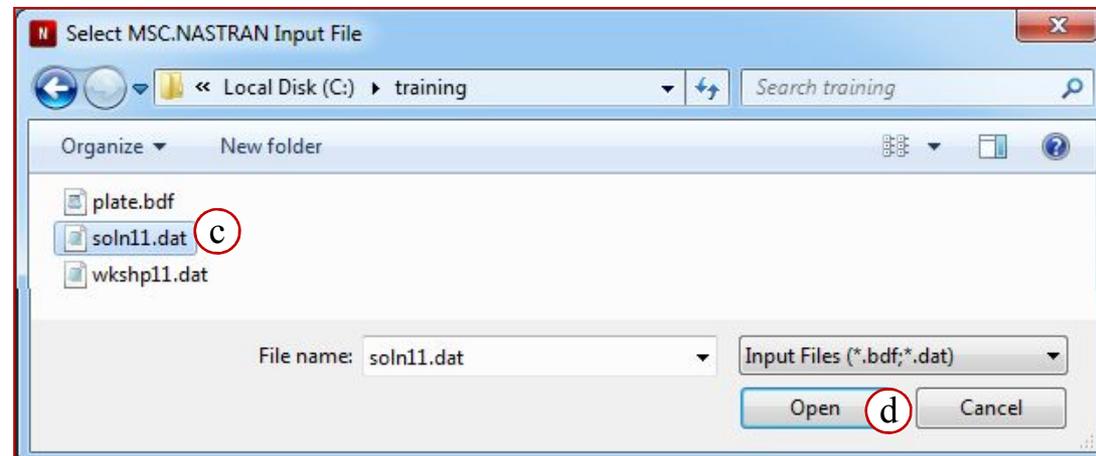
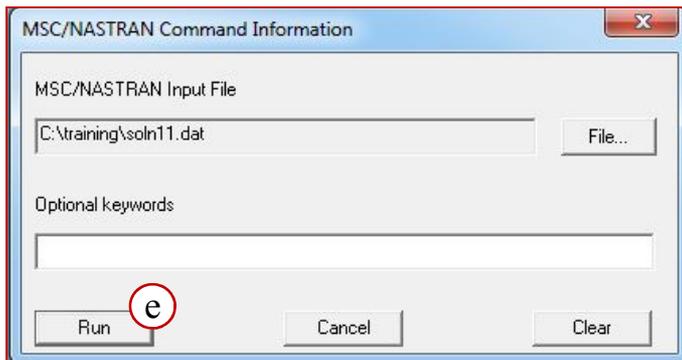
a

b

# Step 8. Save and Run the New Input File

Save and run the modified file in MSC Nastran.

- a. Save the modified file as **soln11.dat**
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln11.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 9. Review the Results in the Solution File

```

POINT-ID =      33
                A C C E L E R A T I O N   V E C T O R
                ( P O W E R S P E C T R A L D E N S I T Y F U N C T I O N )

    FREQUENCY  TYPE      T1          T2          T3          R1          R2          R3
    2.000000E+01  G      9.429874E-20  5.345172E-18  1.072297E-01  3.639218E-14  9.172084E-06  3.280077E-18
    3.000000E+01  G      1.020668E-18  5.729916E-17  1.171321E+00  3.656741E-13  4.931094E-04  3.517079E-17
    4.000000E+01  G      1.143245E-18  6.333425E-17  1.328495E+00  3.682417E-13  1.700950E-03  3.888899E-17
    6.000000E+01  G      1.611707E-18  8.609048E-17  1.937089E+00  3.764784E-13  1.129872E-02  5.291416E-17

                A C C E L E R A T I O N   V E C T O R
                ( R O O T M E A N S Q U A R E )

    POINT ID.  TYPE      T1          T2          T3          R1          R2          R3
         33    G      7.111491E-08  4.604363E-07  9.228146E+01  2.589326E-05  4.589093E+01  3.622042E-07
         55    G      4.229749E-07  4.790235E-07  9.166710E+01  1.969816E+00  4.610508E+01  3.760181E-07
        9999    G      0.0          0.0          1.561982E+01  0.0          0.0          0.0

                A C C E L E R A T I O N   V E C T O R
                ( N U M B E R O F Z E R O C R O S S I N G S )

    POINT ID.  TYPE      T1          T2          T3          R1          R2          R3
         33    G      2.398331E+02  1.828548E+02  3.924336E+02  6.504147E+02  7.319507E+02  1.844837E+02
         55    G      1.916411E+02  1.818598E+02  3.846913E+02  8.502854E+02  7.328314E+02  1.812151E+02
        9999    G      0.0          0.0          3.991722E+02  0.0          0.0          0.0
    
```

# Step 9. Review the Results in the Solution File (Cont.)

XY - O U T P U T S U M M A R Y ( R E S P O N S E )											
0	SUBCASE	CURVE	FRAME	CURVE ID./	XMIN-FRAME/	XMAX-FRAME/	YMIN-FRAME/	X FOR	YMAX-FRAME/	X FOR	
	ID	TYPE	NO.	PANEL : GRID ID	ALL DATA	ALL DATA	ALL DATA	YMIN	ALL DATA	YMAX	
0	1	ACCE	1	9999( 5,--)	2.000000E+01	1.020000E+03	9.999999E-01	1.356945E+02	1.000000E+00	1.296785E+02	
					2.000000E+01	1.020000E+03	9.999999E-01	1.356945E+02	1.000000E+00	1.296785E+02	
0	1	ACCE	1	9999(--, 11)	2.000000E+01	1.020000E+03	0.000000E+00	2.000000E+01	0.000000E+00	2.000000E+01	
					2.000000E+01	1.020000E+03	0.000000E+00	2.000000E+01	0.000000E+00	2.000000E+01	
0	1	ACCE	2	33( 5,--)	2.000000E+01	1.020000E+03	1.008505E+00	3.800000E+02	2.621269E+01	1.336891E+02	
					2.000000E+01	1.020000E+03	1.008505E+00	3.800000E+02	2.621269E+01	1.336891E+02	
0	1	ACCE	2	33(--, 11)	2.000000E+01	1.020000E+03	1.044561E+01	1.020000E+03	3.599818E+02	2.000000E+01	
					2.000000E+01	1.020000E+03	1.044561E+01	1.020000E+03	3.599818E+02	2.000000E+01	
0	1	ACCE	3	55( 5,--)	2.000000E+01	1.020000E+03	1.000849E+00	3.800000E+02	2.617657E+01	1.336891E+02	
					2.000000E+01	1.020000E+03	1.000849E+00	3.800000E+02	2.617657E+01	1.336891E+02	
0	1	ACCE	3	55(--, 11)	2.000000E+01	1.020000E+03	1.055619E+01	1.020000E+03	3.599818E+02	2.000000E+01	
					2.000000E+01	1.020000E+03	1.055619E+01	1.020000E+03	3.599818E+02	2.000000E+01	

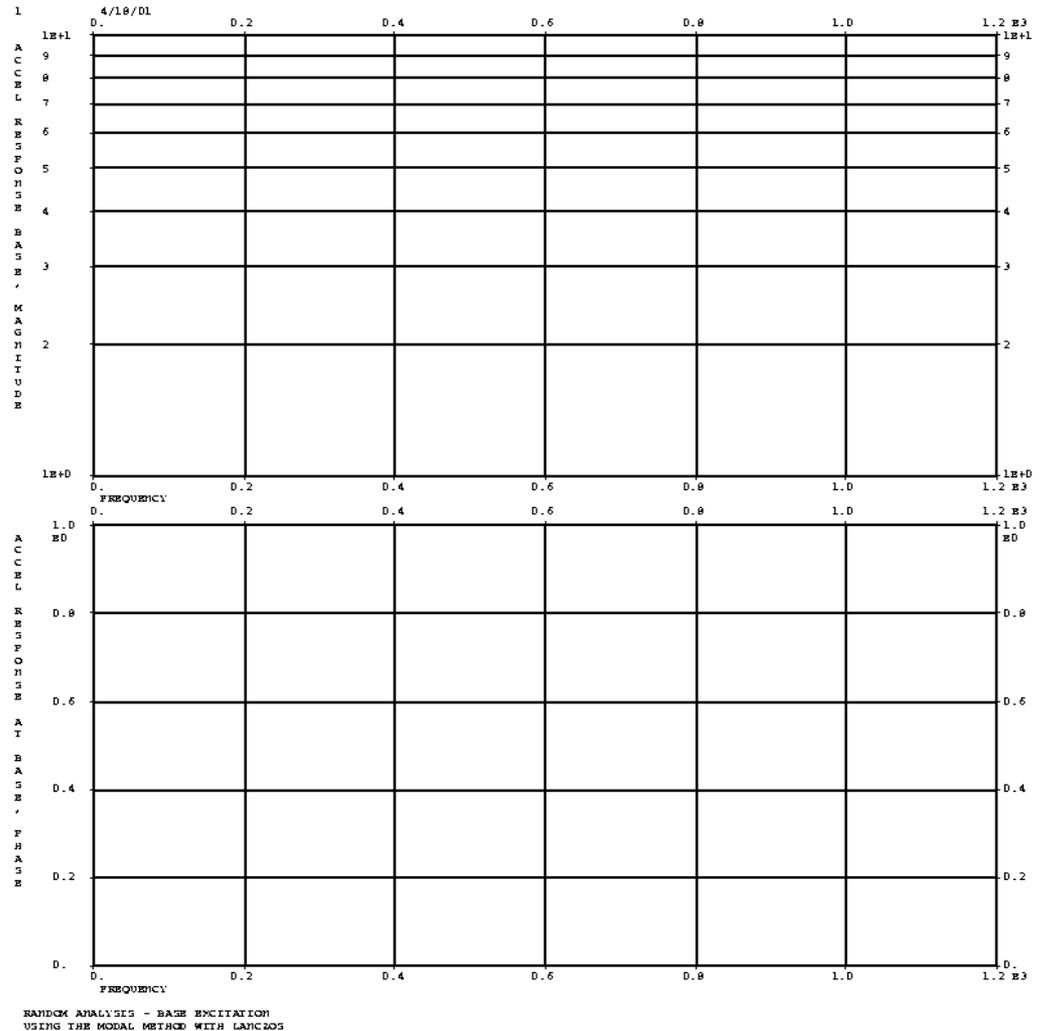
  

XY - O U T P U T S U M M A R Y ( A U T O O R P S D F )												
0	PLOT	CURVE	FRAME	CURVE ID./	RMS	NO. POSITIVE	XMIN FOR	XMAX FOR	YMIN FOR	X FOR	YMAX FOR	X FOR*
	TYPE	TYPE	NO.	PANEL : GRID ID	VALUE	CROSSINGS	ALL DATA	ALL DATA	ALL DATA	YMIN	ALL DATA	YMAX
0	PSDF	ACCE	4	9999( 5)	1.561982E+01	3.991722E+02	2.000E+01	1.020E+03	1.000E-01	6.600E+02	1.000E+00	3.000E+01
0	PSDF	ACCE	5	33( 5)	9.228146E+01	3.924336E+02	2.000E+01	1.020E+03	1.072E-01	2.000E+01	4.535E+02	1.337E+02
0	PSDF	ACCE	6	55( 5)	9.166711E+01	3.846913E+02	2.000E+01	1.020E+03	1.072E-01	2.000E+01	4.523E+02	1.337E+02

# Step 10. Review the Graph Results

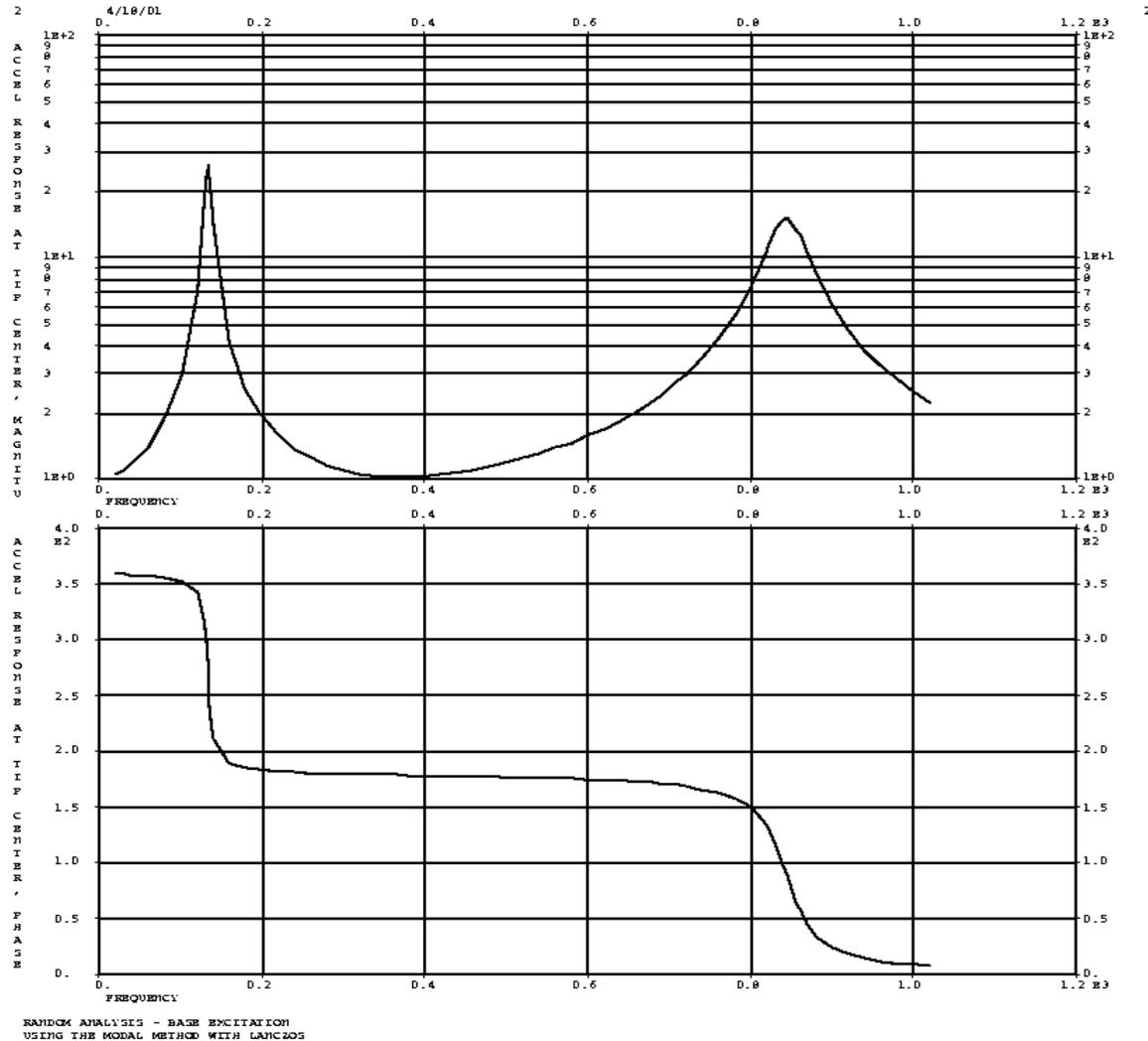
Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions in workshop 4, step 9.

Acceleration response at the base, Grid point 9999



# Step 10. Review the Graph Results (Cont.)

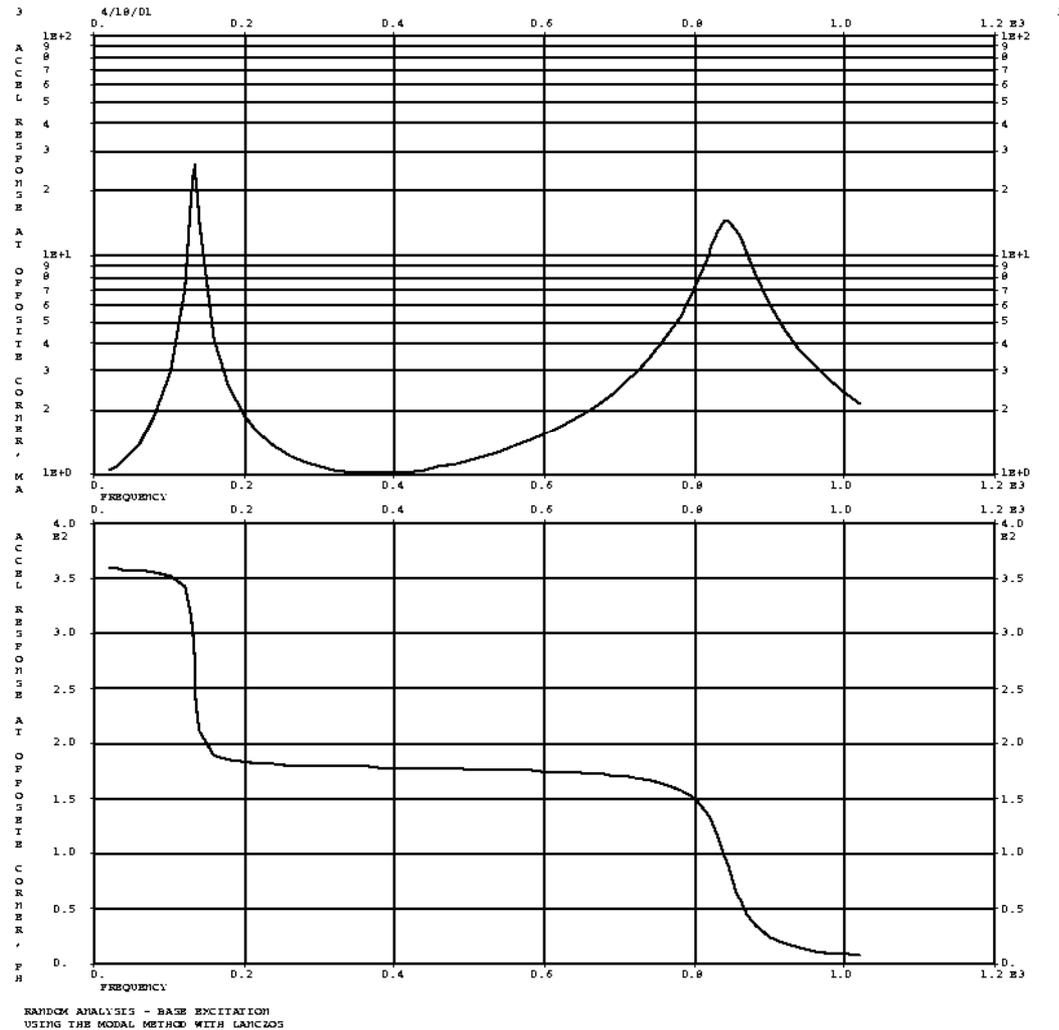
Acceleration response at tip center, Grid point 33



RANDOM ANALYSIS - BASE EXCITATION  
USING THE MODAL METHOD WITH LANCZOS

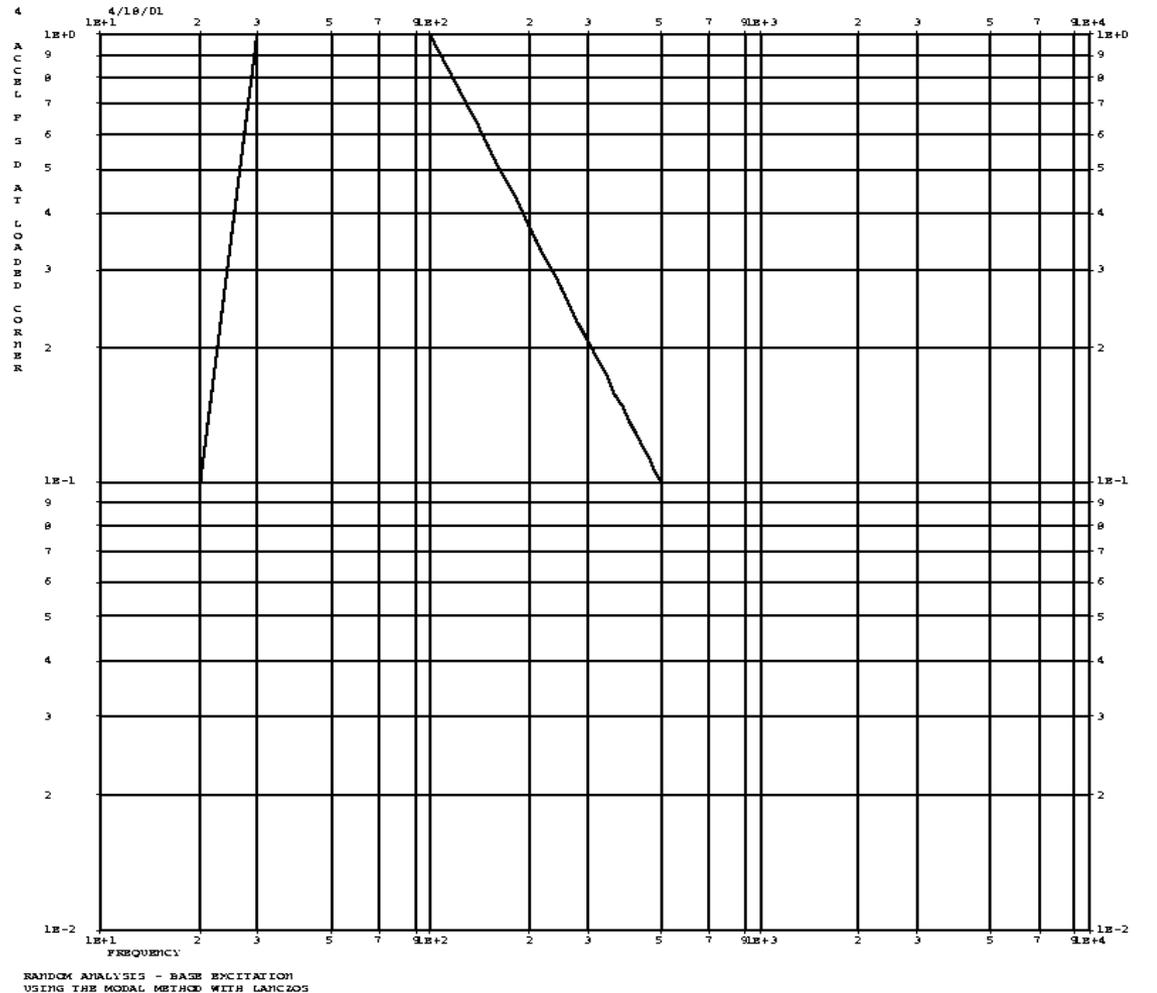
# Step 10. Review the Graph Results (Cont.)

Acceleration response at corner of tip, Grid point 55



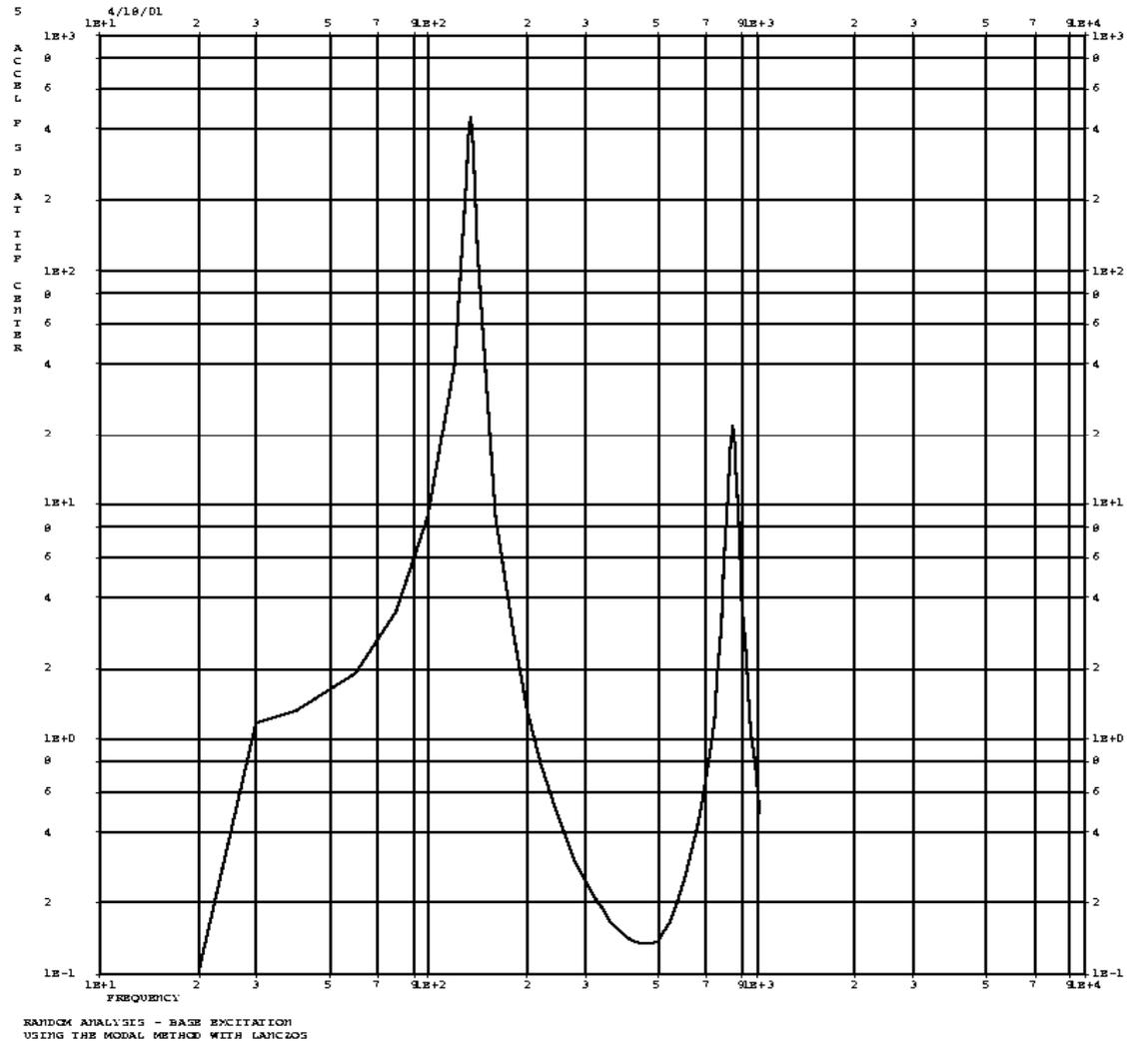
# Step 10. Review the Graph Results (Cont.)

Acceleration PSD at loaded base, Grid 9999



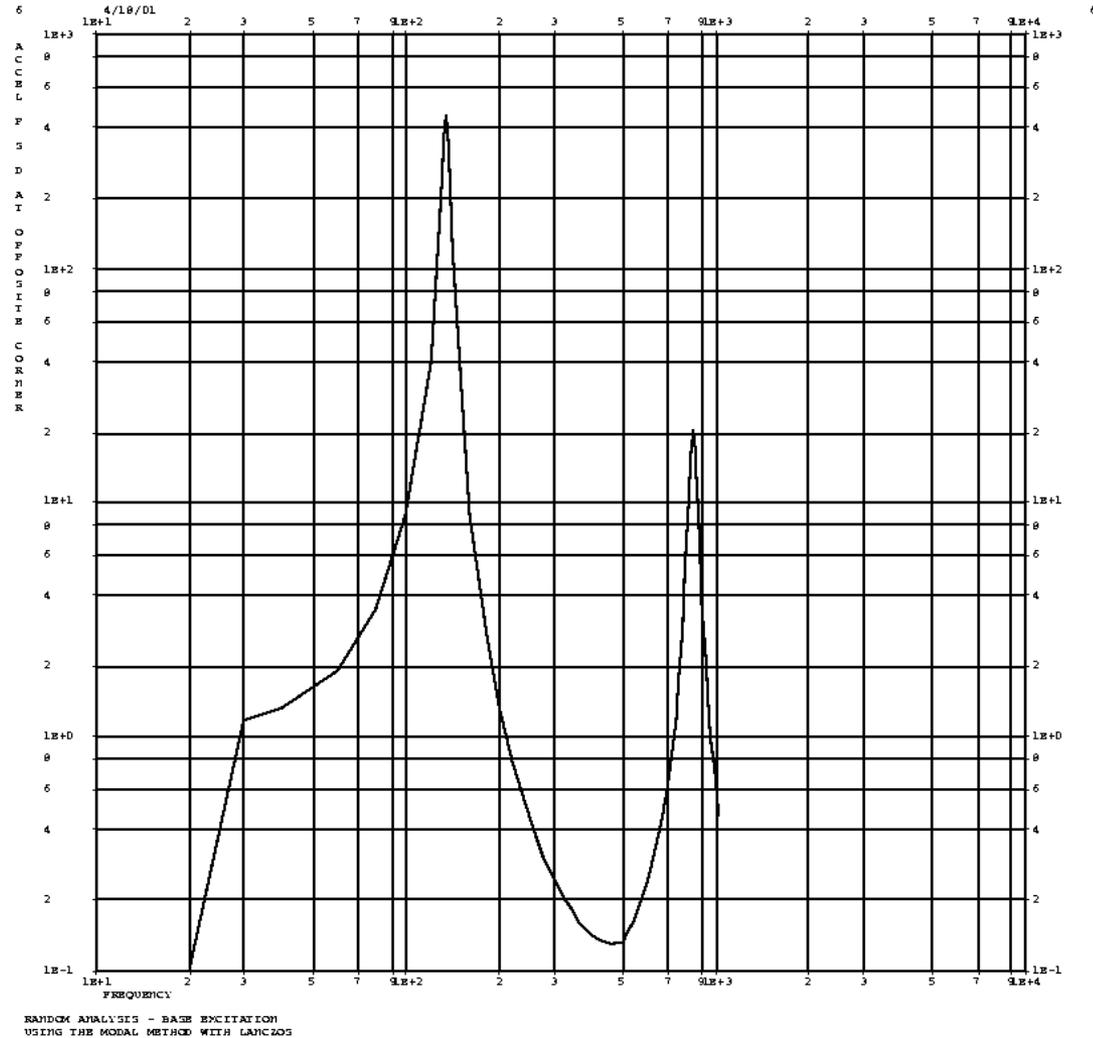
# Step 10. Review the Graph Results (Cont.)

Acceleration PSD at tip center, Grid point 33



# Step 10. Review the Graph Results (Cont.)

Acceleration PSD at tip corner, Grid point 55





# **WORKSHOP 12**

## **RANDOM RESPONSE WITH MULTIPLE INPUTS**



- **Workshop Objective**

- Using the modal method, determine the displacement response spectrum of the tip center point due to the input spectrum of the pressure and point loads listed on the next page.

- **Software Version**

- MSC Nastran 2013

- **Files Required**

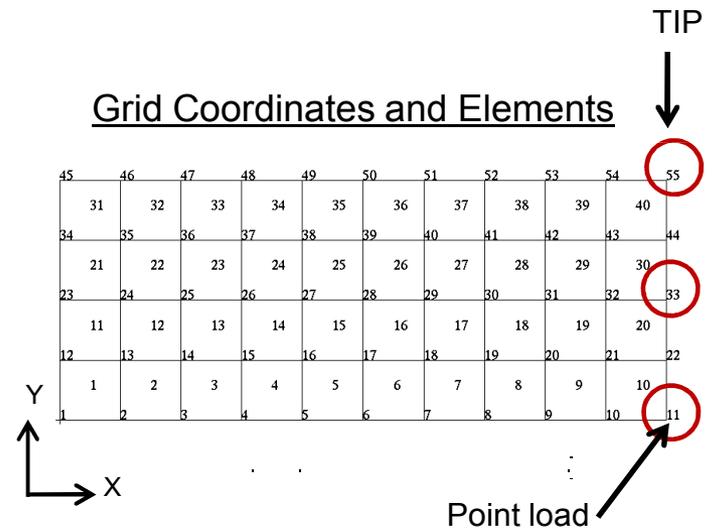
- plate.bdf
- wkshp12.dat

- Problem Description:**

- The model is the plate from workshop 1. The pressure load is a unit pressure load in the z-direction over the entire plate and the point unit load is at grid point 11 in the z direction. The input spectrum of the pressure and unit point is at grid point 11 in the z direction. Use the complex matrix representation (SAB) for the cross spectrum.

Autospectra of Pressure Load		Auto Spectra of Corner Load	
Frequency (Hz)	psi/Hz	Frequency (Hz)	lb/Hz
20	0.1	20	0.5
30	1	30	2.5
100	1	500	2.5
500	0.1	1000	0
1000	0.1		

Cross-Spectrum of Pressure and Corner Loads Real/Imaginary		
Frequency (Hz)	Real Part	Imaginary Part
20	-0.099619	0.007816
100	-0.498097	0.043579
500	0.070711	-0.070711
1000	0	0



- Request Auto psdf and CRMS displacement output at grid points 11, 33, and 55
- Request cross spectrum displacement output between grid point 11 direction 3 and grid point 55 direction 3

- **Suggested Steps**

1. Open and review input file wkshp12.dat.
2. Add Power Spectral Density.
3. Add Auto PSDF and CRSM displacement output.
4. Add request cross spectrum displacement output.
5. Save and run new input file in MSC Nastran.
6. Review the MSC Nastran results using the solution file soln12.f06.
7. Review the graph results.



# Step 2. Add Power Spectral Density

- Define the power spectral density using the **RANDPS** entry in combination with the **TABRND1**.
- For the **RANDPS** entry subcase 1 is the pressure load and subcase 2 is the point load.
- To fill in the tabular information for the **TABRND1** entries use the tables on page WS12-4.
- Add **RANDOM** Case Control Command. With the same identification number as the **RANDPS** entries.

```
soln12.dat
SOL 111
END
TITLE= FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE= USING THE MODAL METHOD WITH LANCZOS
ECHO= UNSORTED
IPC= 1
DET 111= 11, 33, 55
DISPLACEMENT(PLOAD, PHASE)= 111
ACCELERATION(PLOAD, PHASE) = 111
METHOD= 100
FREQUENCY= 200
EDAMPING= 300
RANDOM= 400 (d)
DISP(PSDF, CRMS, PHASE)=111
RCROSS(PSDF, PHASE)=1000
SUBCASE 1
LABEL= PRESSURE LOAD
DLOAD= 100
SUBCASE 2
LABEL= CORNER LOAD
DLOAD= 200
```

```
$ SPECIFY SPECTRAL DENSITY (b)
$
RANDPS, 400, 1, 1, 1., 0., 100
RANDPS, 400, 2, 2, 1., 0., 200
RANDPS, 400, 1, 2, 1., 0., 300
RANDPS, 400, 1, 2, 0., 1., 400
$
TABRND1, 100,
+, 20., 0.1, 30., 1., 100., 1., 500., .1,
+, 1000., .1, ENDT
$
TABRND1, 200,
+, 20., 0.5, 30., 2.5, 500., 2.5, 1000., 0.,
+, ENDT
$
TABRND1, 300,
+, 20., -.099619, 100., -.498097, 500., .070711, 1000., 0.,
+, ENDT
$
TABRND1, 400,
+, 20., .0078158, 100., .0435791, 500., -.70711, 1000., 0.,
+, ENDT
$
```

# Step 3. Add Auto PSDF and CRMS Displacement output

Add a **DISP** command in the Case Control section to request the **PSDF**, **CRMS**, and **PHASE** output. Make sure the value for this command equals the **SET ID** number.

```
$
$   soln12.dat
$
SOL 111
CEND
TITLE= FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE= USING THE MODAL METHOD WITH LANCZOS
ECHO= UNSORTED
SPC= 1
SET 111= 11, 33, 55
DISPLACEMENT(PLOT, PHASE)= 111
ACCELERATION(PLOT, PHASE) = 111
METHOD= 100
FREQUENCY= 200
GDAMPING= 300
$
RANDOM= 400
$
DISP(PSDF, CRMS, PHASE)=111
$
SUBCASE 1
LABEL= PRESSURE LOAD
DLOAD= 100
SUBCASE 2
LABEL = CORNER LOAD
DLOAD= 200
$
OUTPUT (XYPLOT)
$
*TCRIP=
```

# Step 4. Add Request Cross Spectrum Displacement output

- Add the cross-spectral entry **RCROSS**, request displacement output between grid point 11 direction 3 and grid point 55 direction 3
- Add the **RCROSS** output in the Case Control Section. Make sure the identification number matches the SID for the **RCROSS** entry in the Bulk Data section.

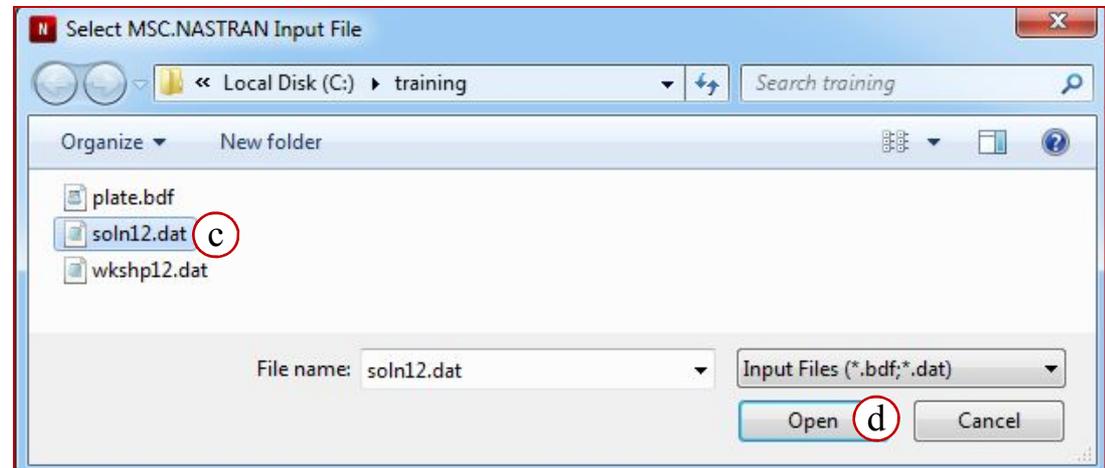
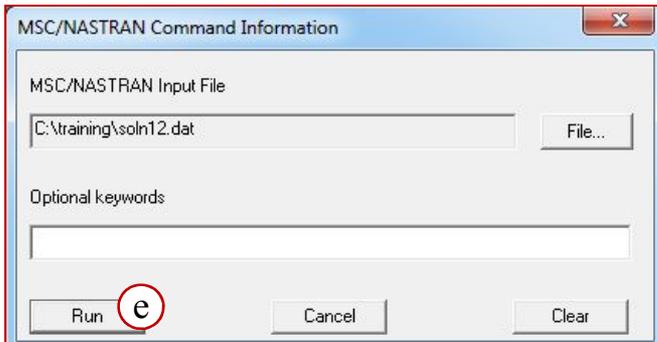
```
soln12.dat
SCL 111
LEND
TITLE= FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS
SUBTITLE= USING THE MODAL METHOD WITH LANCZOS
ECHO= UNSORTED
SPC= 1
SET 111= 11, 33, 55
DISPLACEMENT(PLOT, PHASE)= 111
ACCELERATION(PLOT, PHASE) = 111
METHOD= 100
FREQUENCY= 200
SDAMPING= 300
RANDOM= 400
DISP(PSDF, CRMS, PHASE)=111
b RCROSS(PSDF, PHASE)=1000
SUBCASE 1
LABEL= PRESSURE LOAD
DLOAD= 100
SUBCASE 2
LABEL = CORNER LOAD
DLOAD= 200
```

```
***** SPECTRAL DENSITY *****
RANDPS, 400, 1, 1, 1., 0., 100
RANDPS, 400, 2, 2, 1., 0., 200
RANDPS, 400, 1, 2, 1., 0., 300
RANDPS, 400, 1, 2, 0., 1., 400
TABRND1, 100,
+, 20., 0.1, 30., 1., 100., 1., 500., .1,
+, 1000., .1, ENDT
TABRND1, 200,
+, 20., 0.5, 30., 2.5, 500., 2.5, 1000., 0.,
+, ENDT
TABRND1, 300,
+, 20., -.099619, 100., -.498097, 500., .070711, 1000., 0.,
+, ENDT
TABRND1, 400,
+, 20., .0078158, 100., .0435791, 500., -.70711, 1000., 0.,
+, ENDT
SPECIFY CROSS-SPECTRAL DENSITY
a RCROSS,1000, DISP,11,3,DISP,55,3
ENDDATA
```

# Step 5. Save and Run the New Input File

Save and run the modified file in Nastran.

- a. Save the modified file as **soln12.dat**.
- b. Double click the **MSC Nastran** icon.
- c. Navigate to the correct directory and select the file **soln12.dat**.
- d. Click **Open**.
- e. Click **Run**.



# Step 6. Review the Results in the Solution File

D I S P L A C E M E N T   V E C T O R ( R O O T   M E A N   S Q U A R E )							
POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
11	G	2.217669E-10	3.399755E-10	1.376854E+00	8.629130E-02	3.851210E-01	2.870092E-10
33	G	4.747627E-11	3.394904E-10	1.377021E+00	8.664111E-02	3.844410E-01	2.681256E-10
55	G	3.086639E-10	3.532151E-10	1.378706E+00	8.410326E-02	3.849473E-01	2.787296E-10
JULY 5, 2013 MSC Nastran 5/30/13							

D I S P L A C E M E N T   V E C T O R ( N U M B E R   O F   Z E R O   C R O S S I N G S )							
POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
11	G	1.364917E+02	1.362757E+02	1.401700E+02	6.491689E+02	1.503498E+02	1.362929E+02
33	G	1.355889E+02	1.362910E+02	1.360215E+02	6.552164E+02	1.492609E+02	1.363054E+02
55	G	1.361721E+02	1.362927E+02	1.432664E+02	6.581000E+02	1.498830E+02	1.362823E+02

# Step 6. Review the Results in the Solution File (Cont.)

RANDOM 400

POINT-ID = 11

D I S P L A C E M E N T   V E C T O R  
( P O W E R   S P E C T R A L   D E N S I T Y   F U N C T I O N )

FREQUENCY	TYPE	T1	T2	T3	R1	R2	R3
2.000000E+01	G	2.047311E-24	4.813178E-24	7.947331E-05	2.155795E-07	6.016015E-06	3.429897E-24
4.000000E+01	G	3.063236E-23	7.202370E-23	1.189875E-03	1.059814E-06	8.969508E-05	5.132467E-23
6.000000E+01	G	3.794026E-23	8.919526E-23	1.465137E-03	1.070977E-06	1.104442E-04	6.356211E-23
8.000000E+01	G	5.574523E-23	1.310395E-22	2.142037E-03	1.086197E-06	1.618793E-04	9.338263E-23
1.000000E+02	G	1.114823E-22	2.620410E-22	4.271507E-03	1.111215E-06	3.248373E-04	1.867421E-22
1.200000E+02	G	5.202125E-22	1.222797E-21	1.998794E-02	1.157916E-06	1.539923E-03	8.714393E-22
1.400000E+02	G	1.539327E-21	3.618264E-21	5.925515E-02	1.630665E-06	4.635199E-03	2.578667E-21
1.600000E+02	G	1.029181E-22	2.418989E-22	3.963873E-03	1.260984E-06	3.156277E-04	1.724026E-22
1.800000E+02	G	2.862338E-23	6.726738E-23	1.101076E-03	1.252672E-06	8.950988E-05	4.794377E-23
2.000000E+02	G	1.196908E-23	2.812178E-23	4.588214E-04	1.273440E-06	3.821337E-05	2.004435E-23
2.200000E+02	G	6.082900E-24	1.428679E-23	2.317123E-04	1.305726E-06	1.985387E-05	1.018378E-23
2.400000E+02	G	3.471220E-24	8.148420E-24	1.309352E-04	1.346497E-06	1.159904E-05	5.808679E-24
2.600000E+02	G	2.140898E-24	5.021786E-24	7.962531E-05	1.395422E-06	7.335359E-06	3.580120E-24
2.800000E+02	G	1.397064E-24	3.273601E-24	5.096935E-05	1.453113E-06	4.916464E-06	2.334032E-24
3.000000E+02	G	9.521937E-25	2.228048E-24	3.386632E-05	1.520738E-06	3.447607E-06	1.588748E-24
3.200000E+02	G	6.722475E-25	1.570069E-24	2.313863E-05	1.599961E-06	2.508359E-06	1.119715E-24
3.400000E+02	G	4.889780E-25	1.139250E-24	1.614930E-05	1.693015E-06	1.882844E-06	8.126016E-25
3.600000E+02	G	3.651952E-25	8.481742E-25	1.146142E-05	1.802851E-06	1.452345E-06	6.050995E-25
3.800000E+02	G	2.795128E-25	6.465663E-25	8.249326E-06	1.933388E-06	1.147908E-06	4.613752E-25
4.000000E+02	G	2.190875E-25	5.042267E-25	6.447273E-06	2.089890E-06	1.263417E-06	3.599034E-25

RANDOM 400

POINT-ID = 11

D I S P L A C E M E N T   V E C T O R  
( C U M U L A T I V E   R O O T   M E A N   S Q U A R E )

FREQUENCY	TYPE	T1	T2	T3	R1	R2	R3
2.000000E+01	G	0.0	0.0	0.0	0.0	0.0	0.0
4.000000E+01	G	1.807752E-11	2.771947E-11	1.126653E-01	3.571265E-03	3.093721E-02	2.339969E-11
6.000000E+01	G	3.182016E-11	4.879096E-11	1.981000E-01	5.836252E-03	5.439213E-02	4.118754E-11
8.000000E+01	G	4.415176E-11	6.769716E-11	2.744364E-01	7.458793E-03	7.537732E-02	5.714771E-11
1.000000E+02	G	6.018019E-11	9.226977E-11	3.734311E-01	8.809524E-03	1.027079E-01	7.789164E-11
1.200000E+02	G	9.969255E-11	1.528466E-10	6.180981E-01	1.001494E-02	1.708698E-01	1.290307E-10
1.400000E+02	G	1.747398E-10	2.679043E-10	1.083732E+00	1.132187E-02	3.015754E-01	2.261636E-10
1.600000E+02	G	2.166944E-10	3.322263E-10	1.344123E+00	1.253401E-02	3.747746E-01	2.804651E-10
1.800000E+02	G	2.197086E-10	3.368471E-10	1.362834E+00	1.349955E-02	3.801413E-01	2.843662E-10
2.000000E+02	G	2.206304E-10	3.382601E-10	1.368545E+00	1.440482E-02	3.818175E-01	2.855591E-10
2.200000E+02	G	2.210392E-10	3.388864E-10	1.371065E+00	1.527386E-02	3.825772E-01	2.860879E-10
2.400000E+02	G	2.212552E-10	3.392172E-10	1.372387E+00	1.611871E-02	3.829880E-01	2.863673E-10
2.600000E+02	G	2.213820E-10	3.394113E-10	1.373154E+00	1.694792E-02	3.832351E-01	2.865312E-10
2.800000E+02	G	2.216378E-10	3.395435E-10	1.373728E+00	1.778344E-02	3.834950E-01	2.866344E-10

# Step 6. Review the Results in the Solution File (Cont.)

XY - OUTPUT SUMMARY (RESPONSE)										
SUBCASE ID	CURVE TYPE	FRAME NO.	CURVE ID. / PANEL : GRID ID	XMIN-FRAME / ALL DATA	XMAX-FRAME / ALL DATA	YMIN-FRAME / ALL DATA	X FOR YMIN	YMAX-FRAME / ALL DATA	X FOR YMAX	
1	DISP	1	11( 5,--)	2.000000E+01	1.000000E+03	5.214994E-04	1.000000E+03	2.645494E-01	1.400000E+02	
1	DISP	1	11(--, 11)	2.000000E+01	1.000000E+03	5.214994E-04	1.000000E+03	2.645494E-01	1.400000E+02	
2	DISP	2	11( 5,--)	2.000000E+01	1.000000E+03	1.937994E+01	1.000000E+03	3.594682E+02	2.000000E+01	
2	DISP	2	11(--, 11)	2.000000E+01	1.000000E+03	7.341043E-05	3.800000E+02	6.694620E-02	1.400000E+02	
1	DISP	3	33( 5,--)	2.000000E+01	1.000000E+03	7.341043E-05	3.800000E+02	6.694620E-02	1.400000E+02	
1	DISP	3	33(--, 11)	2.000000E+01	1.000000E+03	1.841973E+02	2.400000E+02	3.595171E+02	2.000000E+01	
2	DISP	4	33( 5,--)	2.000000E+01	1.000000E+03	1.841973E+02	2.400000E+02	3.595171E+02	2.000000E+01	
2	DISP	4	33(--, 11)	2.000000E+01	1.000000E+03	5.543213E-04	1.000000E+03	2.649228E-01	1.400000E+02	
1	DISP	5	55( 5,--)	2.000000E+01	1.000000E+03	5.543213E-04	1.000000E+03	2.649228E-01	1.400000E+02	
1	DISP	5	55(--, 11)	2.000000E+01	1.000000E+03	1.875292E+01	1.000000E+03	3.594681E+02	2.000000E+01	
2	DISP	6	55( 5,--)	2.000000E+01	1.000000E+03	1.875292E+01	1.000000E+03	3.594681E+02	2.000000E+01	
2	DISP	6	55(--, 11)	2.000000E+01	1.000000E+03	4.009693E-05	6.000000E+02	6.759480E-02	1.400000E+02	
2	DISP	6	55( 5,--)	2.000000E+01	1.000000E+03	4.009693E-05	6.000000E+02	6.759480E-02	1.400000E+02	
2	DISP	6	55(--, 11)	2.000000E+01	1.000000E+03	1.822676E+02	3.400000E+02	3.594853E+02	2.000000E+01	
1	DISP	5	55( 5,--)	2.000000E+01	1.000000E+03	5.213259E-04	1.000000E+03	2.645494E-01	1.400000E+02	
1	DISP	5	55(--, 11)	2.000000E+01	1.000000E+03	5.213259E-04	1.000000E+03	2.645494E-01	1.400000E+02	
2	DISP	6	55( 5,--)	2.000000E+01	1.000000E+03	1.938930E+01	1.000000E+03	3.594682E+02	2.000000E+01	
2	DISP	6	55(--, 11)	2.000000E+01	1.000000E+03	1.938930E+01	1.000000E+03	3.594682E+02	2.000000E+01	
2	DISP	6	55( 5,--)	2.000000E+01	1.000000E+03	2.097658E-04	1.000000E+03	6.799091E-02	1.400000E+02	
2	DISP	6	55(--, 11)	2.000000E+01	1.000000E+03	2.097658E-04	1.000000E+03	6.799091E-02	1.400000E+02	
2	DISP	6	55( 5,--)	2.000000E+01	1.000000E+03	7.973937E+00	7.599999E+02	3.594539E+02	2.000000E+01	
2	DISP	6	55(--, 11)	2.000000E+01	1.000000E+03	7.973937E+00	7.599999E+02	3.594539E+02	2.000000E+01	

XY - OUTPUT SUMMARY (AUTO OR PSD F)											
PLOT TYPE	CURVE TYPE	FRAME NO.	CURVE ID. / PANEL : GRID ID	RMS VALUE	NO. POSITIVE CROSSINGS	XMIN FOR ALL DATA	XMAX FOR ALL DATA	YMIN FOR ALL DATA	X FOR YMIN	YMAX FOR ALL DATA	X FOR* YMAX
PSDF	DISP	7	11( 5)	1.376854E+00	1.401700E+02	2.000E+01	1.000E+03	2.720E-08	1.000E+03	5.926E-02	1.400E+02
PSDF	DISP	8	33( 5)	1.377021E+00	1.360215E+02	2.000E+01	1.000E+03	3.073E-08	1.000E+03	5.949E-02	1.400E+02
PSDF	DISP	9	55( 5)	1.378706E+00	1.432664E+02	2.000E+01	1.000E+03	2.718E-08	1.000E+03	5.937E-02	1.400E+02

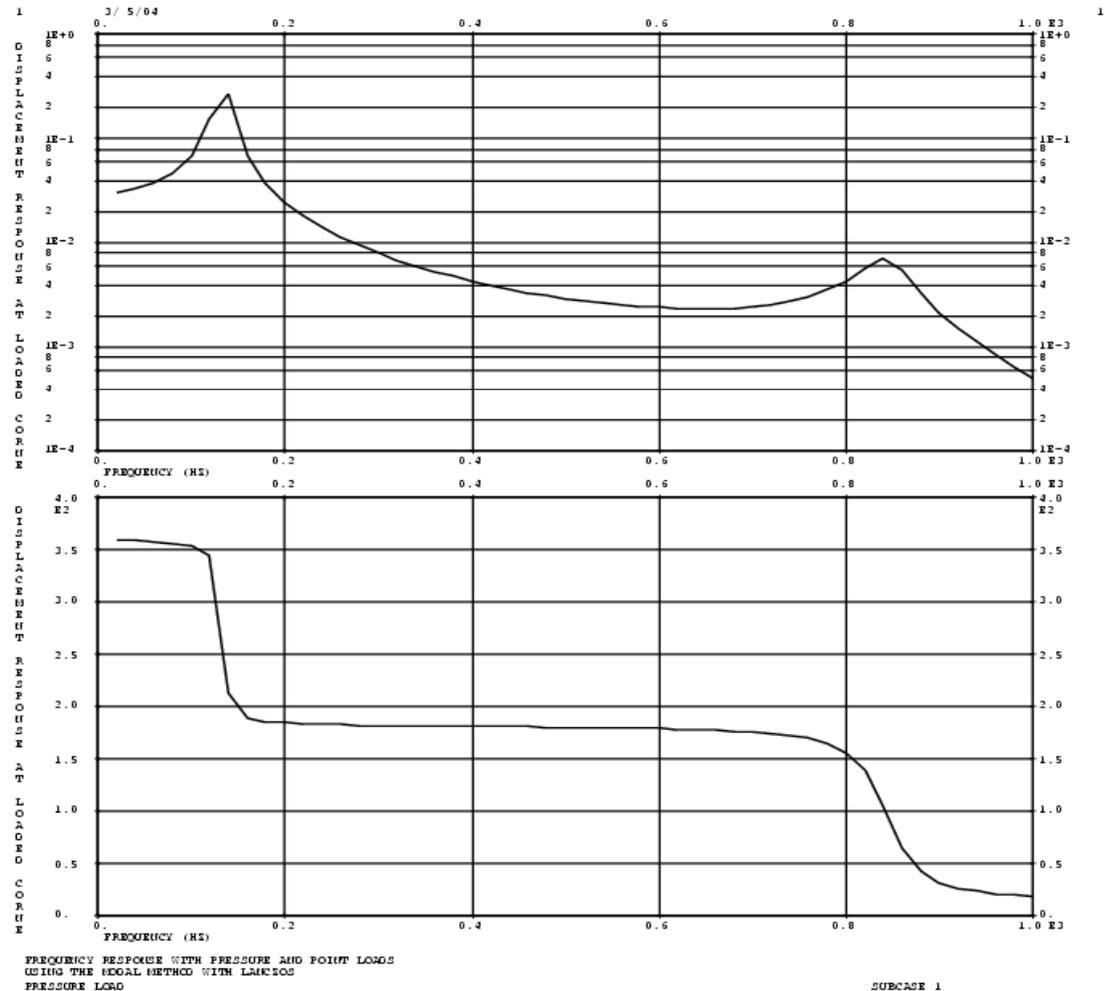
# Step 6. Review the Results in the Solution File (Cont.)

FREQUENCY RESPONSE WITH PRESSURE AND POINT LOADS USING THE MODAL METHOD WITH LANCZOS PRESSURE LOAD SEQUENTIAL CURVE-ID = 1							PAGE 49
COMPLEX CROSS-POWER SPECTRAL DENSITY FUNCTION (MAGNITUDE/PHASE)							RANDOM 400
RCROSS	RTYPE1	ID1	COMP1	RTYPE2	ID2	COMP2	CURID
1000	DISP	11	3	DISP	55	3	0
FREQUENCY	CPSDF			FREQUENCY	CPSDF		
2.000000E+01	7.782715E-05	/	359.7912	4.000000E+01	1.169207E-03	/	359.9816
6.000000E+01	1.446440E-03	/	359.9715	8.000000E+01	2.125043E-03	/	359.9651
1.000000E+02	4.256192E-03	/	359.9659	1.200000E+02	1.995366E-02	/	0.0206
1.400000E+02	5.931301E-02	/	0.0270	1.600000E+02	3.981689E-03	/	359.9641
1.800000E+02	1.110766E-03	/	359.8067	2.000000E+02	4.651507E-04	/	359.5229
2.200000E+02	2.361836E-04	/	359.0721	2.400000E+02	1.342108E-04	/	358.4012
2.600000E+02	8.205519E-05	/	357.4377	2.800000E+02	5.276163E-05	/	356.0812
3.000000E+02	3.515652E-05	/	354.1868	3.200000E+02	2.402327E-05	/	351.5385
3.400000E+02	1.670592E-05	/	347.8049	3.600000E+02	1.176429E-05	/	342.4655
3.800000E+02	8.387206E-06	/	334.7123	4.000000E+02	6.119114E-06	/	323.4214
4.200000E+02	4.722277E-06	/	307.6403	4.400000E+02	4.072000E-06	/	288.2907
4.600000E+02	4.034619E-06	/	269.2190	4.800000E+02	4.427422E-06	/	253.8799
5.000000E+02	5.106795E-06	/	242.7013	5.200000E+02	5.390141E-06	/	236.1572
5.400000E+02	5.879030E-06	/	229.9111	5.600000E+02	6.667261E-06	/	223.8539
5.800000E+02	7.941909E-06	/	217.8873	6.000000E+02	1.009843E-05	/	211.9292
6.200000E+02	1.407104E-05	/	205.9172	6.400000E+02	2.244281E-05	/	199.8112
6.600000E+02	4.367880E-05	/	193.5947	6.799999E+02	9.592201E-05	/	187.2714
6.999999E+02	7.964315E-05	/	180.8491	7.200000E+02	2.743966E-05	/	174.2929
7.400000E+02	1.057218E-05	/	167.3723	7.599999E+02	4.433171E-06	/	158.9403
7.800000E+02	1.351509E-06	/	138.3461	8.000000E+02	1.558494E-06	/	1.1614
8.200000E+02	5.536476E-06	/	343.4609	8.399999E+02	1.063914E-05	/	337.7312
8.600000E+02	6.950112E-06	/	334.6017	8.800000E+02	2.748527E-06	/	332.9402
8.999999E+02	1.156801E-06	/	332.4832	9.199999E+02	5.375280E-07	/	333.2076
9.400000E+02	2.648298E-07	/	335.2509	9.600000E+02	1.325349E-07	/	339.0211
9.799999E+02	6.395403E-08	/	345.7172	1.000000E+03	2.718711E-08	/	359.9906

# Step 7. Review the Graph Results

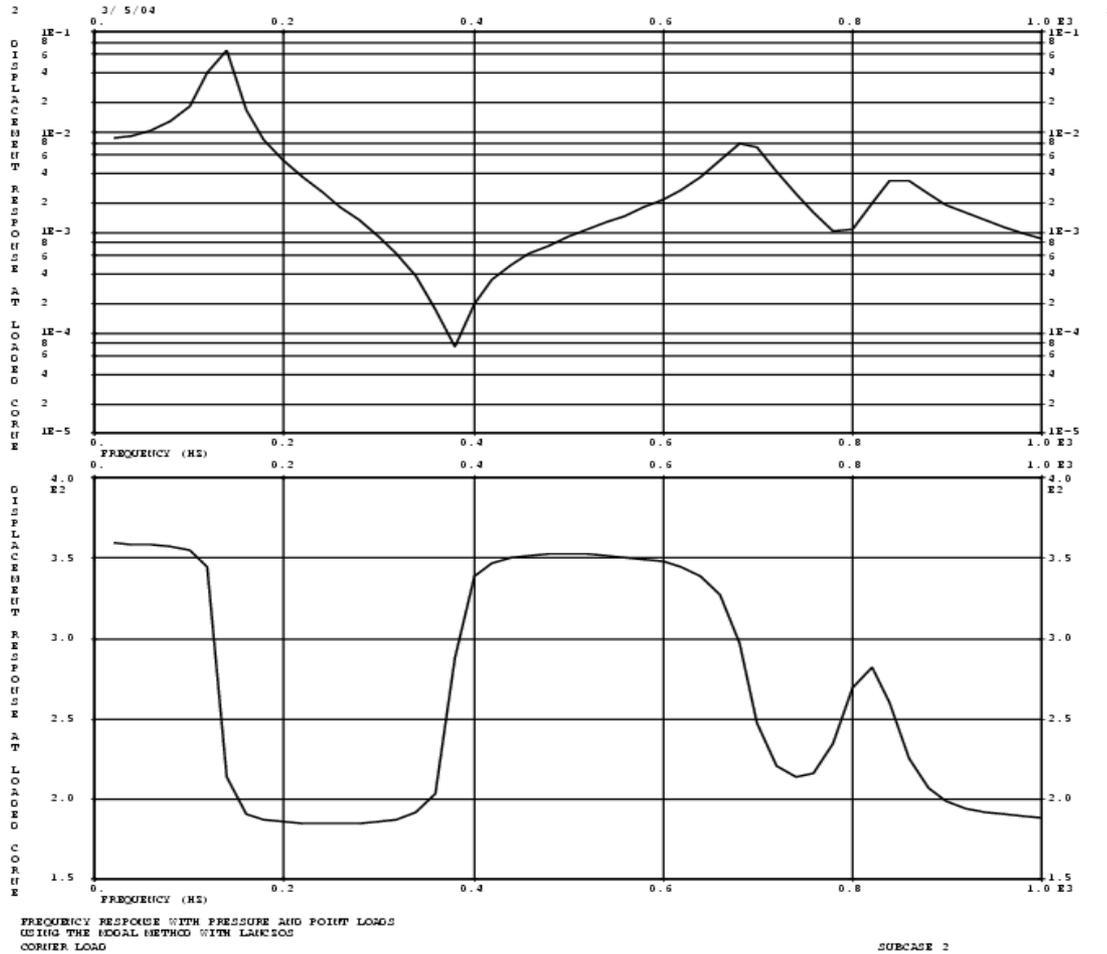
Recall that to obtain the graphs you will need to convert the .plt file to a .ps file, if needed, use the directions given in the workshop 4, step 9.

Pressure load displacement response at loaded corner, grid point 11



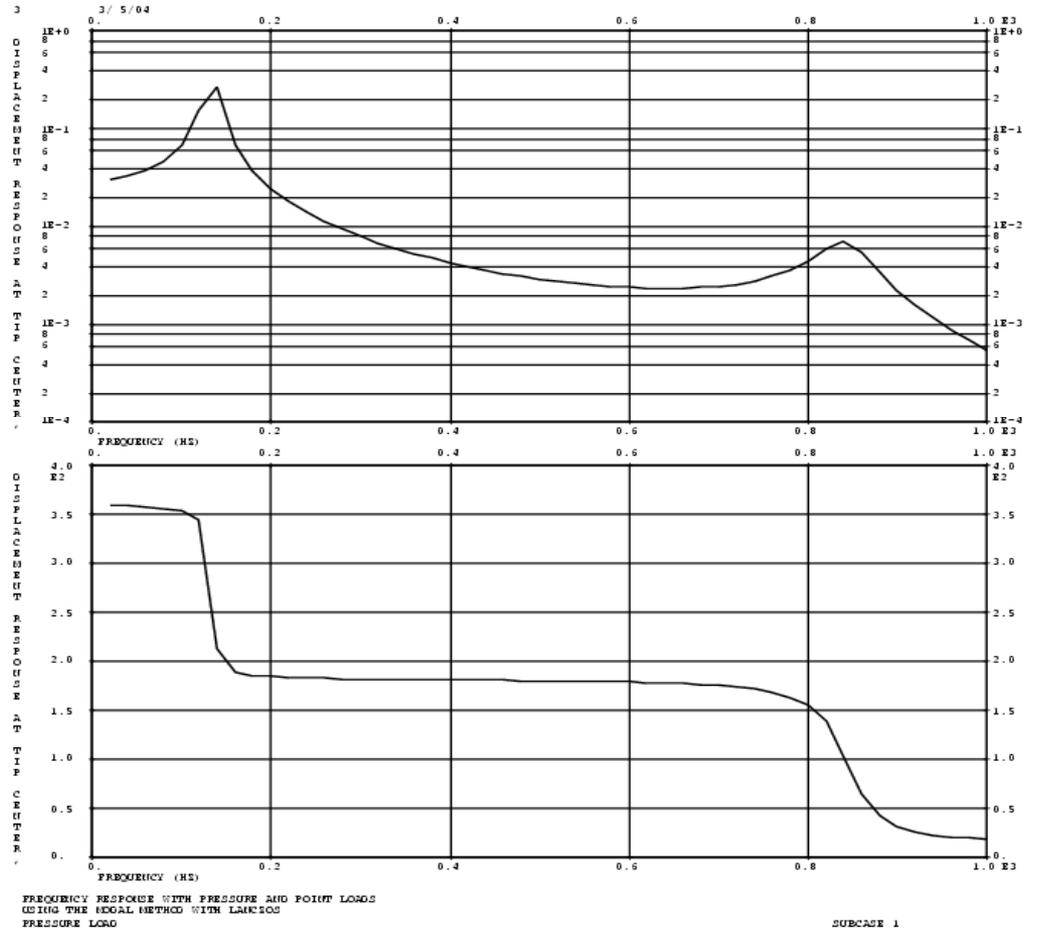
# Step 7. Review the Graph Results (Cont.)

Point load displacement response at loaded corner, grid point 11



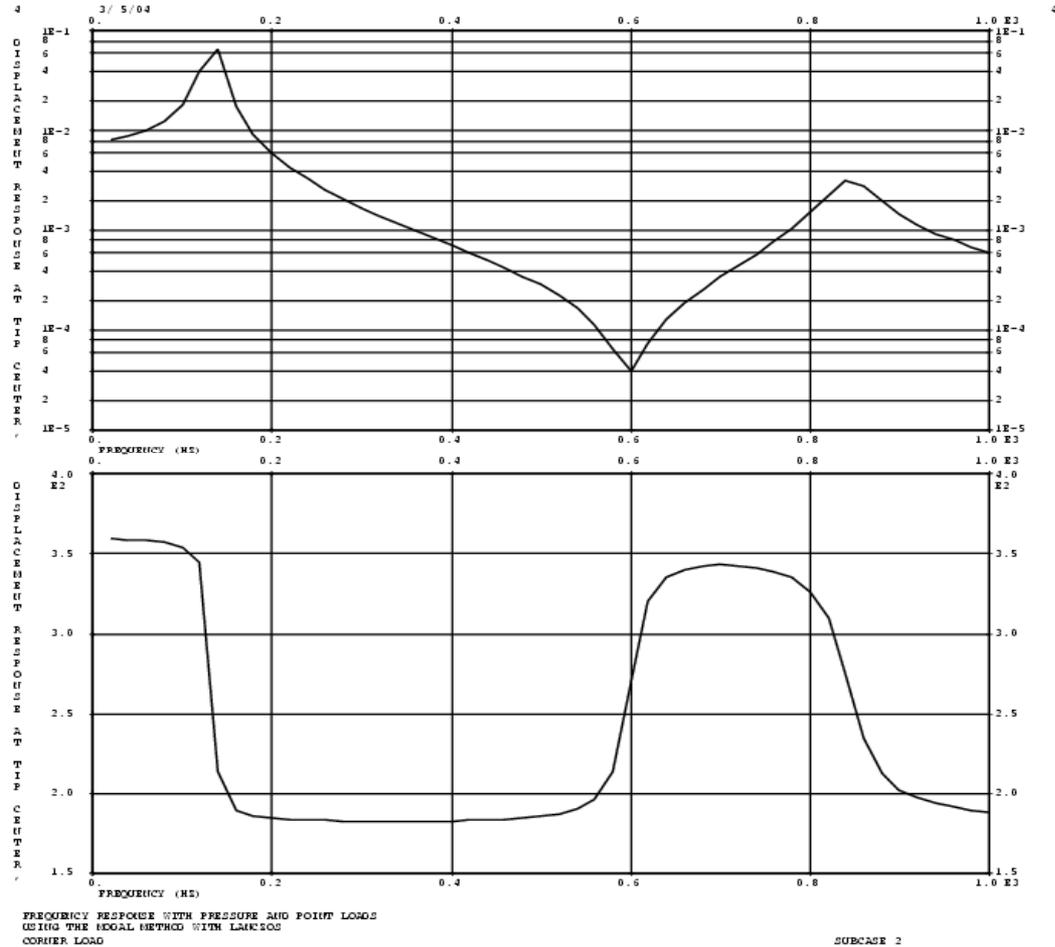
# Step 7. Review the Graph Results (Cont.)

Pressure load displacement response at center tip, grid point 33



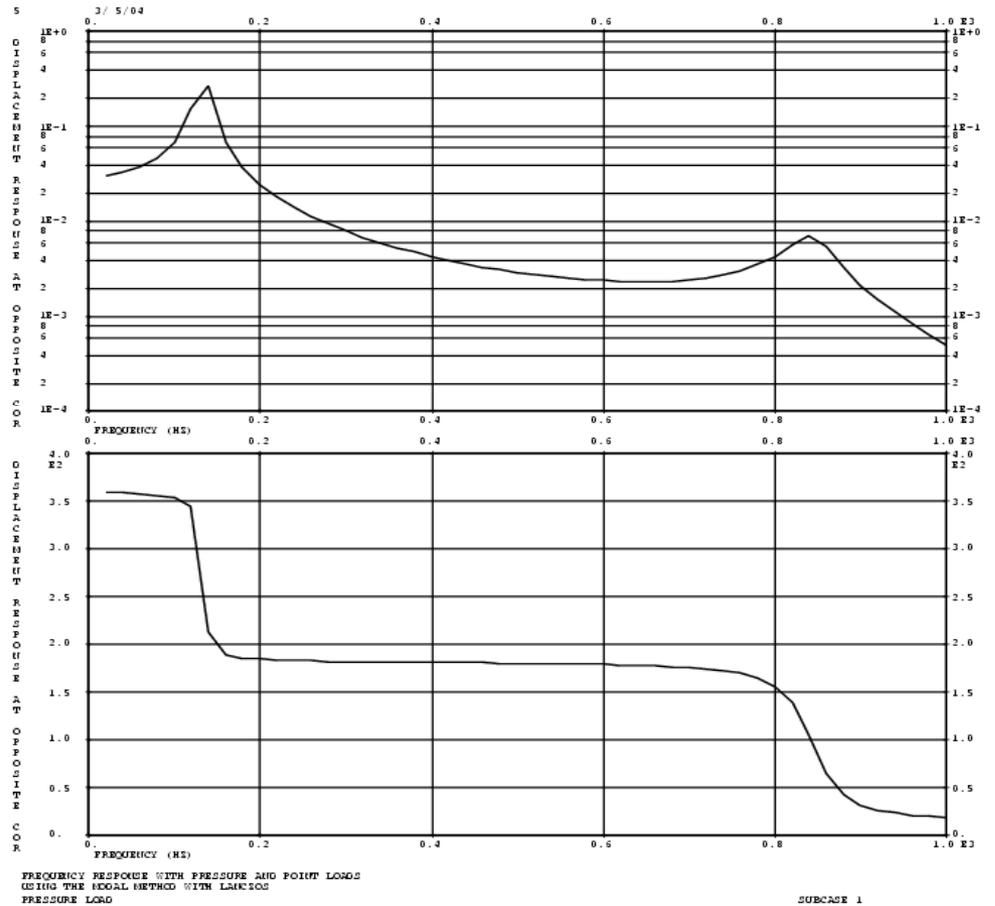
# Step 7. Review the Graph Results (Cont.)

Point load displacement response at center tip, grid point 33



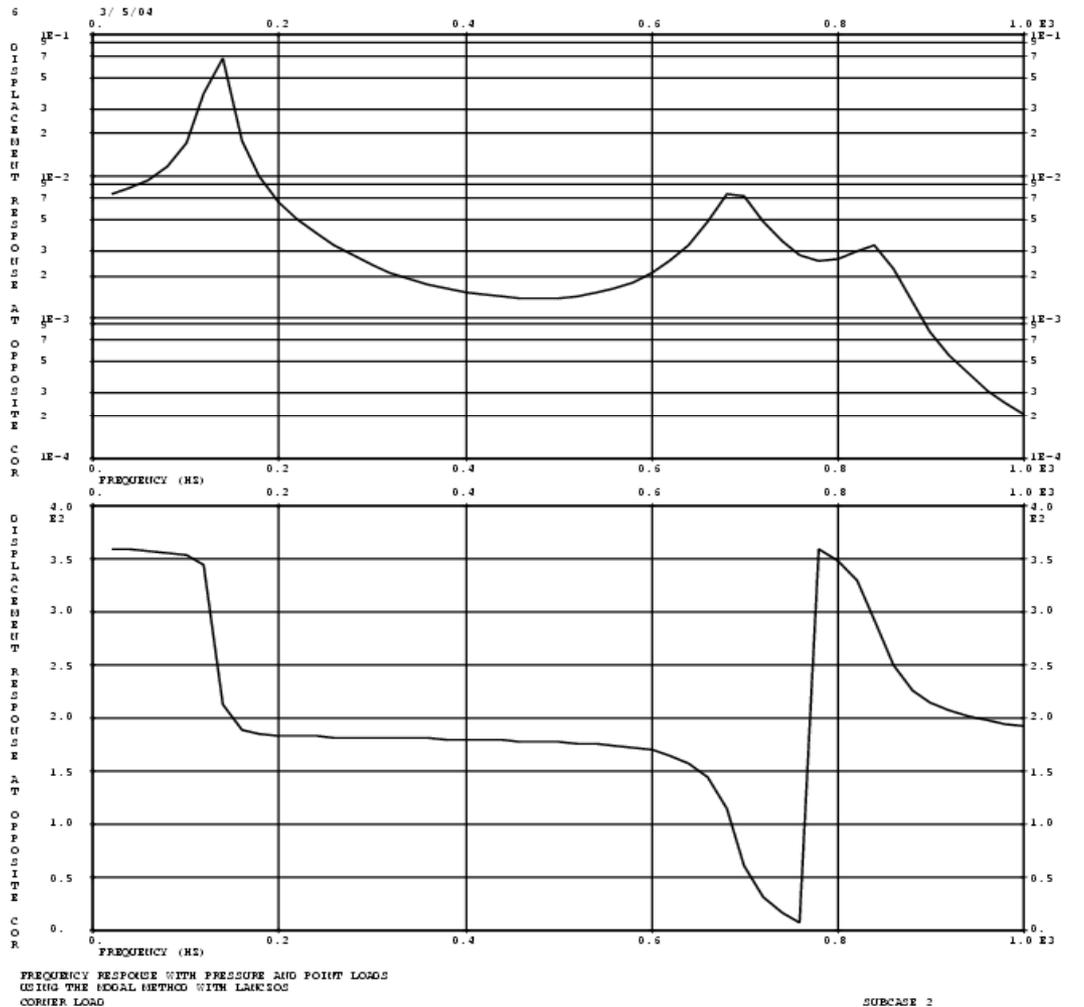
# Step 7. Review the Graph Results (Cont.)

Pressure load displacement response at opposite corner, grid point 55



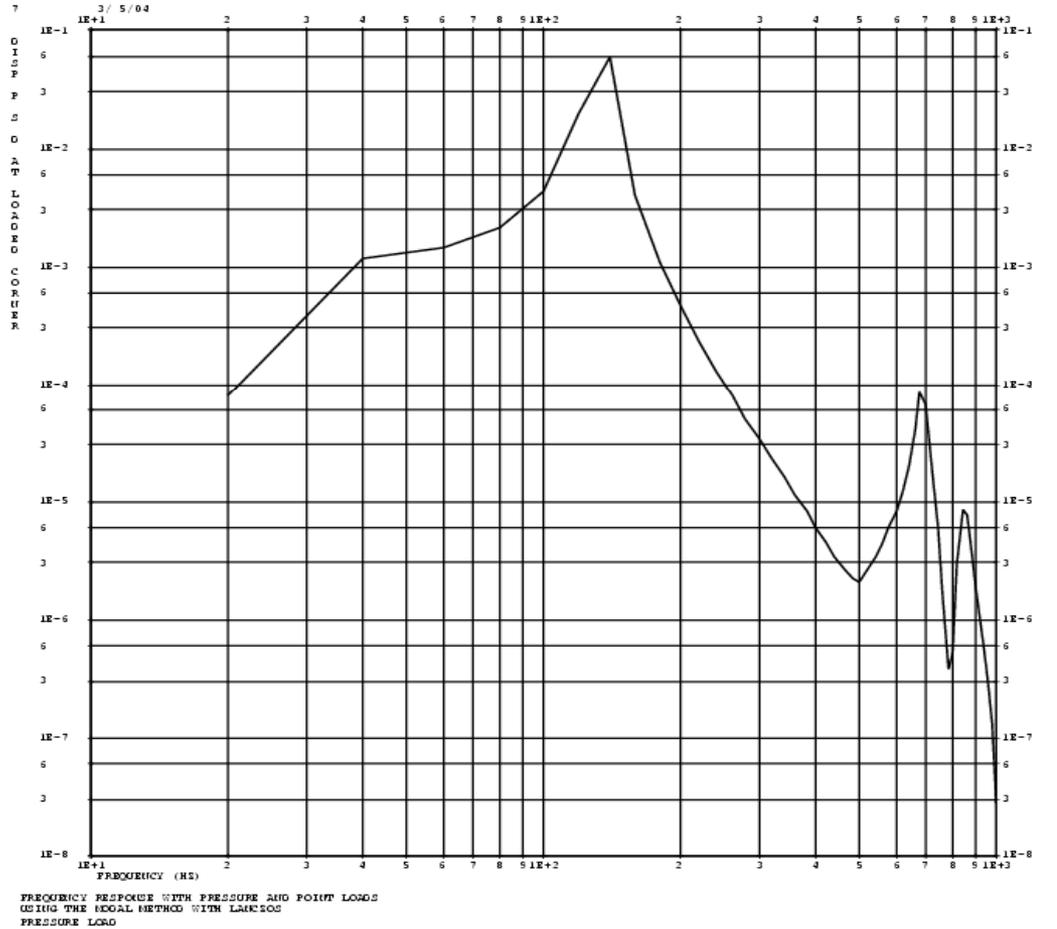
# Step 7. Review the Graph Results (Cont.)

Point load displacement response at opposite corner, grid point 55



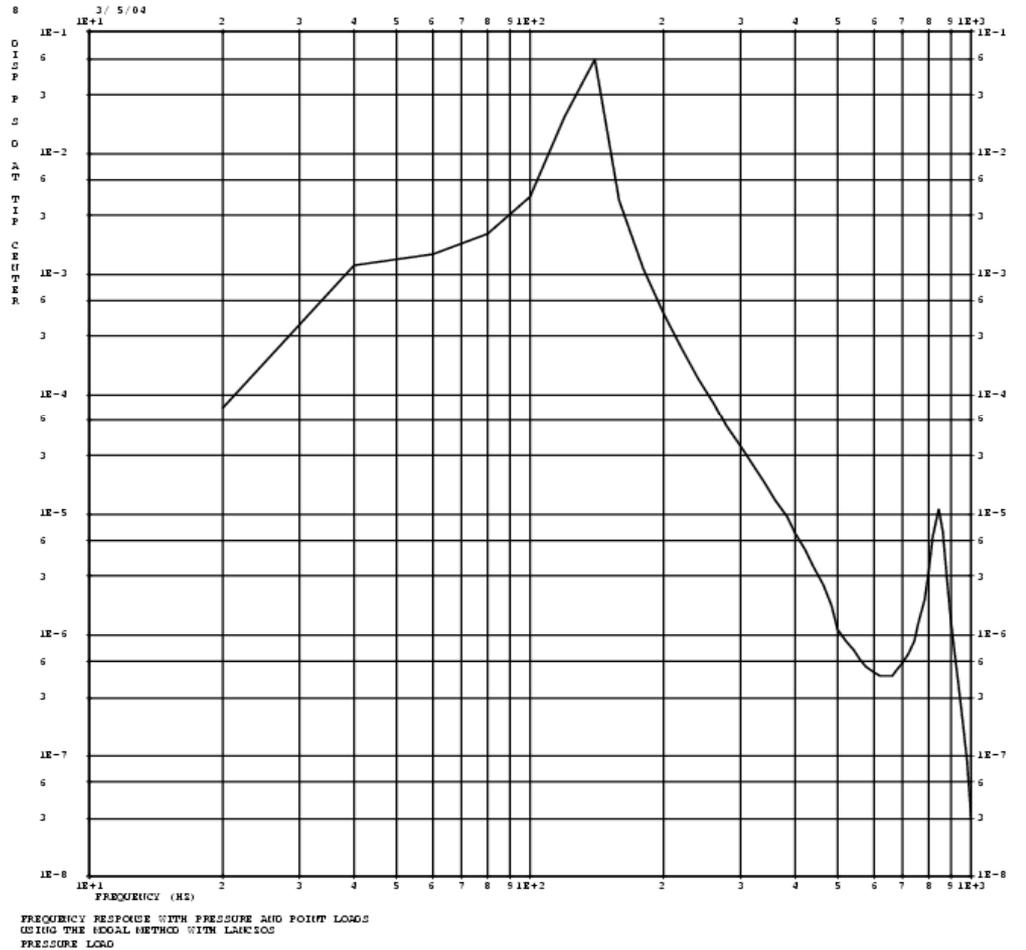
# Step 7. Review the Graph Results (Cont.)

Displacement PSD response at loaded corner, grid point 11



# Step 7. Review the Graph Results (Cont.)

Displacement PSD response at tip center, grid point 33



# Step 7. Review the Graph Results (Cont.)

Displacement PSD response at opposite corner, grid point 55

